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A STUDY OF OPTIMUM COWL SHAPES AND FLOW  
PORT LOCATIONS FOR MINIMUM DRAG WITH  
EFFECTIVE ENGINE COOLING - VOLUME II

Stan R. Fox and Frederick O. Smetana

NORTH CAROLINA STATE UNIVERSITY  
Raleigh, North Carolina 27650

NASA Grant NSG-1584  
November 1980

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National Aeronautics and  
Space Administration

Langley Research Center  
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## ABSTRACT

The successful prediction of the performance of a new or modified aircraft depends heavily on an accurate estimation of its lift and drag. This report consists of the listings, user's instructions, sample inputs, and sample outputs of two computer programs which are especially useful in obtaining an approximate solution of the viscous flow over an arbitrary non-lifting three-dimensional body. The first program performs a potential flow solution by a well-known panel method and readjusts this initial solution to account for the effects of the boundary-layer displacement thickness, a nonuniform but unidirectional onset flow field, and the presence of air intakes and exhausts. The second program is effectually a geometry package which allows the user to change or refine the shape of a body to satisfy particular needs without a significant amount of human intervention.

The report represents in part an effort to reduce the cruise drag of light aircraft through an analytical study of the contributions to the drag arising from the engine cowl shape and the forward fuselage area and also that resulting from the cooling air mass flowing through intake and exhaust sites on the nacelle. The programs may be effectively used to determine the appropriate body modifications or flow port locations to reduce the cruise drag as well as to provide sufficient air flow for cooling the engine.

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## INTRODUCTION

For the past contract year a research program has been conducted for the purpose of reducing the cruise drag of light aircraft for better performance and fuel economy through studying the effects arising from modifications to body shape and the surrounding flow field. The procedures have been described [1] and coded into two FORTRAN computer programs.

The purpose of this report is to present these programs with their complete user's instructions. Sample inputs and outputs are also given to provide references for proper program executions at other computing installations.

The first program - FLOWBODY - performs a potential flow solution by the Hess low-speed panel method [1], [2], [3] and readjusts this initial solution to account for the effects of the boundary-layer displacement thickness, a nonuniform but unidirectional onset flow field, and the presence of air intakes and exhausts. The logic of the program can conveniently be described by the following steps:

- (1) The surface of the isolated fuselage is represented by a sufficiently large number of quadrilaterals or four-sided panels.
- (2) All four corners of the panel are moved into the same plane through a procedure which determines the direction of the normal.
- (3) A nonuniform onset flow field may be superimposed onto the uniform onset flow field.

- (4) A source of undetermined strength is placed on each panel, and the prescribed normal boundary condition is required to be satisfied.
- (5) The resulting system of equations are solved for the source strengths from which the velocity and pressures over the body surface are calculated.
- (6) The system of equations may be resolved for the source strengths to account for the presence of air intakes and exhausts.
- (7) Two-dimensional, momentum-integral-type boundary layer computations are performed along the streamlines to find the local values of displacement thickness and wall shear.
- (8) The wall shear is integrated over the surface to find the skin friction drag.
- (9) The body shape is modified by attaching a wake-body toward the trailing edge and by accounting for the displacement thickness effects.
- (10) A new set of source strengths and surface pressures corresponding to the wake-body shape is calculated.
- (11) The surface pressures are integrated to find the lift and pressure drag.
- (12) The total drag is determined from the sum of the skin friction drag and the pressure drag.

The second program - GRIDPLOT - is a geometry package which may be used to correct body misrepresentations, to change the body geometry, to refine the network or grid of the panels or quadrilaterals that form the surface of the body, and to plot various orthographic, perspective, and stereoscopic views of the

original and the modified body. The workhorse of this program is a cubic-spline curve-fitting method coupled to a coordinate-system rotation-translation technique that is very effective in modeling body shapes with regions of high curvature or changes in slope.

The U. S. customary units used in this report reflect those most commonly used in this country by engineers and scientists in the General Aviation field. The reader may choose to use S.I. units in lieu of U. S. customary units in both FLOWBODY and GRIDPLOT programs with only one restriction in the FLOWBODY program. If locations for air intakes and exhausts are to be specified, U. S. customary units must be used throughout FLOWBODY since the constants in the derivations for internal mass flow obtain from U. S. customary units. Otherwise, S.I. units are completely permissible.

---

## USER'S INSTRUCTIONS - FLOWBODY PROGRAM

The program is written in FORTRAN IV and is designed to execute in single precision on an IBM 370/165 computer with an average execution time of 4 minutes 40 seconds for typically large data set. An average execution requires approximately 426,000 bytes of core storage. The program accepts multiple data sets.

Given a data set describing the half-body\* under consideration, the program may be instructed to calculate an approximate solution of the three-dimensional viscous flow over an arbitrary body and to estimate the body lift and drag coefficients with or without

- (a) a simulated propeller slipstream, and
- (b) mass flow through the body.

The orientation of the body with respect to the body reference axes for the programs is shown in Figure 1.

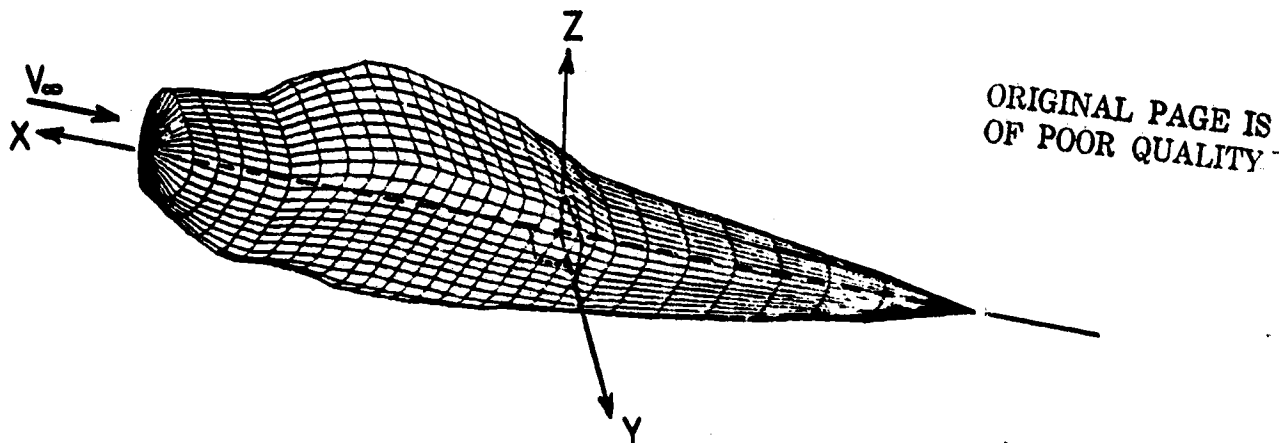


Figure 1: Orientation of the body with respect to the body reference axes

---

\*Since the body is considered to be symmetrical about the X-Z plane, only half of the body is needed to describe the entire body.

The program requires the specification of the following input in the indicated order:

CARD 1:

The read unit number IDS: \_

IDS is a right-adjusted integer number occupying columns 1-5 and specifying that the data is to be read from cards, magnetic tape, disk, etc. The user must supply the suitable job control cards for the specific reads. The IDS parameter controls only the reading of CARD 2, CARD 7, and the Body Description cards.

CARD 2: \_

The title array TITLE: \_\_\_\_\_

The 80 characters of the array TITLE are used for identifying output. The reading of TITLE is controlled by the read unit number IDS.

**\*\* The Flow Control Variables \*\***

CARD 3: .

Columns	<u>F</u> ORTRAN Name	Description
1-20	VINF	Reference free-stream velocity (ft/sec)
21-40	VO	Kinematic viscosity of the fluid in which the body is moving (ft <sup>2</sup> /sec)
41-60	ROE	Density of the fluid in which the body is moving (slug/ft <sup>3</sup> )
61-80	REFA	Reference area upon which the aerodynamic coefficients will be based (ft <sup>2</sup> )

Parameters VINF, VO, ROE, and REFA are single-precision floating-point numbers in E20 fields.

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CARD 4:

Columns	FORTRAN Name	Description
1-20	HVF	Heat of combustion of the fuel being used to develop engine power (BTU/lb <sub>m</sub> )
21-40	SFC	Specific fuel consumption of the engine (lb <sub>m</sub> /ft-lb <sub>f</sub> )
41-60	DEP	Developed engine power or power into airstream (ft-lb <sub>f</sub> /sec)
61-80	CPHA	Specific heat at constant pressure for air (BTU/lb <sub>m</sub> °R)

Parameters HVF, SFC, DEP, and CPHA are single-precision floating-point numbers in E20 fields.

CARD 5:

Columns	FORTRAN Name	Description
1-20	TINF	Reference free-stream temperature (°R)
21-40	EOA	Effective orifice area-representative of that area seen by the cooling fluid passing through the body and about the body (ft <sup>2</sup> )
41-45	IWRITE	Control variable which denotes the amount of output the user desires. IWRITE = 0 yields the normal maximum output ever desired by the user. IWRITE = 1 deletes information given for each input point. IWRITE = 2 deletes streamline and boundary layer information as well as input point information. IWRITE < 0 generates an enormous amount of output dealing with the streamline calculations, and therefore this option should be used with caution.
46-50	IPCH1	Control variable which denotes the punching of the input cards in a form compatible to the NCSU PLOT program of Reference 3. IPCH1 = 0 yields no punched cards, while IPCH1 = 1 produces punched cards.

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CARD 5 (continued):

Columns	FORTRAN Name	Description
51-55	IPCH2	Control variable which denotes the punching of cards of the body after the addition of the wake-body in a form compatible to the NCSU PLOT program of Reference 3. IPCH2 = 0 yields no punched cards, while IPCH2 = 1 produces punched cards.
56-60	IMATCH	Control variable which denotes the matching of the simulated slipstream's power to the specified power into the airstream. With IMATCH = 0, the matching is performed. With IMATCH = 1, no matching occurs and the program utilizes the user-supplied values. Normally, IMATCH = 0 should be specified for an overall program compatibility.

Parameters TINF and EOA are single-precision floating-point numbers in E20 fields, while parameters IWRITE, IPCH1, IPCH2, and IMATCH are right-adjusted integer numbers in I5 fields.

**\*\* Conversion and Test Parameters \*\***

CARD 6:

Columns	FORTRAN Name	Description
1-10	CF	Conversion factor to change the units of the body coordinates points to units of feet. If CF = 0.0, the program automatically sets CF = 1.0. If CF = 1.0, the program assumes that the data units are compatible.
11-15	ITEST	Control parameter which allows only sufficient information of the propeller-slipstream (or series of vortex rings) calculation to be performed for the plotting of the location and diameter of the vortex rings and the induced velocity of such an arrangement of rings. (See Figure 2). ITEST = 0 produces no plots, while ITEST = 1 does.



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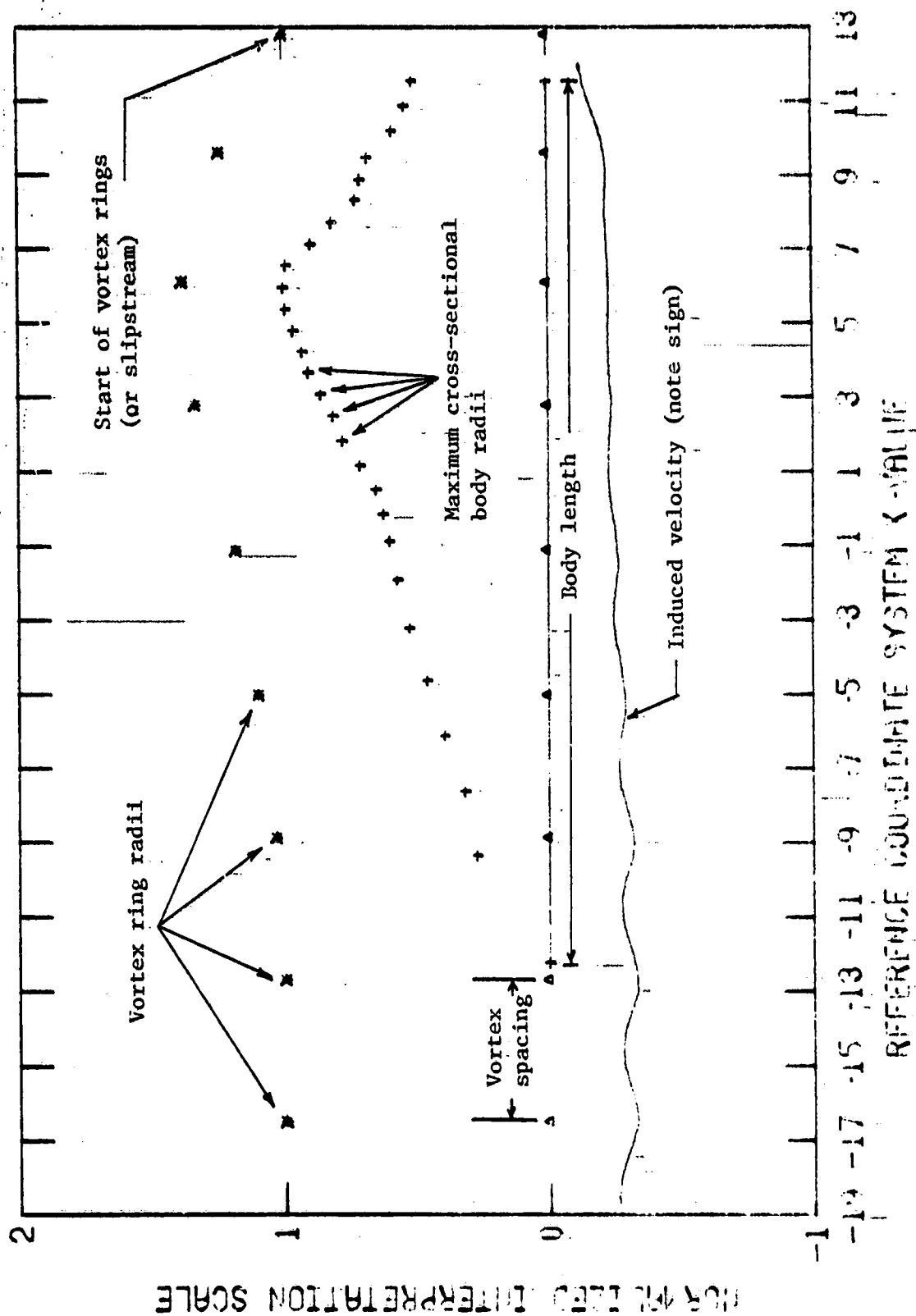


Figure 2: Typical plot of the location and radii of the vortex rings as well as the induced velocity of such an arrangement of rings

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CARD 6 (continued):

Columns	FORTRAN Name	Description
16-20	NODE	Control parameter--equal in value to the node or panel number in question--that generates additional output in that portion of the streamline calculation near the specified node or panel. NODE = 0 produces no additional output, while NODE = "panel number" does.

Parameter CF is a single-precision floating-point number in a F10 field.

Parameters ITEST and NODE are right-adjusted integer numbers in I5 fields.

CARD 7:

The number NQE of quadrilaterals or panels of the input half-body data:

Occupying columns 1-4 in an I4 field, NQE is a right-adjusted integer number determined by the product

$(\text{maximum MI} - 1) * (\text{maximum NI} - 1)$

where MI and NI are defined later. NQE should be restricted in value to approximately 600 because of the array dimensions in the program. The resulting of NQE is controlled by the read unit number IDS.

CARD 8: \*\* Ring Vortex Systems--Propeller Slipstream \*\*

Columns	FORTRAN Name	Description
1-5	NSRV	Number of independent ring-vortex systems. Normally NSRV = 1 or 0.
6-10	ISPACE	Generation parameter for ring vortices. If ISPACE = 0, no automatic generation and spacing of ring vortices are performed. If NSRV > 1, ISPACE must be equal to zero. If ISPACE > 0, NSRV is set equal to 1 and the program is permitted to generate a system of ring vortices.
11-20	XCRP(1)	The approximate vortex spacing along the x-axis before the x-position of maximum body diameter (ft).

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CARD 8 (continued):

Columns	FORTTRAN Name	Description
21-30	XCRP(2)	The approximate vortex spacing along the x-axis aft of the x-position of maximum body diameter (ft).  $X_i = X_{i-1} - XCRP(1) * EXP(-AEXP(1) * (R-RMX)/RMX)$ where $X_i, X_{i-1}$ = x-locations $R$ = body radius at $X_i$ $RMX$ = maximum body radius  for vortex spacing before the x-location of the maximum body diameter.
31-40	AEXP(1)	Factor in the exponential of the equation
41-50	AEXP(2)	Factor in the exponential of the equation  $X_i = X_{i-1} - XCRP(2) * EXP(-AEXP(2) * (R-RMX)/RMX)$ where $X_i, X_{i-1}$ = x-locations $R$ = body radius at $X_i$ $RMX$ = maximum body radius  for vortex spacing aft of the x-location of the maximum body diameter.
51-60	XRM	Limiting downstream x-location of the axially-spaced vortices (ft).

NSRV and ISPACE are right-adjusted integer numbers in I5 fields, while XCRP(1), XCRP(2), AEXP(1), AEXP(2) and XRM are single-precision floating-point numbers in F10 fields.

**\*\* Ring Vortex Parameters' Cards \*\***

Two cards are necessary to specify the information about the location and orientation of the starting vortex (or vortices) of a generated system of vortices or an individual independent ring vortex. It should be noted that if NSRV = 0,

no cards are specified under this section. If NSRV  $\neq$  0, the user must specify NSRV set(s) of these two cards in the order indicated in the section Circulation Variation Cards.

The first card contains

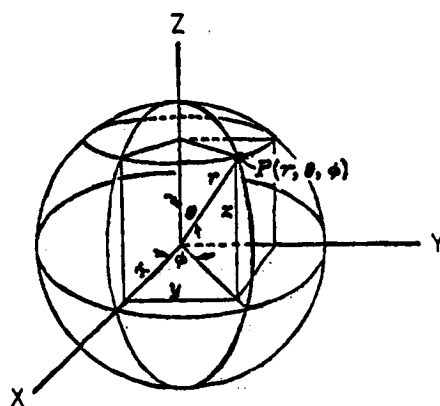
Columns	FORTTRAN Name	Description
1-10	XCV	x-coordinate of the center of the vortex ring (ft).
11-20	YCV	y-coordinate of the center of the vortex ring (ft).
21-30	ZCV	z-coordinate of the center of the vortex ring (ft).
31-40	RDM	Maximum vortex radius (ft).. RDM is usually considered to be the boundary of the propeller slipstream. If NSRV = 1, ISPACE > 0, and if XCV, YCV, and ZCV correspond to the propeller's center of rotation, RDM is the propeller radius.
41-50	CA	Initial central angle, degrees (See Figure 3).
51-60	PHI	Rotation angle, degrees (See Figure 3).
61-65	NCA	Central angle increment number. NCA is that number dividing 360 degrees into NCA equal parts from which NCA segments are determined to approximate the perimeter of a circle.
66-70	NVPHI	Rotation tilt parameter. NVPHI = 0: Plane of the vortex ring(s) is perpendicular to the x-axis of body (Set PHI = 90.0). NVPHI = 1: Plane of the vortex ring(s) is not perpendicular to the x-axis of the body. Parameter allows PHI to change at the same rate as CA so that initial choices of PHI and CA determine the path taken by point P of Figure 3.

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first card (continued):

Columns	FORTRAN Name	Description
71-75	NRS	Number of radial stations or concentric vortex rings.
76-80	NPTS	Number of (circulation vs. radial distance) points ( $\leq 50$ ).

The parameters XCV, YCV, ZCV, RDM, CA, and PHI are single-precision floating-point numbers in F10 fields. The parameters NCA, NVPHI, NRS, and NPTS are right-adjusted integer numbers in I5 fields.



$$CA = \theta$$

$$PHI = \phi$$

Figure 3: Definition of angles for specification of vortex ring(s) orientation (Point P described in Cartesian coordinates by  $x = r \sin \theta \cos \phi$ ,  $y = r \sin \theta \sin \phi$ , and  $z = r \cos \theta$ )

The second card contains

Columns	FORTRAN Name	Description
1-10	GFACT	The circulation-strength scale factor. If GFACT = 0.0, the program automatically sets GFACT = 1.0. Since an arbitrary normalized circulation variation may be specified that may not be compatible to the-specified DEP, GFACT provides an easy means to adjust power into the air-stream by changing the magnitude of the circulation variation. If IMATCH = 0, GFACT is automatically adjusted to match

second card (continued):

the simulated slipstream's power to the specified power into the air-stream. GFACT is a single-precision floating-point number in an F10 field.

**\*\* Circulation Variation Cards \*\***

For each independent vortex system, a set of NPTS cards must be specified in this section. Each card of the set contains

Columns	FORTTRAN Name	Description
1-10	RAD	The radius at which the circulation (or strength) of the vortex ring is to be specified (ft).
11-20	GAM	The circulation (or strength) of the vortex ring at radius RAD.

The parameters RAD and GAM are single-precision floating-point numbers in F10 fields.

Ordering of cards: For each of the NSRV vortex systems, the user must supply the two cards from the Ring-Vortex-Parameters section first and, secondly, the NPTS cards of this section. For every independent ring-vortex system, the user must repeat this sequence.

**\*\* Body Description Cards \*\***

Each card contains the information to specify one half-body point. Each card contains

Columns	FORTTRAN Name	Description
1-12	XI	x-coordinate
13-24	YI	y-coordinate
25-36	ZI	z-coordinate

Body Description Cards (continued):

Columns	FORTRAN Name	Description
37-40	NI	N-station index (See Figure 4)
41-44	MI	M-station index (See Figure 4)
45-48	NS	Body number

XI, VI and ZI are single-precision floating-point numbers in F12 fields, while NI, MI and NS are right-adjusted integer numbers in I4 fields. The maximum value of NI or MI must be restricted to less than or equal to 30 because of the array dimensions of the program. NS should be a constant for a given data set, which must be greater than zero but not equal to 1000. A blank card must be supplied at the end of these cards to signal the end of the body description cards. The reading of the body description cards is controlled by the read unit number IDS.

**\*\* Inlet and Exhaust Panel Cards \*\***

Each card contains the information to specify one panel or quadrilateral either as an inlet (flow into the body) panel or as an exhaust (flow out of the body) panel. Each card contains

Columns	FORTRAN Name	Description
1-5	MS1	1st reference M-station index [MS1 $\geq$ 1]
6-10	MS2	2nd reference M-station index [MS1 < MS2 $\leq$ max (MI)]
11-15	NS1	1st reference N-station index [NS1 $\geq$ 1]
16-20	NS2	2nd reference N-station index [NS1 < NS2 $\leq$ max (NI)]

Columns	FORTTRAN Name	Description
21-25	IPNS	Parameter which denotes the panel enclosed by the M- and N-station indexes as an inlet or exhaust panel. If IPNS = -1, the panel is designated as an inlet panel, while the panel is designated as an exhaust panel if IPNS = +1. If IPNS = 0, the panel is bypassed as being impermeable to mass flow.

The panels are designated by the order in which the data cards are encountered. It must be true--with the exception of a blank card--that

$$(MS2 - MS1) = 1$$

and

$$(NS2 - NS1) = 1$$

since only one panel specification is allowed per card. Since stagnation flows are not permitted in the program, at least one exhaust panel is required if at least one inlet panel is specified, and vice versa. MS1, MS2, NS1, NS2, and IPNS are right-adjusted integer numbers in I5 fields. A blank or zero card must be supplied to serve either of two purposes. If no inlet and exhaust panels are specified, the blank card terminates the attempt to read more cards. If inlet and exhaust panels are specified, the blank card signals the end of this information.

Specification of the cards above represent a complete set of data for a particular body. Additional data sets are programmed similarly starting again at CARD 1.



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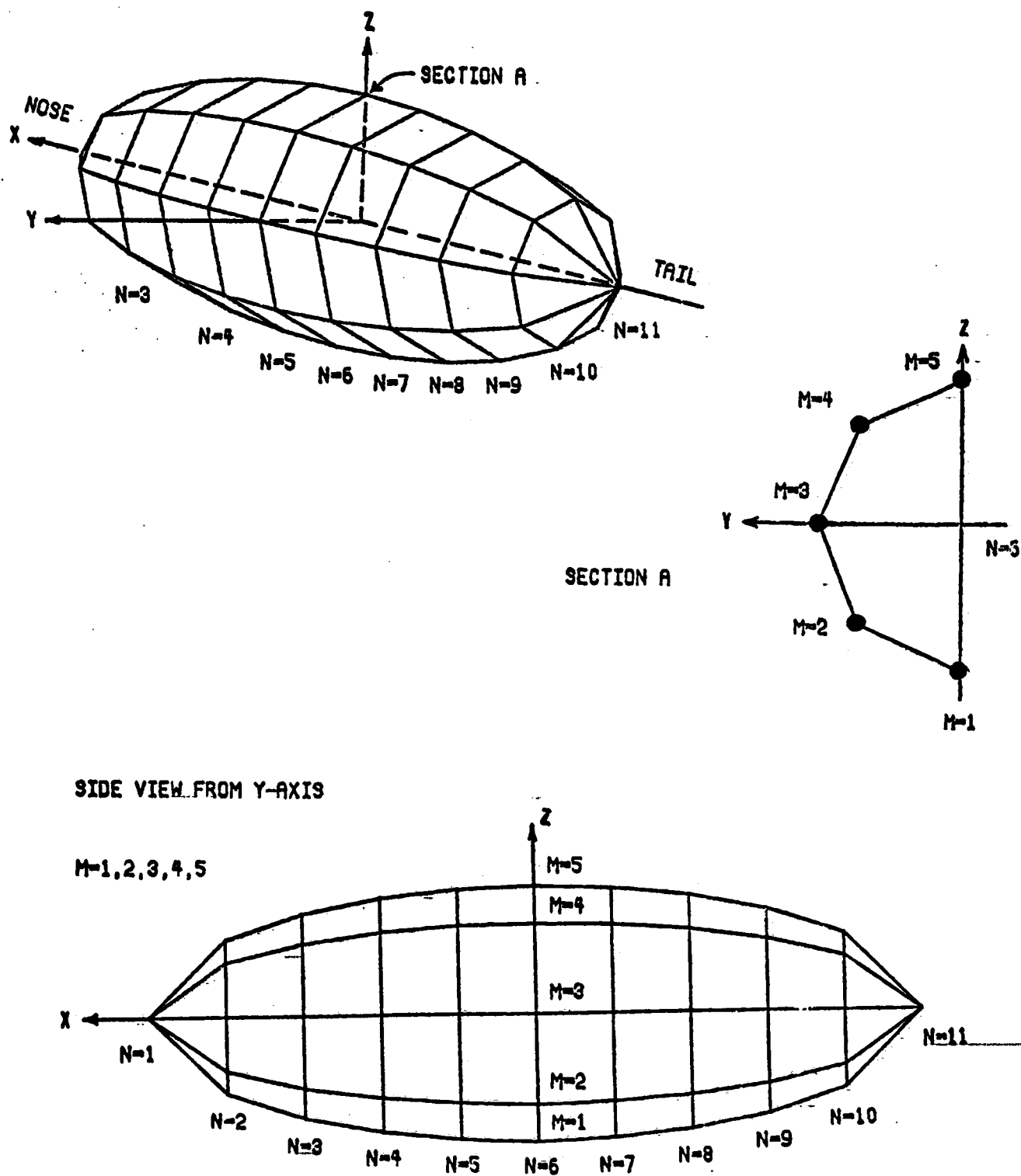


Figure 4: Schematic of indexing scheme

THE NCSU BODY PROGRAM  
F.O. SMETANA, ET AL  
NASA CR-2523  
N.C. STATE UNIVERSITY  
RALEIGH, NORTH CAROLINA 27650

ANY QUESTIONS CONCERNING THE USE OF THIS PROGRAM SHOULD BE  
DIRECTED TO STAN R. FOX OR F.O. SMETANA  
2404 AROUGHTON BLDG  
DEPT ME ENGRG. NCSU  
RALEIGH, N.C. 27650  
(919/737-2374)

```

DIMENSION INDEX(9,3),C(9,f),D(9),CZ(9),IP(9),XP(9),YP(9),ZP(9),X(C
150),Y(650),Z(650),ID(31,31),B(192),FF(9,1),BHOLD(192),XNEW(150),YN
1EW(150),ZNFW(150),XK(4),RK(4),IDD(650,4),IPT(4),XS(651),YS(651),ZS
1(651),XCV(40),YCV(40),ZCV(40),FDM(40),PHI(40),NCA(40),NVPHI
1(40),NFS(40),NPYS(40),PAD(50),GAM(50),SVV(31,2),XCPR(2),AEXP(2)
DIMENSION XORD(5,200),YORD(5,200),XDUM(5,200),YDUM(5,200),KIND(5)
EQUIVALENCE (XNEW(1),DELS(1)),(YNFW(1),CFI(1)),(ZNCW(1),JHT(1)),(C
17(1),D(1)),(D(1),FF(1,1))
COMMON TITLE(20),XCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AOP(650),BEFA,BERDD,NQUAD,IWRITE,NP,KNEW
COMMON /SPV/CIRCV(40)

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38 PF1
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78 PF1
79 PF1

COMMON /SIK/SN(650),VNP(650),IPN(650)
COMMON /RING/VTX(3,650)
COMMON /VCK/HVF,SFC,DEP,CPHA,TINF,ADUT,AIN,EOA
COMMON /BL/VOV(75),SS(75),VIN,V0,ROE,DELS(150),CFI(150),THT(150),
1STOTAL,KKK
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15
COMMON /CANCEL/ICANCL,NODE
INTEGER P,P1,P2,P3,P4,PC,P5,P6,P7,P8,P9

C***
SET CARRIAGE CONTROL PARAMETERS FOR INSTALLATION
JREAD=1
JPUNCH=2
JWRITE=3
KFILE1=7
KFILE2=8
KFILE3=9
KFILE4=10
KFILES=11
SET INITIAL PARAMETERS
PI=3.1415927
IPL0T=0
LINE=0
PXLIN=50
READ DATA CARDS
1 READ (JREAD,2, END=173) IDS
2 FORMAT (15)
ICANCL=0
READ (IDS,3) (TITLE(I),I=1,20)
3 FORMAT (20A4)
WRITE (JWRITE,4)
4 FORMAT (1H1,/,10X,105HNCSSU FLOWBODY PROGRAM: POTENTIAL FLOW + BD
1UNDARY LAYER + NONUNIFORM SLIPSTREAM FLOW + INTERIOR MASS FLOW.//)
1 KFILE=KFILE1
REWIND KFILE1
REWIND KFILE2
REWIND KFILE3
REWIND KFILE4
REWIND KFILE5
KNFW=1
ICK=3

```



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```

NPMAX=650
DO 13 LL=1,NPMAX
DC 13 I=1,3
13 VTX(I,LL)=0.0
C** READ NUMBER OF VORTEX SYSTEMS
14 READ (JRFAD,14) NSRV,ISPACE,XCRP(1),XCRP(2),AEXP(1),AEXP(2),XRM
FORMAT (2I5,5F10.0)
IF (NSRV.LE.0) ISPACE=0
IF (ISPACE.NE.0) NSRV=1
ISEE=0
IF (ISPACE.NE.0) ISEE=1
INSRV=NSRV
IF (NSRV.LE.0) GO TO 24
WRITE (JWRITE,15) NSRV,ISPACE,XCRP(1),AEXP(1),XCRP(2),AEXP(2),XRM
15 FCRMAT (1X,/,2X,12,27H VORTEX SYSTEM(S) SPECIFIED,/,31X,7H ISPACE=
1,12,/,31X,10H XCRP(1)=,F10.5,3X,8HAEXP(1)=,F10.5,/,31X,10H XCRP(
12)=,F10.5,3X,8HAEXP(2)=,F10.5,5X,4HXRM=,F10.5,/)
LINE=LINE+6
C** READ COORDINATES FOR VORTEX CENTER. MAXIMUM VORTEX RADIUS, THE
C** INITIAL CENTRAL ANGLE, ROTATION ANGLE, CENTRAL-ANGLE-INCREMENT
C** NUMBER, ROTATION TILT PARAMETER, NUMBER OF RADIAL STATIONS FOR
C** VORTEX SYSTEM, THE NUMBER OF POINTS OF CIRCULATION VS RADIAL
C** DISTANCE, AND THE CIRCULATION STRENGTH SCALE FACTOR
DO 23 LL=1,NSRV
READ (JPEAD,16) XCV(LL),YCV(LL),ZCV(LL),RDM(LL),CA(LL),PHI(LL),NCA
1(1),NVPHI(LL),NRS(LL),NPTS(LL),GFAC
16 FORMAT (6F10.0,4I5,/,F10.0)
IF (GFAC.EQ.0.0) GFAC=1.0
IF (RDM(LL).GT.0.0) GO TO 17
NRS(LL)=1
NPTS(LL)=0
ISEE=1
17 IF ((LINE+7).LE.MXLINE) GO TO 19
WRITE (JWRITE,19)
18 FCRMAT (1H1)
LINE=0
19 WRITE (JWRITE,23) LL,XCV(LL),YCV(LL),ZCV(LL),RDM(LL),CA(LL),PHI(LL
1),NCA(LL),NVPHI(LL),NRS(LL),NPTS(LL),GFAC
20 FORMAT (1X,/,FOR VORTEX SYSTEM:,12,/,4X,/,XCV=,F10.5,/, YCV=,F10.
15,/, ZCV=,F10.5,/,PDM=,F10.5,/, CA=,F10.5,/, PHI=,F10.5,/,
14X,NCA=,15,/, NVPHI=,15,/, NRS=,15,/, NPTS=,15,/,4X,GFAC=,
1F16.9,/)

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LINE=LINE+7
CA(LL)=CA(LL)*PI/180.0
PHI(LL)=PHI(LL)*PI/180.0
IF (NPTS(LL).EQ.0) GO TO 23
READ SPLINE POINTS FOR CIRCULATIONS
MNPTS=NPTS(LL)
DO 22 I=1,MNPTS
  READ (JREAD,21) RAD(I),GAM(I)
21 FCRMAT (2F10.0)
  GAM(I)=GAM(I)*GFACT
22 CONTINUE
CALL SPLINE (MNPTS,GAM,RAD,LL)
23 CONTINUE
24 K=0
  IF (NSRV.EQ.1) LMATCH=1
  XMIN=0.0
  XMAX=0.0
  MN=0
  P=1
  Q=1.0
  DO 25 I=1,31
    DC 25 J=1,31
    ID(I,J)=0
25 J=0
C** READ INPUT POINTS--AN ODD NUMBER MUST BE USED FOR BOTH NI AND MI
  READ (IDS,26) XI,YI,ZI,NI,MI,NS,NE,VN
26 FCRMAT (3F12.9,4I4,F12.9)
  MMAX=MI
  MMIN=MI
  NMAX=NI
  NMIN=NI
  NSS=NS
  PC=1
  GO TO 31
27 READ (IDS,26) XI,YI,ZI,NI,MI,NS,ME,VN
  GO TO 30
28 MI=MI+1
  IF (MI.LE.MMAX) GO TO 29
  NI=NI+1
  IF (NI.EQ.6) NS=J
  IF (NI.EQ.6) GO TO 35

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29 XI=XNEW(PC+1)
   YI=YNEW(PC+1)
   ZI=ZNEW(PC+1)
30 PC=PC+1
31 IF (NS.NE.NSS) GO TO 35
   IF (KNEW.EQ.1.AND.NE.EQ.0) GO TO 32
   IF (KNEW.NF.1.AND.NE.EQ.0) GO TO 33
   IW=NI
   NI=NI
   MI=IW
C** CONVERT BODY COORDINATES TO COMPATIBLE UNITS
32 XI=XI*CF
   YI=YI*CF
   ZI=ZI*CF
C** STORE INPUT POINTS IN POINT ARRAY
33 X(PC)=XI
   Y(PC)=YI
   Z(PC)=ZI
   IF (KNEW.NE.1) GO TO 34
   XS(PC)=X(PC)
   YS(PC)=Y(PC)
   ZS(PC)=Z(PC)
34 ID(MI,NI)=PC
   NMAX=MAXO(MMAX,MI)
   NMIN=MINO(MMIN,MI)
   NMAX=MAXO(NMAX,NI)
   NMIN=MINO(NMIN,NI)
   IF (XMIN.GE.XI) XMIN=XI
   IF (XMAX.LE.XI) XMAX=XI
   GO TO (27,28).KNEW
35 IF ((LINE+3).LE.NXLINF) GO TO 36
   WRITE (JWRITE,18)
   LINE=0
36 WRITE (JWRITE,37) NSS
37 FCFMAT (/10H0 SECTION ,I4)
   IF (IISF.EQ.0.OR.NSRV.EQ.0) GO TO 66
   PC=PC-1
C** DEFINE CENTERLINE OF BODY
   X21=X(PC)-X(1)
   Y21=Y(PC)-Y(1)
   Z21=Z(PC)-Z(1)
   BCDC=SQ2(X21,Y21,Z21)

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XDCS=X21/BCDC
YDCS=Y21/BCDC
ZDCS=Z21/BCDC
WRITE (JWRITE,33) XDCS,YDCS,ZDCS
28 FORMAT (1X,/,10X,35HBODY-CENTERLINE DIRECTION COSINES( ,F7.4,3H .
1 ,F7.4,3H , ,F7.4,2H ))
IF (1TEST.F0.0) GC TO 39
XGRD(2,1)=X(1)
XCRD(2,2)=X(PC)
YCRD(2,1)=0.0
YCRD(2,2)=0.0
KIND(2)=-1
KIND(3)=3
39 FOR EACH N-STATION, DETERMINE CROSS-SECTIONAL AREA AND MAX RADIUS
LPT=1
XMR=X(1)
RMR=0.0E0
MMAXM1=MMAX-1
LZF=0
DC 41 JN=NMIN,PMAX
LZF=LZF+1
X3=X(LPT)
XOPD(3,JN)=X3
Y3=Y(1)+(X3-X(1))*Y21/X21
Z3=Z(1)+(X3-X(1))*Z21/X21
AREAS=0.0E0
DC 40 JM=MMIN,MMAXM1
Y4=Y(LPT)
Z4=Z(LPT)
IF (JM.FG,MMIN) RMX=SQ2F(0.0,0.0,Y3,Y4,Z3,Z4)
Y5=Y(LPT+1)
Z5=Z(LPT+1)
AREAS=0.5E0*ABS(Y3*Z4+Z3*Y5+Z5*Y4-(Z4*Y5+Z3*Y4+Y3*Z5))
APFAS=APFAS+2.0E0*AREA
PMX1=SQ2F(0.0,0.0,Y3,Y5,Z3,Z5)
IF (PMX1.GT.RMX) RMX=PMX1
IF (PMX.LT.1.0E-06) RMX=0.0E0
IF (PMX.GT.RXMR) RXMR=RMX
IF (PMX.EQ.RXMR) XMR=X3
40 LPT=LPT+1
LPT=LPT+1
SVV(JN,1)=APFAS

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SVV(JN,2)=RMX
41 CONTINUE
  IROUND=0
  IF (ITEST.EQ.0) GO TO 43
  DO 42 JN=1,LZP
    YORD(3,JN)=SVV(JN,2)/RXMR
  42 YORD(3,JN)=SVV(JN,2)/RXMR
  43 IF (ISPACE.EQ.0) GO TO 45
  C** COMPUTE LOCATION OF VORTICES
  CALL SPACF(NSRV,SVV,XCV,NMIN,NMAX,X-MMAX,XCRP,AEXP,XRM,ISPACE,RXMR
    1,XMR)
  INSRV=NSRV
  DO 44 JV=2,NSRV
    NRS(JV)=1
    NPTS(JV)=0
    CA(JV)=CA(1)
    PHI(JV)=PHI(1)
    NCA(JV)=NCA(1)
    RDM(JV)=0.0
  44 NVPHI(JV)=NVPHI(1)
  45 IF ((LINE+25).LE.MXLINE) GO TO 46
  WRITE (JWRITE,19)
  LINE=0
  46 IF (LMATCH.NE.1) GO TO 47
  IF (IMATCH.FQ.0) GO TO 49
  47 WRITE (JWRITE,48)
  48 FCORMAT (1X,/,5X,24HRING VORTEX INFORMATION:,,.6X,6HNUMBER,9X,18H
    1,CENTER COORDINATES,8X,6HRAIDUS,3X,11HCIRCULATION,/,19X,1HX,9X,1HY,
    19X,1HZ,/)
  IROUND=1
  49 DO 60 JV=1,NSRV
    IF (JV.GT.1) GO TO 51
    COMPUTE A TOTAL CIRCULATION
    PDR=RDM(JV)
    NR=NRS(JV)
    GGDR=0.0
    DO 50 MV=1,NR
      RVX=F(NR,MV,PDR,DRX)/PDR
      GGDR=GGDR+G(JV,RVX)/RVX
    CIRC(JV)=GGDR
  50 CIRC(JV)=GGDR
  51 IF (RDM(JV).NE.0.0.AND.JV.NE.1.AND.IMATCH.NE.0) GO TO 60
  C** CENTER VORTEX IN BODY CENTERLINE
  X3=XCV(JV)

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IF (ITEST.EQ.0) GO TO 52
XCRD(1,JV)=XCV(JV)
YORD(1,JV)=0.0
KIND(1)=2
52 YCV(JV)=Y(1)+(X3-X(1))*Y21/X21
ZCV(JV)=Z(1)+(X3-X(1))*Z21/X21
IF (JV.EQ.1) GO TO 56
C** SCAN N-STATIONS FOR VORTEX LOCATION
LPT=1
NMAXM1=NMAX-1
DO 53 JN=NMIN,NMAXM1
LC1=JN
LC2=JN+1
IF (XCV(JV).LE.X(LPT).AND.XCV(JV).GE.X(LPT+MMAX)) GO TO 54
53 RDM(JV)=RDM(1)
GO TO 55
C** VORTEX LOCATED. DETERMINE RADIUS
54 RXTL=(X(LPT)-XCV(JV))/(X(LPT)-X(LPT+MMAX))
RDM(JV)=SVV(LC1,2)+RXTL*(SVV(LC2,2)-SVV(LC1,2))
RAV1=SQRT(SVV(LC1,1)/PI)
RAV2=SQRT(SVV(LC2,1)/PI)
RAV=RAV1+RXTL*(RAV2-PAV1)
RAVD=SQRT(PDR**2+RAV**2)
IF (RAVD.GT.RDM(JV))RDM(JV)=RAVD
55 CIRC(JV)=GGDR/(RDM(JV)/PDR)
56 IF (ITEST.EQ.0) GO TO 57
XORD(4,JV)=XCV(JV)
YORD(4,JV)=RDM(JV)/PDR
KIND(4)=6
57 IF (LMATCH.NE.1) GO TO 58
IF (IMATCH.EQ.0.AND.IFOUND.EQ.0) GO TO 60
58 WRITE (JWRITE,59) JV,XCV(JV),YCV(JV),ZCV(JV),RDM(JV),CIRC(JV)
59 FORMAT (8X,12.5X,F9.5,1X,F9.5,1X,F9.5,1X,F9.5,2X,F11.7)
60 CCNTINUE
IF (IROUND.EQ.1) GO TO 64
IROUND=1
CALL RGVRTX(XCV,YCV,ZCV,XCV(1),YCV(1),ZCV(1),RDM,NCA,CA,PHI,NVPHI,
1NRS,N'RV,VX,VY,VZ,IM,NPTS)
VI=SQ2(VX,VY,VZ)
IF (IMATCH.NF.0.OR.LMATCH.NE.1) GO TO 64
DELV=VINF*(1.0+VI)

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PNET=ROE*PI*(RDM(1)*VINFL)**2*DELV
GFACT=DFP/PNET
WRITE (JWRITE,61) VI
61 FORMAT (1X,/,5X,29HREFERENCE INDUCED VELOCITY = ,E16.9)
WRITE (JWRITE,62) GFACT
62 FORMAT (1X,/,5X,80HMATCHING OF AIRSTREAM POWER TO DEVELOPED ENGIN
1E POWER(DFP) REQUIRED GFACT TO BE ,E16.9,20H TIMES THE ORIGINAL.)
DC 63 I=1,MNPTS
63 GAM(I)=GAM(1)*GFACT
CALL SPLINE(MNPTS,GAM,RAD,1)
GO TO 47
64 WRITE (JWRITE,65)
65 FORMAT (1X,/)
IF (ITEST.EQ.0) GO TO 66
DETERMINE PARAMETERS FOR PLOT OF EXTENT OF VORTICES
XKEEP=ABS(X21)
XHOLD=ABS(XRM-X(1))
IF (XHOLD.GT.XKEEP) XKEEP=XHOLD
IKEEP1=FIX(X(X(1)+2.0))
IKEEP2=FIX(X(X(1)+2.0))
IF (((2*IKEEP1)/2).NE.IKEEP1) IKEEP1=IKEEP1+1
IF (((2*IKEEP2)/2).NE.IKEEP2) IKEEP2=IKEEP2+1
LTEST=IABS(IKEEP1)+IABS(IKEEP2)
XINC=2.0
XKEEP1=FLOAT(IKEEP1)
XKEEP2=FLOAT(IKEEP2)
IHL1=FIX(X(1))
IHL2=FIX(XKEEP)
XHLD=FLOAT(IHL1)+1.0
LL1=1
LL2=2*(IABS(IHL1)+IABS(IHL2))+1
GO TO 111
66 IF (IWRITE.GT.0) GO TO 68
C** SET LINE COUNTER
WRITE (JWRITE,13)
LINE=0
WRITE (JWRITE,67)
67 FORMAT (4H P.7X,2HX1,12X,2HX2,12X,2HX3,12X,2HX4,12X,2HXC,12X,2HX
1N,12X,1HA,13X,3HCZ4/4H N,7X,2HY1,12X,2HY2,12X,2HY3,12X,2HY4,12X,
12HXC,12X,2HYN,12X,2HFL,12X,3HCZ5/4H P,7X,2HZ1,12X,2HZ2,12X,2HZ3,
112X,2HZ4,12X,2HZC,12X,2HZN,12X,4HCZ1,10X,3HCZ6/)
LINE=LINE+5

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68 IF (KNEW.EQ.2) GO TO 69
   STCTAL=XMAX-XMIN
   PEBODY=Y-VINE*STOTAL/VO
69 MMAXQD=MMAX
   IF (KNEW.NE.1) GO TO 70
   NMX=NMAX+2
70 IDO=(MMAXQD-3)*(MMAXQD-1)/12
   N1=NMIN
   NM2=MMAX-MMIN
   NN2=NMAX-NMIN
   IF (MOD(MM2,2).EQ.0.AND.MOD(NN2,2).EQ.0) GO TO 71
   ISP=1
71 MM2=MM2/2
   NN2=NN2/2
   IF ((KNEW.EQ.1.AND.IPC1.EQ.0).OR.(KNEW.EQ.2.AND.IPC2.EQ.0)) GO TO 72
10 72
C** PUNCH CARDS FOR PLOTTING
CALL PUNCH(NMIN,NMX,MMIN,MMAX,XS,YS,ZS,JPUNCH,JWRITE)
C** DC LOOPS WHICH SWEEP POINT ARRAYS & SET UP PANEL GEOMETRY
72 DO 110 NN=1,NN2
   M1=MMIN
   DO 109 MM=1,MM2
   NQ=1
   IT=ID(M1,N1)*ID(M1+1,N1)*ID(M1+2,N1)*ID(M1,N1+1)*ID(M1+1,N1+1)*ID(
   M1+1,N1+2)*ID(M1,N1+2)*ID(M1+1,N1+2)
   IF (IT.EQ.0) GO TO 109
   M2=M1+1
   DO 108 M=M1,M2
   N2=N1+1
   DC 108 N=N1,N2
73 GO TO (73,74,75,76),NQ
   P1=ID(M,N)
   P2=ID(M+1,N)
   P3=ID(M+1,N+1)
   P4=ID(M,N+1)
   P5=ID(M+2,N)
   P6=ID(M+2,N+1)
   P7=ID(M+1,N+2)
   P8=ID(M,N+2)
   P9=P1
   IF ((X(P1).NE.X(P2).OF.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1

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1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
P9=ID(M+2,N+2)
GO TO 77
74 P1=ID(M,N+1)
P2=ID(M,N)
P3=ID(M+1,N)
P4=ID(M+1,N+1)
P5=ID(M,N-1)
P6=ID(M+1,N-1)
P7=ID(M+2,N)
P8=ID(M+2,N+1)
P9=P1
IF ((X(P1).NE.X(P2).OR.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1
1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
P9=ID(M+2,N-1)
GC TO 77
75 P1=ID(M+1,N)
P2=ID(M+1,N+1)
P3=ID(M,N+1)
P4=ID(M,N)
P5=ID(M+1,N+2)
P6=ID(M,N+2)
P7=ID(M-1,N+1)
P8=ID(M-1,N)
P9=P1
IF ((X(P1).NE.X(P2).OR.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1
1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
P9=ID(M-1,N+2)
GC TO 77
76 P1=ID(M+1,N+1)
P2=ID(M,N+1)
P3=ID(M,N)
P4=ID(M+1,N)
P5=ID(M-1,N+1)
P6=ID(M-1,N)
P7=ID(M,N-1)
P8=ID(M+1,N-1)
P9=P1
IF ((X(P1).NE.X(P2).OR.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1
1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
P9=ID(M-1,N-1)
77 IP(1)=P1

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IP(2)=P2
IP(3)=P3
IP(4)=P4
IP(5)=P5
IP(6)=P6
IP(7)=P7
IP(8)=P8
IP(9)=P9
C*** STORE CORNER POINTS TO PANEL NUMBER
      DC 78 JX=1.4
      78 IDD(P,JX)=IP(JX)
C*** COMPUTE NORMAL VECTOR TO PANEL (IN TERMS OF REFERENCE COORDINATE
C*** SYSTEM)
      X1=X(P3)-X(P1)
      X2=X(P4)-X(P2)
      Y1=Y(P3)-Y(P1)
      Y2=Y(P4)-Y(P2)
      Z1=Z(P3)-Z(P1)
      Z2=Z(P4)-Z(P2)
      XN=Y2*Z1-Y1*Z2
      YN=X1*Z2-X2*Z1
      ZN=X2*Y1-X1*Y2
      R=SQ2(XN.YN.ZN)
      XN=XN/R
      YN=YN/R
      ZN=ZN/R
      AQ=.5*R
C*** COMPUTE PANEL CENTROID (IN TERMS OF REFERENCE COORDINATE SYSTEM)
      X1=X(P3)-X(P2)
      Y1=Y(P3)-Y(P2)
      Z1=Z(P3)-Z(P2)
      X5=Y1*Z2-Y2*Z1
      Y5=Z1*X2-Z2*X1
      Z5=X1*Y2-X2*Y1
      A1=SQ2(X5.Y5.Z5)
      A2=R-A1
      IT=1
      XC=(X(P2)+X(P4)+(A1*X(P3)+A2*X(P1))/R)/3.
      YC=(Y(P2)+Y(P4)+(A1*Y(P3)+A2*Y(P1))/R)/3.
      ZC=(Z(P2)+Z(P4)+(A1*Z(P3)+A2*Z(P1))/R)/3.
      X4=YN*Z1-Y1*ZN
      Y4=ZN*X1-Z1*XN
      79
  
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Z4=XN*Y1-X1*YN
A=1./SQ2(X4.Y4.Z4)
X4=X4*A
Y4=Y4*A
Z4=Z4*A
X3=ZN*Y4-Z4*YN
Y3=XN*Z4-X4*ZN
Z3=YN*X4-Y4*ZN
C** COMPUTE POINTS IN QUAD SYSTEM (I.E.. ELEMENT COORDINATE SYSTEM)
DO 80 I=1,9
L=IP(I)
XP(I)=X3*(X(L)-XC)+Y3*(Y(L)-YC)+Z3*(Z(L)-ZC)
YP(I)=X4*(X(L)-XC)+Y4*(Y(L)-YC)+Z4*(Z(L)-ZC)
ZP(I)=XN*(X(L)-XC)+YN*(Y(L)-YC)+ZN*(Z(L)-ZC)
C** COMPUTE MATRIX COEFFICIENTS TO FIND LOCAL BODY SURFACE EQUATION
DO 81 I=2,9
C(I,1)=1.
C(I,2)=XP(I)
C(I,3)=YP(I)
C(I,4)=XP(I)**2
C(I,5)=YP(I)**2
C(I,6)=XP(I)*YP(I)
C(I,7)=ZP(I)
81 DO 82 I=1,6
C(I,1)=C(I,1)+C(I,7)
C(I,2)=C(I,2)+C(I,7)
C(I,3)=C(I,3)+C(I,7)
C(I,4)=C(I,4)+C(I,7)
C(I,5)=C(I,5)+C(I,7)
C(I,6)=C(I,6)+C(I,7)
82 D(I)=D(I)+C(I,7)
D(5)=D(5)+D(6)
D(6)=D(6)+D(8)
C** SOLVE MATRIX EQ. C*CZ=D FOR CZ
CALL MATINS(C,9,6,FF,6,1,DETERM,IDM,INDEX)
IF (IDM.EQ.1) GO TO (84,85).IT
WRITE (JWRITE,83)
83 FORMAT (33H ERROR IN INPUT - SINGULAR MATRIX)
LINE=LINE+1
ISP=1
GO TO 85
84 IT=2
C** COMPUTE NEW NORMAL VECTORS
XN=XN-CZ(2)*X3-CZ(3)*X4
YN=YN-CZ(2)*Y3-CZ(3)*Y4

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ZN=ZN-CZ(2)\*Z3-CZ(3)\*Z4  
A=1./SQ2(XN.YN.ZN)

XN=XN\*A  
YN=YN\*A  
ZN=ZN\*A

GO TO 79

C\*\* 85 STORE DATA IN ARRAY TO BE WRITTEN ON TAPE

B(J+1)=XP(1)  
B(J+2)=YP(1)  
B(J+3)=XP(2)  
B(J+4)=YP(2)  
B(J+5)=XP(3)  
B(J+6)=YP(3)  
B(J+7)=XP(4)  
B(J+8)=YP(4)  
B(J+9)=X3  
B(J+9)=Y3  
B(J+10)=Z3  
B(J+11)=X4  
B(J+12)=Y4  
B(J+13)=Z4  
XCP(K+1)=XC  
YCP(K+1)=YC  
ZCP(K+1)=ZC  
XNP(K+1)=XN  
YNP(K+1)=YN  
ZNP(K+1)=ZN  
AQP(K+1)=AQ

C\*\* COMPUTE QUADRUPOLE MOMENTS

XI1=XP(1)+XP(2)  
XI2=XP(1)+XP(4)  
XI3=XP(3)+XP(2)  
XI4=XP(3)+XP(4)  
XI5=XP(2)+XP(4)  
YI1=YP(1)+YP(2)  
YI2=YP(1)+YP(4)  
YI3=YP(3)+YP(2)  
YI4=YP(3)+YP(4)  
YI5=YP(2)+YP(4)  
R1=A1/24.  
R2=A2/24.  
R3=AQ/12.  
AXX=(XI1\*\*2+XI2\*\*2)\*R1+(XI3\*\*2+XI4\*\*2)\*R2+XI5\*\*2\*R3



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C**
AXY=(X11*Y11+X12*Y12)*R1+((X13*Y13+X14*Y14)*R2+X15*Y15)*R3
AVY=(Y11*Y12+Y12*Y13)*R1+((Y13*Y14+Y14*Y15)*R2+Y15*Y16)*R3
COMPUTE BODY SOLID ANGLE
X1=XC*X3+YC*Y3+ZC*Z3
Y1=XC*X4+YC*Y4+ZC*Z4
Z1=XC*XN+YC*YN+ZC*ZN
RD=1./SQ2(X1,Y1,Z1)
RCU=RD**3
RSV=RCU**2*RD
SA=SA+Z1*(AQ*RCU-((AXX*(Y1**2+Z1**2-4.*X1**2)+AVY*(X1**2+Z1**2-4.*
1Y1**2))*1.5-15.*X1*Y1*AXY)*RSV)
B(J+14)=AXX
B(J+15)=AXY
B(J+16)=AVY
BODY ERROR TESTS
D1=SQ2((XP(3)-XP(1))*(YP(3)-YP(1)).0.)
D2=SQ2((XP(4)-XP(2))*(YP(4)-YP(2)).0.)
FL=.5*AMAX1(D1,D2)
CZ23=ABS(CZ(2))+ABS(CZ(3))
IF (ABS(CZ(2))+ABS(CZ(3)).GT.FL*.001) GO TC 86
IF (ABS(CZ(1)).LT.FL*.3) GO TO 88
86 IF (IWRITE.GT.0) GO TO 88
WRITE (JWRITE.87) CZ23
87 FCRMAT (29H QUESTIONABLE PCINT -POOR FIT.6E14.3)
LINE=LINE+1
88 IF (XP(4).LT.XP(1)) GO TO 89
IF ((YP(4)-YP(3))*(YP(1)-YP(2)).GE.0.) GO TO 92
89 IF (IWRITE.GT.0) GO TO 91
WRITE (JWRITE.90) (XP(1),YP(1),I=1,4)
90 FCRMAT (30H ERROR IN INPUT - CROSSED QUAD.4(2F10.5.3X))
LINE=LINE+1
91 ISP=1
92 CRCF=SQ2((XP(2)-XP(1))*(YP(2)-YP(1)).0.)+XP(3)-XP(2)+SQ2((XP(1)-XP
1(4))*(YP(1)-YP(4)).0.)+SQ2((XP(4)-XP(3))*(YP(4)-YP(3)).0.)
IF (36.*AQ.GT.CRCF**2) GO TO 94
IF (IWRITE.GT.0) GO TO 104
LINE=LINE+1
WRITE (JWRITE.93)
93 FCRMAT (24H WARNING LONG THIN QUAD.)
94 IF (IWRITE.GT.0) GO TO 104
IF (Z1.GE.0.) GO TO 96
WRITE (JWRITE.95)

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95 FORMAT (35H QUESTIONABLE POINT - INWARD NORMAL)
   LINE=LINE+1
C*** EDIT QUADRILATERAL INFORMATION
96 GO TO (97,98,99,100),NO
97 WRITE (JWRITE,101) M,X(P1),X(P2),X(P3),X(P4),XC,XN,AQ,CZ(4),N,Y(P1)
   1),Y(P2),Y(P3),Y(P4),YC,YN,FL,CZ(5),P,Z(P1),Z(P2),Z(P3),Z(P4),ZC,ZN
   1,CZ(1),CZ(6)
   GO TO 102
98 WRITE (JWRITE,101) M,X(P2),X(P3),X(P4),X(P1),XC,XN,AQ,CZ(4),N,Y(P2)
   1),Y(P3),Y(P4),Y(P1),YC,YN,FL,CZ(5),P,Z(P2),Z(P3),Z(P4),ZC,ZN
   1,CZ(1),CZ(6)
   GO TO 102
99 WRITE (JWRITE,101) M,X(P4),X(P1),X(P2),X(P3),XC,XN,AQ,CZ(4),N,Y(P4)
   1),Y(P1),Y(P2),Y(P3),YC,YN,FL,CZ(5),P,Z(P4),Z(P1),Z(P2),Z(P3),ZC,ZN
   1,CZ(1),CZ(6)
   GO TO 102
100 WRITE (JWRITE,101) M,X(P3),X(P4),X(P1),X(P2),XC,XN,AQ,CZ(4),N,Y(P3)
   1),Y(P4),Y(P1),Y(P2),YC,YN,FL,CZ(5),P,Z(P3),Z(P4),Z(P1),Z(P2),ZC,ZN
   1,CZ(1),CZ(6)
101 FORMAT (1H,13,8E14.5/1X,13,8E14.5/1X,13,8E14.5/)
102 LINE=LINE+4
   IF (LINE.LT.MXLINE) GO TO 104
   WRITE (JWRITE,103)
103 FORMAT (4H1 M,7X,2HX1,12X,2HX2,12X,2HX3,12X,2HX4,12X,2HXC,12X,2HX
   1N,12X,1HA,13X,3HCZ4/4H N,7X,2HY1,12X,2HY2,12X,2HY3,12X,2HY4,12X,
   12HXC,12X,2HYN,12X,2HFL,12X,3HCZ5/4H P,7X,2HZ1,12X,2HZ2,12X,2HZ3,
   112X,2HZ4,12X,2HXC,12X,2HZN,12X,4HCZ1,10X,3HCZ6/)
   LINE=0
104 J=J+16
   IF (KNEW.NE.1.AND.P.LE.NOES) GO TO 105
C*** INITIALIZE ARRAYS
   VNP(P)=0.0
   IFN(P)=0
105 I=P
   P=P+1
   NC=NC+1
   K=K+1
C*** WRITE B ARRAY CONTAINING INFORMATION FOR 12 QUADRILATERALS
   IF (J.LT.102) GO TO 108
   IF (KNEW.EQ.1) KWRITE=KWRITE+1
   WRITE (KFILE)Q,(E(I),I=1,192)
   IF (KNEW.NF.1) GC TO 107

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IF (KWRITE.NE.IDO+1) GO TO 107
QHOLD=0
DC 106 I=1,192
106 BOLD(I)=B(I)
107 Q=P
J=0
108 CCNTINJE
109 M1=M1+2
110 N1=N1+2
111 IF (KNEW.NE.1) GC TO 129
IMESS=0
C** READ AND TEST M AND N STATIONS TO SPECIFY NCNZERO NORMAL VELOCITY
C** ON A QUADRILATERAL
112 READ (JREAD,113) MS1,MS2,NS1,NS2,IPNS
113 FCFORMAT (515)
IF (MS1.EQ.0.AND.IPNS.EQ.0) GO TO 129
IF (IPNS.EQ.0) GO TO 112
IF (((MS1.LF.0.OR.MS1.GT.MMAX).OR.(MS2.LE.0.OR.MS2.GT.MMAX)).OR.((
1)NS1.LE.0.OR.NS1.GT.NMAX).OR.(NS2.LE.0.OR.NS2.GT.NMAX)).OR.(MS2-MS1
1).NE.1.OR.(NS2-NS1).NE.1) GO TO 116
IF (IMESS.EQ.1) GO TO 115
WRITE (JWRITE,114)
114 FORMAT (1H1,///.5X,4HDESIGNATION OF NORMAL VELOCITY ON QUADRILATE
1)RALS,/)
LINE=6
115 IMESS=1
GC TO 118
116 WRITE (JWRITE,117) MS1,MS2,MMAX,NS1,NS2,NMAX
117 FORMAT (1X,/,10X,36HAN ERROR IN DATA INPUT HAS OCCURRED:/.15X,4HM
1)S1=,13.3X,4HMS2=,13.3X,5HMMAX=,13./,15X,4HNS1=,13.3X,4HNS2=,13.3X,
1)SHNMAX=,13./,10X,12HCALLING EXIT,/)
GC TO 172
118 MC=0
ICK=1
LC=0
C** LOCATE CORNER POINTS OF NONZERG-NORMAL-VELOCITY QUADRILATERAL
DC 120 NX=NM1N,NS2
DC 120 MX=MM1N,MMAX
LC=LC+1
IF ((NX.EQ.NS1.OR.NX.EQ.NS2).AND.(MX.EQ.MS1.OR.MX.EQ.MS2)) GO TO 1
119 GO TO 120

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119 MC=MC+1
    IPT(MC)=LC
    IF (NX.EQ.NS2.AND.MX.EQ.MS2) GO TO 121
120 CCNTINUE
C*** CORNER POINTS LOCATED. NOW FIND CORRESPONDING PANEL NUMBER
121 DC 124 JX=1,NQE
    NPL=JX
    LC=0
    DC 123 MX=1.4
    DO 122 NX=1.4
    IF (IPT(MX).EQ.IDD(JX,NX))LC=LC+1
122 CONTINUE
123 CONTINUE
    IF (LC.EQ.4) GO TO 125
124 CONTINUE
C*** PANEL NUMBER FOUND. STORE INDICATION OF NONZERO NORMAL VELOCITY
125 IPN(NPL)=IFNS
    IF (IPNS.LT.0) GO TO 127
    WRITE (JWRITE,126) MSI,MS2,NS1,NS2,NPL
126 FORMAT (2X,4(15.1X),2X,6HPANEL,14.2X,75HHAS BEEN DESIGNATED TO HA
1VE A NONZERO OUTWARD NORMAL COMPONENT OF VELCCITY.)
    LINE=LINE+1
    GO TO 112
127 WRITE (JWRITE,128) MSI,MS2,NS1,NS2,NPL
128 FORMAT (2X,4(15.1X),2X,6HPANEL,14.2X,74HHAS BEEN DESIGNATED TO HA
1VE A NONZERO INWARD NORMAL COMPONENT OF VELCCITY.)
    LINE=LINE+1
    GO TO 112
C*** SET UP FOR NEXT SECTION
129 IF (ITFST.NE.0) GO TO 150
    DC 130 M=MMIN,MMAX
    DO 130 N=MIN,NMAX
130 IC(M,N)=0
131 ASS=NS
    PC=1
    MMAX=MI
    VMIN=MI
    NMIN=NI
    NMAX=NI
    NE=ME
    IF (NS.GT.0) GO TO 31
    JHOLD=((NMAXQD-3)*(MMAXQD-1)-12*ID0)*16

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IF (J.EQ.192) GO TO 133
IF (KNEW.EQ.1) KWRITE=KWRITE+1
WRITE (KFILE) Q, (B(I), I=1, 192)
IF (KNEW.NE.1) GO TO 133
IF (KWRITE.NE.100+1) GO TO 133
QHOLD=Q
DO 132 I=1, 192
132 BHCLD(I)=B(I)
133 NP=K
NGUAD=NP
ISMP=ISMP+1
GO TO (137, 136, 135, 134), ISMP
134 SA=SA+SA
135 SA=SA+SA
136 SA=SA+SA
137 J=1
C*** CHECK SOLID ANGLE
IF (ABS(SA-12.566).LT..05) GO TO 138
IF (ABS(SA).LF..05) GO TO 140
138 WRITE (JWRITE, 139) SA
139 FORMAT (40HOPROBABLE ERROR IN INPUT - SOLIC ANGLE =, 2F12.3)
140 REWIND KFILE
C*** CHECK NO. OF QUADRILATERALS
IF (NP.FQ.NQE) GO TO 143
WRITE (JWRITE, 141) NP, NQE
141 FCRMAT (IX, I4.27H QUADRILATERALS GIVEN, NOT , I4)
142 FCRMAT (JWRITE, 142)
GO TO 172
143 IF (ISP.LE.3) GO TO 144
WRITE (JWRITE, 142)
GO TO 172
C*** CALL REMAINING SECTIONS OF THE POTENTIAL FLOW PROGRAM
144 CALL PFP2(ISM, K)
IF (ICANCL.NE.0) GO TO 172
NSRV=INSRV
145 IF (NSRV.LF.0) GO TO 158
LL1=1
LL2=NP
IF (KNEW.NE.2) GO TO 146
LL1=LL1S
LL2=LL2S

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146 IF (KNEW.EQ.1) WRITE (JWRITE,147)
147 FCRMAT (1H1,/,1X,67HINDUCED VELOCITY BY RING VORTICES AT ORIGINAL
1-BODY PANEL CENTROIDS:./)
IF (KNEW.EQ.2) WRITE (JWRITE,148)
148 FCRMAT (1H1,/,1X,63HINDUCED VELOCITY BY RING VORTICES AT WAKE-BOD
1V PANEL CENTROIDS:./)
WRITE (JWRITE,149)
149 FCRMAT (2X,5HPANEL,3X,10(.-),1X,23HPANEL CENTROID LOCATION,1X,11(
1.-),4X,12(.-),1X,19HVELOCITY COMPONENTS,1X,13(.-),/,1X,6HNUMBER
1,9X,1HX,15X,1HY,15X,1HZ,17X,1HX,15X,1HY,15X,1HZ,/)
LINE=0
GC TO 153
150 WRITE (JWRITE,151)
151 FCRMAT (1H1,/,1X,63HINDUCED VELOCITY BY RING VORTICES ALONG BODY-
1CENTERLINE POINTS:./)
WRITE (JWRITE,152)
152 FCRMAT (1X,5HPPOINT,3X,15(.-),1X,14HPPOINT LOCATION,1X,15(.-),4X,1
12(.-),1X,19HVELOCITY COMPONENTS,1X,13(.-),/,1X,6HNUMBER,9X,1HX,1
15X,1HY,15X,1HZ,17X,1HX,15X,1HY,15X,1HZ,/)
153 DC 157 LL=LL1,LL2
IF (ITEST.EQ.0) GO TO 154
FCR ITEST=1. SET AXIAL STATIONS FOR VORTEX INDUCED VELOCITIES
VCP(LL)=0.0
ZCP(LL)=0.0
IF (LL.EQ.1) XCP(LL)=XHLD
IF (LL.GT.1) XCP(LL)=XCP(LL-1)-0.5E0
XORD(5,LL)=XCP(LL)
C** COMPUTE INDUCED VELOCITY COMPONENTS AT PANEL CENTROIDS BY THE RING
C** VORTICES
154 CALL RGVRTX(XCV,YCV,ZCV,XCP(LL),YCP(LL),ZCP(LL),PDV,NCA,CA,PHI,NVP
1HI,NRS,NRSV,VX,VY,VZ,IM,NPTS)
VTX(1,LL)=VX
VTX(2,LL)=VY
VTX(3,LL)=VZ
IF (ITEST.NE.0) YCRD(5,LL)=VTX(1,LL)
IF ((LINE+1).LE.MXLINE) GO TO 155
WRITE (JWRITE,153)
IF (ITEST.EQ.0) WRITE (JWRITE,149)
IF (ITEST.NE.0) WRITE (JWRITE,152)
LINE=0
155 WRITE (JWRITE,156) LL,XCP(LL),YCP(LL),ZCP(LL),(VTX(1S,LL),1S=1,3)
156 FCRMAT (2X,14,3X,1H(,1PEI4.7,2H, .1PEI4.7,2H, .1PEI4.7,4H) .1PEI

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14.7.2X,1PE14.7,2X,1PE14.7)
LINE=LINE+1
157 CCONTINUE
C** IF (ITEST.EQ.0) GO TO 158
WARNING: THE FOLLOWING PLOT CARDS MAY BE INSTALLATION-DEPENDENT.
KIND(5)=-1
IPLOT=1
CALL PICSI(10,3,10,0)
CALL GRAFF(7.5,XKEEP1,XKEEP2,XINC,0,'REFERENCE COORDINATE SYSTEM X
1-VALUE,XORD,XDUM,5,0,-1,0,2,0,1,0,0,'NORMALIZED INTERPRETATION S
1CALE,YORD,YDUM,1,5,5,200,NSRV,2,NMAX,NSRV,LL2,KIND,1,0,0)
158 IF (ITEST.NE.0) GO TO 172
CALL PFP3(EPS,MIX)
CALL PFP4(CDPA,CDPA,ICK)
C** COMPUTE INTERIOR PRESSURE COEFFICIENT AND NORMAL VELOCITIES
IF (ICK.EQ.1) CALL VINOUT(JWRITE,VINF,ROE,NQE,VI)
IF (ICANCL.NE.0) GO TO 172
NSRV=0
ICK=ICK+1
IF (ICK.FQ.2) GO TO 145
IF (KNEW.NE.2) GO TO 160
C** ON SECOND PASS THROUGH COMPUTE LIFT & DRAG COEFFICIENTS
CL=CLPA/REFA
CD=(CDPA+CDFA)/REFA
WRITE (JWRITE,159) CL,CD,REFA,REBODY,STOTAL
159 FFORMAT (///,31X,23HTOTAL BODY COEFFICIENTS///,28X,29(1H*))/30X,16H
1TOTAL BODY CL = ,F11.5,/30X,16HTOTAL BODY CD = ,F11.5,/29X,17HREFE
1RENCE APEA = ,F11.5,/28X,18HREYNOLDS NUMBER = ,E11.4,/32X,14HBODY
1LENGTH = ,F11.5,/28X,29(1H*))/
GO TO 172
160 CALL PFP5(MMAXQD,NMAXQD,AREAAV,AVDELS,AVXCG,CDFA)
IF (ICANCL.NE.0) GO TO 172
C** REMAINING CARDS COMPUTE NECESSARY INFORMATION FOR WAKE-BODY
KNEW=2
NOFS=NQF
NI=1
NI=1
NS=1000
K=(NMAXQD-3)*(MMAXQD-1)
NF=3
NQE=NQE+2*(MMAXQD-1)
LL1S=K

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LL2S=NQE
REWIND KFILE1
DC 161 I=1,IDO
READ (KFILE1)Q,(B(IJK),IJK=1,192)
WRITE (KFILE2)Q,(B(IJK),IJK=1,192)
161 CONTINUE
KFILE=KFILE2
J=JHOLD
IF (J.EQ.0) GO TO 163
DO 162 I=1,J
B(I)=BHOLD(I)
162 Q=QHOLD
163 JP=JHOLD/16
QADD=QHOLD+.5
P=QADD+JP
I=ISTART+(NMAXQD-3)*MMAXQD
IST=ISTART+MMAXQD
XHOLD1=X(ISTART+1)
XHOLD2=X(IST+1)
Y REFERENCE LINE MUST BE 0.0
C**
ZAV=0.0
DC 164 I=1,MMAXQD
XNEW(I)=X(ISTART+1)
YNEW(I)=Y(ISTART+1)
ZNEW(I)=Z(ISTART+1)
ZAV=ZAV+ZNEW(I)
164 THETA=-90.0*3.14159/180.0
ZAV=ZAV/MMAXQD
RAV=0.0
DC 165 I=1,MMAXQD
PNEW=SQRT((YNEW(I))**2+(ZNEW(I)-ZAV)**2)
PAV=RAV+RNEW
165 RAV=RAV/MMAXQD
FAC=(AVXCG-XHOLD1)/(XHOLD2-XHOLD1)
AVSLOP=0.0
DO 166 I=1,MMAXQD
YCG=YNEW(I)-(YNEW(I)-Y(IST+1))*FAC
ZCG=ZNEW(I)-(ZNEW(I)-Z(IST+1))*FAC
P1=SQRT((YNEW(I))**2+(ZNEW(I)-ZAV)**2)
R2=SQRT((YCG)**2+(ZCG-ZAV)**2)+2.0*AVDELS
SLOPF=(R2-R1)/(XHOLD1-AVXCG)
166 AVSLOP=AVSLOP+SLOPE

```



```

C**      AVSLOP=AVSLOP/MMAXQD
        AREAT=4.0*AREAAV*2.0*MMAXQD
        XINF=XHOLD1-AREAT/(3.14159*RAV)
        CHECK TO MAKE SURE BODY SLOPE IS DECREASING
        IF (AVSLOP-GE.0.)AVSLOP=-ABS(RAV/(XINF-XHOLD1))
        WRITE (JWRITE,167) AVSLOP,AREAAV,AVXCG,XINF
167      FORMAT (1H1/50X.24HBEGIN WAKE BODY GEOMETRY//,.17H AVERAGE SLOPE =
        .1 .F8.5.3X.22H AVERAGE PANEL AREA = .F8.5.3X.22H AVERAGE X-CENTROID
        .1 = .F10.5.3X.20H END OF BODY AT X = .F10.5)
        DELTAZ=.01
        KK=1
        XX1=XHOLD1
        ZZ2=0.0
        RR1=RAV
168      ZZ2=ZZ2+DELTAZ
        XX2=ZZ2*(XINF-XHOLD1)+XHOLD1
        RR2=RAV*EXP(AVSLOP*ZZ2)*(1.0-ZZ2)
        DTETA=3.14159/(MMAXQD-1)
        AREA2=((RR2+RR1)*SIN(DTETA/2.0)*SQRT((RR2-RR1)**2+(XX2-XX1)**2)
        IF (AREA2-LT.AREAAV) GO TO 168
        XK(KK)=XX2
        RK(KK)=RR2
        XX1=XX2
        RR1=RR2
        KK=KK+1
        IF (KK-GE.4) GO TO 169
169      XK(4)=XINF
        RK(4)=0.0
        X1=XK(1)
        X2=XK(2)
        X3=XK(3)
        X4=XK(4)
        R1=RK(1)
        R2=RK(2)
        R3=RK(3)
        R4=RK(4)
        NSTRT1=MMAXQD
        NSTRT2=2*MMAXQD
        NSTRT3=3*MMAXQD
        NSTRT4=4*MMAXQD
        YFAC=(-Y(1))/(XINF-XHOLD1)

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PF11037

SQ2 1  
SQ2 2  
SQ2 3  
SQ2 4  
SQ2 5

```

ZFAC=(ZAV-Z(1))/(XINF-XHOLD1)
DO 170 I=1,MMAXQD
  CCSTHT=CCS(THETA)
  SINHT=SSIN(THETA)
  XNEW(NSRT1+1)=X1
  XNEW(NSRT2+1)=X2
  XNEW(NSRT3+1)=X3
  XNEW(NSRT4+1)=X4
  XNEW(NSRT1+1)=R1*CCSTHT-(XNEW(NSRT1+1))-XHOLD1)*YFAC
  XNEW(NSRT2+1)=R2*CCSTHT-(XNEW(NSRT2+1))-XHOLD1)*YFAC
  XNEW(NSRT3+1)=R3*CCSTHT-(XNEW(NSRT3+1))-XHOLD1)*YFAC
  XNEW(NSRT4+1)=R4*CCSTHT-(XNEW(NSRT4+1))-XHOLD1)*YFAC
  ZNEW(NSRT1+1)=R1*SINHT+ZAV-(XNEW(NSRT1+1))-XHOLD1)*ZFAC
  ZNEW(NSRT2+1)=R2*SINHT+ZAV-(XNEW(NSRT2+1))-XHOLD1)*ZFAC
  ZNEW(NSRT3+1)=R3*SINHT+ZAV-(XNEW(NSRT3+1))-XHOLD1)*ZFAC
  ZNEW(NSRT4+1)=R4*SINHT+ZAV-(XNEW(NSRT4+1))-XHOLD1)*ZFAC
  THETA=THETA+DTHETA
170 STCRE COORDINATES FOR PUNCHING
C** KPI=5*MMAXQD
DO 171 I=1,KPI
  XS(I*START+1)=XNEW(I)
  YS(I*START+1)=YNEW(I)
  ZS(I*START+1)=ZNEW(I)
  XI=XNEW(I)
  YI=YNEW(I)
  ZI=ZNEW(I)
GO TO 131
C** PREPARE FOR NEXT DATA SET
172 IF (IDS.NE.JREAD) REWIND IDS
GO TO 1
C** WARNING: THE FOLLOWING PLOT CARD MAY BE INSTALLATION-DEPENDENT.
173 IF (IPLT.NF.0) CALL PICSIZ(0.0,0.0)
STOP
END

```

```

FUNCTION SQ2(X,Y,Z)
C
C** FUNCTION SQ2 CALCULATES THE SQUARE ROOT OF R**2
C
RS=X**2+Y**2+Z**2

```

```

SQ2=SQRT(RS)
RETURN
END

SUBROUTINE MATINS(A,NR,N1,B,NC,M1,DETERM,ID,INDEX)
MIN 1
MIN 2
MIN 3
MIN 4
MIN 5
MIN 6
MIN 7
MIN 8
MIN 9
MIN 10
MIN 11
MIN 12
MIN 13
MIN 14
MIN 15
MIN 16
MIN 17
MIN 18
MIN 19
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MIN 29
MIN 30
MIN 31
MIN 32
MIN 33
MIN 34
MIN 35
MIN 36

MATRIX INVERSION(PIVOT METHOD) WITH SIMULTANEOUS EQUATION SOLUTION
INPUT A(NR,NR),B(NR,NC),& INDEX(NR,3)--NR,NC ARE ARRAY DIMENSIONS.
DEFINITIONS: N1--THE ORDER OF A, M1--THE NUMBER OF COLUMN VECTORS IN
B(MAY BE 0), DETERM--CONTAINS DETERMINANT ON EXIT, INDEX--WORK ARRAY
ID-(ID=2--SINGULAR MATRIX,ID=1--SUCCESSFUL INVERSION), A--THE INPUT
MATRIX WHICH IS REPLACED BY A INVERSE, B--COLUMN VECTORS WHICH IS
REPLACED BY CORRESPONDING SOLUTION VECTORS.

DIMENSION A(9,6),B(9,1),INDEX(9,3)
EQUIVALENCE (IROW,JROW),(ICOL,JCOL),(AMAX,T,SWAP)

INITIALIZATION
N=N1
M=M1
DETERM=1.0
DO 1 J=1,N
1 INDEX(J,3)=0
DO 20 I=1,N
SEARCH FOR PIVOT ELEMENT
AMAX=0.0
DO 6 J=1,N
IF (INDEX(J,3)-1) 2,6,2
2 DC 5 K=1,N
IF (INDEX(K,3)-1) 3,5,26
3 IF (AMAX-ABS(A(J,K))) 4,5,5
4 IROW=J
ICOL=K
AMAX=ABS(A(J,K))
5 CONTINUE
6 INDEX(ICOL,3)=INDEX(ICOL,3)+1
INDEX(I,1)=IROW
INDEX(I,2)=ICOL
INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL

```

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78 MIN

```

7 IF (IROW-ICOL) 7,11,7
  DETERM=-DETERM
  DO 8 L=1,N
    SWAP=A(IROW,L)
    A(IROW,L)=A(ICOL,L)
    A(ICOL,L)=SWAP
  8 IF (M) 11,11,9
  9 DO 10 L=1,M
    SWAP=B(IROW,L)
    B(IROW,L)=B(ICOL,L)
  10 B(ICOL,L)=SWAP
  11 DIVIDE PIVOT ROW BY PIVOT ELEMENT
  12 PIVOT=A(ICOL,ICOL)
  13 DETERM=DETERM*PIVOT
  14 A(ICOL,ICOL)=1.0
  15 DO 12 L=1,N
    A(ICOL,L)=A(ICOL,L)/PIVOT
  16 IF (M) 15,15,13
  17 DO 14 L=1,M
    B(ICOL,L)=B(ICOL,L)/PIVOT
  18 B(ICOL,L)=B(ICOL,L)/PIVOT
  19 REDUCE NON-PIVOT ROWS
  20 DO 20 L=1,N
    IF (L1-ICOL) 16,20,16
  21 T=A(L1,ICOL)
  22 A(L1,ICOL)=0.0
  23 A(L1,L)=A(L1,L)-A(ICOL,L)*T
  24 IF (M) 20,20,19
  25 DO 19 L=1,M
    B(L1,L)=B(L1,L)-B(ICOL,L)*T
  26 CONTINUE
  27 INTERCHANGE COLUMNS
  28 DO 23 I=1,N
    L=N+1-I
  29 IF (INDEX(L,1)-INDEX(L,2)) 21,23,21
  30 JROW=INDEX(L,1)
  31 JCOL=INDEX(L,2)
  32 DO 22 K=1,N
    SWAP=A(K,JROW)
    A(K,JROW)=A(K,JCOL)
    A(K,JCOL)=SWAP
  33 CC CONTINUE

```

MIN	MIN	MIN	MIN	MIN	MIN	MIN	MIN
79	80	81	82	83	84	85	86
87							

[illegible]

```

23 CCNTINUE
   DO 24 K=1,N
   IF (INDEX(K,3)-1) 26,24,26
24 CONTINUE
   ID=1
25 RETURN
26 ID=2
   GC TO 25
   END

```

SUBROUTINE PFP2(ISM,KM)

```

C***
C***
C
SUBROUTINE PPF2 CALCULATES THE INDUCED VELOCITIES OF EACH QUAD-
RILATERAL ON EVERY OTHER QUADRILATERAL

DIMENSION B(193),V1(1000),C1(900),VX(8),VY(8),VZ(8)
EQUIVALENCE (V3,Y2)
COMMON TITLE(20),XCP(650),YCP(650),ZCP(650),XNP(650),ZNP(
1650),AQP(650),REFA,REBODY,NQUAD,IWRITE,NP,KNEW
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15

```

15 COMMON /SIK/SN(650),VNP(650),IPN(650)  
COMMON /CANCEL/ICANCEL,NODE

```

      BLK=1.0
      IDW=0
      READ FIRST BLOCK OF B ARRAY
C***
      READ (KFILE)(B(I),I=1,193)

```

```

K=1
J=1
P=1
JC=1
JV=2
KMM=5*((NP+4)/5)+1
START LCOP OVER QUADRILATERALS
IF (B(1)-P) 68,3,68
3 J=2
C** 3 CHOOSE QUADRILATERAL AS REFERENCE POINT
C** 4 X1=B(J)
Y1=B(J+1)

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C***      ZNQ=ZNP(1)
C***      COMPUTE DISTANCE BETWEEN CENTROID OF REFERENCE QUADRILATERAL AND
C***      CENTROID OF ANOTHER QUADRILATERAL
26      RPQ=SQ2F(XC,XCQ,YC,YCQ,ZC,ZCQ)
C***      IF (RPQ-ST#4) 27,27,39
C***      TRANSFORM POINT FROM REFERENCE COORDINATE SYSTEM TO ELEMENT(QUAD)
C***      COORDINATE SYSTEM
27      X=(XCQ-XC)*XX+(YCQ-YC)*YX+(ZCQ-ZC)*ZX
          Y=(XCQ-XC)*XY+(YCQ-YC)*YY+(ZCQ-ZC)*ZY
          Z=(XCQ-XC)*XN+(YCQ-YC)*YN+(ZCQ-ZC)*ZN
          IF (RPQ-ST#2,0) 28,28,37
C***      COMPUTE VELOCITY COEFFICIENTS BY EXACT METHOD (QUAD SYSTEM)
28      R1=SQ2F(X,X1,Y,Y1,Z,0.)
          R2=SQ2F(X,X2,Y,Y2,Z,0.)
          R3=SQ2F(X,X3,Y,Y3,Z,0.)
          R4=SQ2F(X,X4,Y,Y4,Z,0.)
          IF ((R1+R2).LE.D12) GO TO 75
          IF ((R2+R3).LE.D23) GO TO 75
          IF ((R3+R4).LE.D34) GO TO 75
          IF ((R4+R1).LE.D41) GO TO 75
          CLA1=ALOG((R1+R2-D12)/(R1+R2+D12))
          CLA2=ALOG((R2+R3-D23)/(R2+R3+D23))
          CLA3=ALOG((R3+R4-D34)/(R3+R4+D34))
          CLA4=ALOG((R4+R1-D41)/(R4+R1+D41))
          TVX=CY12*CLA1+CY23*CLA2+CY34*CLA3+CY41*CLA4
          TVY=CX12*CLA1+CX23*CLA2+CX34*CLA3+CX41*CLA4
          TVZ=0.
          IF (ABS(Z/ST)-.010) 38,29,29
29      ZSQ=Z**2
          E1=ZSQ+(X-X1)**2
          E2=ZSQ+(X-X2)**2
          E3=ZSQ+(X-X3)**2
          E4=ZSQ+(X-X4)**2
          H1=(Y-Y1)*(X-X1)
          H2=(Y-Y2)*(X-X2)
          H3=(Y-Y3)*(X-X3)
          H4=(Y-Y4)*(X-X4)
          IF (CI12) 30,30,31
30      WS1=(CM12*FI-H1)/(Z*R1)
          WS2=(CM12*E2-H2)/(Z*R2)
          TV7=ATAN(WS1)-ATAN(WS2)
31      IF (CI23) 32,32,33

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32 TVZ=TVZ+ATAN((CM23*E2-H2)/(Z*R2))-ATAN((CM23*E3-H3)/(Z*R3))
33 IF (CI34) 34,34,35
34 TVZ=TVZ+ATAN((CM24*E3-H3)/(Z*R3))-ATAN((CM24*E4-H4)/(Z*R4))
35 IF (CI41) 36,36,38
36 TVZ=TVZ+ATAN((CM41*E4-H4)/(Z*R4))-ATAN((CM41*E1-H1)/(Z*R1))
GO TO 38
C*** COMPUTE VELOCITY COEFFICIENTS BY QUADRAPOLE METHOD (QUAD SYSTEM)
37 RPQ3=RPQ**3
RPQ7=(RPQ3**2)*RPQ
WS1=X/RPQ3
XSQ=X**2
YSQ=Y**2
ZSQ=Z**2
PS=YSQ+ZSQ-4.*XSQ
QS=XSQ+ZSQ-4.*YSQ
WS2=X*(9.*PS+30.*XSQ)/RPQ7
WS3=3.*Y*PS/RPQ7
WS4=3.*X*QS/RPQ7
TVX=A*WS1-CIXY*WS3-CIXX*WS2-CIYY*WS4
WS1=Y/RPQ3
WS2=Y*(9.*QS+30.*YSQ)/RPQ7
TVY=A*WS1-CIXX*WS3-CIXY*WS4-CIYY*WS2
TVZ=Z*(1/RPQ3-3.*(CIXX*PS-5.*CIXY*X*Y+CIYY*GS)/RPQ7)
TRANSFORM FROM ELEMENT TO REFERENCE COORDINATE SYSTEM
38 VX(1S)=TVX*XX+TVY*XY+TVZ*XN
VY(1S)=TVX*YX+TVY*YY+TVZ*YN
VZ(1S)=TVX*ZX+TVY*ZY+TVZ*ZN
GO TO 40
C*** COMPUTE VELOCITY COEFFICIENTS BY MONOPOLE METHOD (DIRECTLY IN THE
C*** REFERENCE COORDINATE SYSTEM)
39 ARPQ3=A/(RPQ**3)
VX(1S)=(XCQ-XC)*ARPQ3
VY(1S)=(YCQ-YC)*ARPQ3
VZ(1S)=(ZCQ-ZC)*ARPQ3
C*** REFLECT CENTROID POINT IN PLANE OF SYMMETRY
40 GO TO (41,43,45,46,48,49,50,51),IS
C*** DC LOOPS SET UP TO FORCE USE OF INDEX REGISTERS
41 J1=JV
J2=JC
V1(J1)=VX(1)
V1(J1+1)=VY(1)
V1(J1+2)=VZ(1)

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IF (ISM) 54.54.42
  42 IS=2
  C** XZ SYMMETRY
  YCQ=-YCQ
  GO TO 26
  43 IF (ISM-1) 53.53.44
  C** XY SYMMETRY
  IS=3
  ZCQ=-ZCQ
  GO TO 26
  45 IS=4
  YCQ=-YCQ
  GO TO 26
  46 IF (ISM-2) 52.52.47
  C** YZ SYMMETRY
  IS=5
  XCQ=-XCQ
  GO TO 26
  48 IS=6
  YCQ=-YCQ
  GO TO 26
  49 IS=7
  ZCQ=-ZCQ
  GO TO 26
  50 IS=8
  YCQ=-YCQ
  GO TO 26
  C** ADD CONTRIBUTIONS OF ALL REFLECTIONS TO OBTAIN NET INDUCED
  C** VELOCITY COMPONENTS IN REFERENCE COORDINATE SYSTEM
  51 V1(J1)=V1(J1)+VX(8)+VX(7)+VX(6)+VX(5)
  V1(J1+1)=V1(J1+1)-VY(8)+VY(7)+VY(6)-VY(5)
  V1(J1+2)=V1(J1+2)-VZ(8)+VZ(7)+VZ(6)+VZ(5)
  52 V1(J1)=V1(J1)+VX(4)+VX(3)
  V1(J1+1)=V1(J1+1)+VY(4)-VY(3)
  V1(J1+2)=V1(J1+2)-VZ(4)-VZ(3)
  53 V1(J1)=V1(J1)+VX(2)
  V1(J1+1)=V1(J1+1)-VY(2)
  V1(J1+2)=V1(J1+2)+VZ(2)
  C** CALCULATE THE NORMAL VELOCITY INDUCED AT THE CONTROL POINT OF THE
  C** 1-TH ELEMENT BY A UNIT SOURCE DENSITY ON THE J-TH ELEMENT (STORED
  C** BY COLUMNS)
  54 C1(J2)=XNQ*V1(J1)+YNQ*V1(J1+1)+ZNQ*V1(J1+2)

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55  JV=JV+3
    JC=JC+1
    C**  WRITE COEFFICIENTS ON TAPE
        IF (JV-1001) 61.56,56
56  JV=2
    V1(1)=BLK
    IF (BLK-636.0) 57.58,59
57  WRITE (KFILE3)BLK,V1
    GO TO 60
58  REWIND KFILE3
59  WRITE (KFILE5)BLK,V1
60  BLK=BLK+1.
61  IF (JC-901) 63.62,62
62  IDW=IDW+1
    WRITE (KFILE4)IDW,C1
    JC=1
63  KO=KQ+1
    L=L+1
    C**  END OF LOOP OVER CENTROIDS
        IF (KO-KM) 25.25,64
64  C1(JC)=0
65  P=P+1
    IF (KO-KMM) 55.65,65
    K=K+1
    J=J+16
    IF (K-KM) 66.66,70
    C**  FND OF LOOP OVER QUADRILATERALS
    C**  READ NEXT BLOCK OF B ARRAY IF NEEDED
66  IF (J-193) 4.67,67
67  READ (KFILE)(B(I),I=1,193)
    J=2
    IF (B(1)-P) 68.4.68
68  WRITE (JWRITE,69) B(1),P
69  FORMAT (28H0 POINTS OUT OF ORDER B(1)=,1F4.0,4H P=,1F4.0)
    ICANCL=1
    RETURN
70  IF (BLK-636.0) 71.72,73
    C**  WRITE REMAINING COEFFICIENTS ON TAPE
71  WRITE (KFILE3)BLK,V1
    REWIND KFILE3
    GO TO 74
72  REWIND KFILE3

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73 WRITE (KFILES)BLK.V1
  REWIND KFILES
74 WRITE (KFILES4)IDW.C1
  REWIND KFILES4
  REWIND KFILE
  GO TO 77
75 WRITE (JWRITE,76) L,P
76 FORMAT (3H L=.15.20X,3H P=.F5.1)
77 RETURN
  END

```

```

C***
C      FUNCTION SQ2F(X1,X2,Y1,Y2,Z1,Z2)
C
      FUNCTION SQ2F CALCULATES THE DISTANCE BETWEEN TWO POINTS
      X=X1-X2
      Y=Y1-Y2
      Z=Z1-Z2
      RS=Z**2+Y**2+X**2
      SQ2F=SQRT(RS)
      RETURN
      END

```

```

SUBROUTINE PFP3(EPS,MIX)
SUBROUTINE PFP3 SOLVES FOR SOURCE DENSITY
DIMENSION VIP(650),S(5,650),COEF(900),VTX(650)
COMMON TITLF(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AQP(650),REFA,RFRCDY,NQUAD,IWRITE,NP,KNEW
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15
COMMON /SIK/SN(650),VNP(650),IPN(650)
COMMON /RING/VXX(3,650)
WRITE (JWRITE,1)
1 FCFORMAT(1H1,/,24H0SOURCE DENSITY SOLUTION)
  WRITE (JWRITE,2) (TITL(I),I=1,20)

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2 FORMAT (1H0,20A4)
  K1=1
  K2=NP
  SET CONDITIONS FOR ONSET FLOW OF -1.0+VXX(1,K) IN X DIRECTION.
  ZERO IN Y AND Z DIRECTIONS
  FX=-1.0
  CCMPUTE (1) DOT PRODUCT OF PANEL NORMAL TO ONSET FLOW, VIP(K),
  (2) DOT PRODUCT OF PANEL NORMAL TO NONUNIFORM FLOW, VIX(K),
  (3) INITIAL SOURCE DENSITY. AND SET PARTIAL SUM VECTOR TO ZERO
  DO 3 K=1,NP
    VIP(K)=XNP(K)*FX
    VIX(K)=XNP(K)*VXX(1,K)
    S(5,K)=-(VIP(K)+VIX(K)-VNP(K))*11936
  3 SN(K)=0.
    SN(NP+1)=0.
    SN(NP+2)=0.
    SN(NP+3)=0.
    SN(NP+4)=0.
    WRITE (JWRITE,30) FX
    WRITE (JWRITE,4)
  4 FORMAT (/,12X,37HITERATIVE MATRIX SOLUTION INFORMATION.,/27H0ITERA
  1TION SUM OF CHANGES,9X,1HA,10X,2HB1,10X,2HB2)
  IT=1
  IC=5
  START ITERATION, READ FIRST BLOCK OF COEFFS., START LOOP OVER QUADS.
  5 READ (KFILE4)IDW,COEF
  (DO LOOP 40) CALCULATES THE SUM OF THE PRODUCTS OF THE INDUCED
  VELOCITIES AND THE SOURCE DENSITIES
  J=0
  DO 8 K=1,NP
    PICK UP SOURCE DENSITY & START LOOP OVER CENTROID POINTS
    SP=S(IC,K)
    DO 8 KP=1,NP,5
      IF (J-900) 7,6,6
  6 READ (KFILE4)IDW,COFF
  J=0
  CCMPUTE PARTIAL SUMS FOR NEXT 5 POINTS
  7 SN(KP)=SN(KP)+COEF(J+1)*SP
    SN(KP+1)=SN(KP+1)+COEF(J+2)*SP
    SN(KP+2)=SN(KP+2)+COEF(J+3)*SP
    SN(KP+3)=SN(KP+3)+COEF(J+4)*SP
    SN(KP+4)=SN(KP+4)+COEF(J+5)*SP

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C*** J=J+5
      END LOOP OVER CENTROID POINTS & END LOOP OVER QUADS.
C*** CCNTINUE
      8 CCMPUTE NEW SOURCE DENSITIES
C*** REWIND KFILE4
      PASS=1.0
      SUM=0.
      DO 9 K=K1,K2
        SN(K)=-(SN(K)+VIP(K)-VNP(K)+VTX(K))/6.283185308
        TEST=ABS(SN(K)-S(IC,K))
        SUM=SUM+TEST
        IF (TEST.GT.EPS)PASS=-1.0
      9 CCNTINUE
        WRITE (JWRITE,29) IT,SUM
        IF (PASS.EQ.1.0) GO TO 27
        IF (IT.EQ.MIX) GO TO 27
        IT=IT+1
        IC=IC-1
        IF (IC.EQ.0) GO TO 11
        DO 10 K=K1,K2
          S(IC,K)=SN(K)
        10 SN(K)=0.
          GC TO 5
        11 A=0.
          B1=0.
          B2=0.
          DA=0.
          D1=0.
          D2=0.
          DO 17 K=K1,K2
            DS9=2*S(1,K)-SN(K)-S(2,K)
            IF (DS9.GT.0.) GO TO 12
            A=A+S(2,K)-S(1,K)
            CA=DA-DS9
            GC TO 13
          12 A=A+S(1,K)-S(2,K)
            DA=DA+DS9
          13 DS1=S(4,K)-S(3,K)
            DS2=S(3,K)-S(2,K)
            DS3=DS1-DS2
            DSS=S(2,K)-S(1,K)
            DSS=DS2-DSS

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DS6=DS1-DSS
DS4=DS2-S(1,K)+SN(K)
DS7=DS3+DS4-DSS*DS6
DS8=DS6+DS5-DS4*DS3
IF (DS7.GT.0.) GO TO 14
B1=B1-DS1+DS4+DS2*DS6
D1=D1-DS7
GC TO 15
14 B1=B1+DS1*DS4-DS2*DS6
D1=D1+DS7
15 IF (DS8.GT.0.) GC TO 16
B2=B2-DS1+DS5+DS2*DS3
D2=D2-DS8
GO TO 17
16 B2=B2+DS1*DS5-DS2*DS3
D2=D2+DS8
17 CONTINUE
A=A/DA
B1=B1/D1
B2=B2/D2
IF (IT.EQ.6) GO TO 23
AA=ABS(A-AS)
IF (AA.GT..02) GO TO 20
DC 18 K=K1,K2
S(5,K)=A*(SN(K)-S(1,K))+S(1,K)
SN(K)=0.
18 WRITE (JWRITE,19)
19 FCORMAT (29X,17H3 EXTRAPCLATION )
GC TO 25
20 BB1=50.*ABS(B1-B51)
BB2=50.*ABS(B2-B52)
BBB=ABS(B1)+ABS(B2)
IF ((BB1.GT.BBB).OR.(BB2.GT.BBB)) GO TO 23
DC 21 K=K1,K2
S(5,K)=S(2,K)+B1*(S(1,K)-S(2,K))+B2*(SN(K)-S(2,K))
21 SN(K)=0.
WRITE (JWRITE,22)
22 FCORMAT (29X,17H3 EXTRAPCLATION )
GC TO 25
23 DO 24 K=K1,K2
24 S(5,K)=SN(K)
24 SN(K)=0.

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25 IC=5  
26 WRITE (JWRITE,26) A,B1,B2  
26 FORMAT (29X,3E12.3)  
27 AS=A

BS1=B1  
BS2=B2  
GC TO 5

27 DC 28 K=K1,K2

28 S(1,K)=SN(K)

29 FFORMAT (4X,13,E18.5)

30 FFORMAT (/.13H0 X VELOCITY=.F4.1.24H+VXX(1,K)  
1.15H Z VELOCITY=.4H 0.0)

Y VELOCITY=.4H 0.0

1.15H  
RETURN  
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SUBROUTINE PFP4(CLPA,CDPA,ICK)

SUBROUTINE PFP4 COMPUTES VELOCITIES AND PRESSURE COEFFICIENTS AT  
THE PANEL CENTROID POINTS

DIMENSION CV1(1000)  
COMMON TITLE(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(

1650),AQP(650),REFA,REBODY,NQUAD,IWRITE,NP,KNEW

COMMON /RING/VTX(3,650)

COMMON /SIK/SI(650),VNP(650),IPN(650)

COMMON /VCK/HVF,SFC,DEP,CPHA,TINF,ADUT,AIN,EDA

COMMON /CFSX/CPX(650),CPIN,CPOUT

COMMON /VXYZ/VX1(650),VY1(650),VZ1(650),VABS(650)

COMMON /HOLD/XNH(650),ZNH(650),AQPH(650)

COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE

15

C

WRITE (JWRITE,1)

1 FFORMAT (1H1,/,1X,75H COMPUTATION OF VELOCITIES AND PRESSURE COEFF

1 ICIENTS AT THE PANFL CENTROIDS)

INITIALIZE PARAMETERS

D=-.5/3.14159265

J=1

K1=1

IF (KNEW.EQ.1) K HOLD=NP

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K2=NP
BBR=1.0
CD=0.0
CL=0.0
AREA=0.0
C** READ FIRST BLOCK OF COEFFICIENTS
ITAPE=KFILE3
READ (KFILE3) BB,CV1
IF (BB-BBR) 45,2,45
C** CALCULATE VELOCITY COMPONENTS DUE TO ENTIRE FLOW FIELD
DO 3 I=K1,K2
  VX1(I)=-1.0+VTX(1,I)+VNP(I)*XNP(I)-S1(I)*XNP(I)/D
  VY1(I)=VTX(2,I)+VNP(I)*YNP(I)-S1(I)*YNP(I)/D
  VZ1(I)=VTX(3,I)+VNP(I)*ZNP(I)-S1(I)*ZNP(I)/D
3 CCNTINUE
C** SET UP LOOP OVER QUADS. PICK UP SOURCE, SET UP LOOP OVER CENTROIDS
C** TO SUM THE PRODUCTS OF THE VELOCITY REFLECTIONS AND THE SOURCE
C** DENSITIES
JC=2
4 SIJ=S1(J)
DO 10 JP=K1,K2
  C** COMPUTE PARTIAL SUM FOR 3 COMPONENTS OF 3 VELOCITIES
  VX1(JP)=VX1(JP)+SIJ*CV1(JC)
  VY1(JP)=VY1(JP)+SIJ*CV1(JC+1)
  VZ1(JP)=VZ1(JP)+SIJ*CV1(JC+2)
  JC=JC+3
C** READ MORE COEFFICIENTS IF NEEDED
IF (JC-1000) 10,5,5
5 JC=2
IF (BBR-635.0) 6,7,8
6 READ (KFILE3) BB,CV1
GO TO 9
7 REWIND KFILE3
9 READ (KFILE5) BB,CV1
9 BBR=BBR+1.
IF (BBR-BB) 45,10,45
C** END OF LOOP OVER CENTROIDS THEN END OF LOOP OVER QUADS.
10 CCNTINUE
J=J+1
IF (J-NP) 4,4,11
11 IF (BBR-635.0) 12,12,13
12 REWIND KFILE3

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13 GO TO 14
14 REWIND KFILES
15 IP=K1+49
16 THE VELOCITIES AT THE CONTROL POINTS ON THE BODY SURFACE HAVE BEEN
17 CALCULATED
18 IS=K1
19 IPAGE=1
20 IIN=0
21 ICUT=0
22 CPIN=0.0
23 CPOUT=0.0
24 ACUT=0.0
25 AIN=0.0
26 IF (IP-K2) 16,16,28
27 COMPUTE PRESSURE COEFFICIENT, ABSOLUTE VALUE OF VELOCITY, CL, & CD
28 IF (IPAGE.EQ.1) WRITE (JWRITE,17) (TITLE(1),I=1,20),IPAGE
29 FFORMAT (//,1H0,20A4,8H PAGE=,15)
30 IF (IPAGE.NE.1) WRITE (JWRITE,18) (TITLE(1),I=1,20),IPAGE
31 FFORMAT (1H1,////,1X,20A4,8H PAGE=,15)
32 WRITE (JWRITE,19)
33 FFORMAT (8H0 X FLOW)
34 WRITE (JWRITE,20)
35 FFORMAT (4H PT.,10X,2HXC,8X,2HYC,8X,2HZC,12X,2HVC,8X,2HVV,8X,2HVZ,9
36 1X,5HABS,V,8X,2HCP,6X,6HSOURCE,5X,8HV NORMAL,5X,4HAREA)
37 DO 27 I=1,IP
38 VSO=VX1(I)**2+VY1(I)**2+VZ1(I)**2
39 VM=SQRT(VSQ)
40 VARS(I)=VM
41 CP=1.-VSO
42 CPS(I)=CP
43 VNR=VX1(I)*XNP(I)+VY1(I)*YNP(I)+VZ1(I)*ZNP(I)
44 IF (KNEW.EQ.2.OR.ICK.GE.2) GO TO 23
45 CHECK INDICATOR FOR A NONZERO NORMAL VFLOCITY SPECIFICATION
46 IF (IPN(I).EQ.0) GO TO 23
47 IF ((1+IPN(I)/IABS(IPN(I))).EQ.0) GO TO 21
48 GO TO 22
49 CPIN=CPIN+CP*AQP(I)
50 AIN=AIN+AQP(I)
51 IIN=IIN+1
52 GC TO 23
53 CPOUT=CPOUT+CP*AQP(I)
54 ACUT=ACUT+AQP(I)

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23 IF (1.GT.KHOLD) GO TO 25
   IF (KNEW.EQ.2) GO TO 24
   CL=CL+CP*AQP(I)*ZNP(I)
   CD=CD+CP*AQP(I)*XNP(I)
   AREA=AREA+AQP(I)
   GO TO 25
C**      COMPUTE CL, CD, AND AREA FOR WAKE-BODY PORTION
24 CL=CL+CP*AQP(I)*ZNH(I)
   CD=CD+CP*AQP(I)*XNH(I)
   AREA=AREA+AQP(I)
C**      WRITE CENTROID POINTS, VELOCITIES, CP'S, CL-PRESSURE, & CD-PRESSURE
25 WRITE (JWRITE,26) I,XCP(I),YCP(I),VX1(I),VY1(I),VZ1(I),VM,C
   IP,S1(I),VNR,AQP(I)
26 FORMAT (1X,13.4X,3F10.5,4X,3F10.5,2F11.5,E12.2,2X,E10.3)
27 CCNTINUE
   IS=IS+50
   IP=IP+50
   IPAGE=IPAGE+1
   IF (K2-IS) 29,28,15
28 IP=K2
   GO TO 16
C**      ADJUST AND REFERENCE CL AND CD DUE TO SYMMETRY AND REFERENCE AREA
29 CLPA=2.0*CL
   CDPA=2.0*CD
   CLP=CLPA/REFA
   CDP=CDPA/REFA
   WRITE (JWRITE,30) CLP,CDP,REFA,REBODY
30 FCRMAT (1H,////.18X,35HPRESSURE LIFT AND DRAG COEFFICIENTS,/,2
   11X,29(1H*),/,25X,14HPRESSURE CL = .F11.5,/,25X,14HPRESSURE CD = .F
   111.5,/,22X,17HREFERENCE AREA = .F11.5,/,21X,18HREYNOLDS NUMBER = .
   1E11.4,/,21X,29(1H*),/)
   IF (KNEW.EQ.2) GO TO 35
   WRITE (JWRITE,31)
31 FCRMAT (1H,////.2X,2HPT,5X,3HXNH,6X,3HYNH,6X,3FZNH,6X,2HCP,5X,6HVX*
   1XNH,3X,6HVV*YNH,3X,6HVZ*ZNH,5X,4HAQP,1.3X,13H2*CP-AQPH*ZNH,3X,13H2*
   1CP*AQPH*XNH,4X,2HPT,/)
   LINE=1
DC 34 I=1,NP
   VXN=VX1(I)*XNP(I)
   VYN=VY1(I)*YNP(I)
   VZN=VZ1(I)*ZNP(I)

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CAZ=2.0*CPS(1)*AQP(1)*ZNP(1)
CAX=2.0*CPS(1)*AQP(1)*XNP(1)
LINE=LINE+1
IF (LINE.LE.50) GO TO 32
LINE=0
WRITE (JWRITE,31)
32 WRITE (JWRITE,33) I,XNP(1),YNP(1),ZNP(1),CPS(1),VXXN,VYYN,VZZN,AQP
1(I),CAZ,CAX,I
33 FORMAT (1X,I4,7F9.5,3X,F10.7,6X,F10.7,5X,I4)
34 CCNTINUE
GO TO 41
35 WRITE (JWRITE,36)
36 FORMAT (1H1,/,2X,2HPT,5X,3HXNP,6X,3HYNP,6X,3HZNP,6X,2HCP,5X,6HVX*,
1XNP,3X,6HVV*YNP,3X,6HVZ*ZNP,5X,4HAQP,3X,13H2*CP*AGPH*ZNH,3X,13H2*
1CP*AGPH*XNH,4X,2HPT,/)
LINE=0
DO 40 I=1,NP
VXXN=VX1(I)*XNP(1)
VYYN=VY1(I)*YNP(1)
VZZN=VZ1(I)*ZNP(1)
LINE=LINE+1
IF (LINE.LE.50) GO TO 37
LINE=0
WRITE (JWRITE,36)
37 IF (I.GT.KHOLD) GO TO 38
CAZ=2.0*CPS(1)*AGPH(1)*ZNH(1)
CAX=2.0*CPS(1)*AGPH(1)*XNH(1)
WRITE (JWRITE,33) I,XNP(1),YNP(1),ZNP(1),CPS(1),VXXN,VYYN,VZZN,AQP
1(I),CAZ,CAX,I
GC TO 40
38 WRITE (JWRITE,39) I,XNP(1),YNP(1),ZNP(1),CPS(1),VXXN,VYYN,VZZN,AQP
1(I),I
39 FCFORMAT (1X,I4,7F9.5,3X,34X,I4)
40 CONTINUE
41 IF (KNEW.EQ.0.OR.ICK.GE.2) GO TO 47
TEST FOR ERRORS
IF (IIN.EQ.0.OR.IOUT.EQ.0) ICK=2
IF (ICK.EQ.1) GO TO 44
WRITE (JWRITE,42)
42 FCFORMAT (1X,/,1X,131HAT LEAST ONE INLET(OUTLET) WAS SPECIFIED WIT
1HCUT AT LEAST ONE OUTLET(INLET)...ASSUMING NO INLETS OR OUTLETS...
1EXECUTION PROCEEDING.//)
C***

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DO 43 I=1,NP
  VNP(I)=0.0
  GO TO 47
C**
  CCMPUTE AVERAGE CP'S
  CPIN=CPIN/AIN
  CPOUT=CPOUT/ADUT
  GO TO 47
45 WRITE (JWRITE,46) ITAPE,BBR,BB
46 FORMAT (6H1TAPE,12.16H OUT OF POSITION/14.6F6.1)
47 RETURN
END

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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28  
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SUBROUTINE VINOUT(JWRITE,VINF,ROE,NQE,VI)
C**
SUBROUTINE VINOUT CALCULATES THE INTERIOR PRESSURE COEFFICIENTS
AND THE NORMAL VELOCITIES ON SPECIFIED PANELS
C
COMMON TITLE(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AQP(650),REFA,REBODY,NQUAD,IWRITE,NP,KNEW
COMMON /SIK/SN(650),VNP(650),IPN(650)
COMMON /VCK/HVF,SFC,DEP,CPHA,TINF,ADUT,AIN,EOA
COMMON /CPSX/CPS(650),CPIN,CPOUT
COMMON /CANCEL/ICANCL,NODE
C
IPASS=0
WRITE (JWRITE,1) CPIN,AIN,CPOUT,ADUT
1 FORMAT (1H1,/,5X,75H** CALCULATION OF INTERIOR PRESSURE COEFFICI
ENTS AND NORMAL VELOCITIES **,/,9X,29H AVERAGE CP ON INLET PANELS
1 =,1PE16.9,3X,13H INLET AREA =,1PE16.9,/,9X,29H AVERAGE CP ON EXHA
UST PANELS =,1PE16.9,3X,13H EXHAUST AREA =,1PE16.9,/)
C**
CALCULATE PRESSURE COEFFICIENTS
2 CPXX=(ADUT**2*CPOUT+(FOA*AIN)**2*CPIN/(AIN**2+EOA**2))*((AIN**2+EO
1A**2)/((ADUT*AIN)**2+(ADUT**2+AIN**2)*EOA**2))
CPX=(AIN**2*CPIN+EOA**2*CPXX)/(AIN**2+EOA**2)
IF (CPX.GT.CPXX) GO TO 3
IF (ABS(CPX-CPXX).LT.1.0E-05) CPXX=CPX
3 WRITE (JWRITE,4) CPX,CPXX
4 FORMAT (10X,5HCPX =,1PE16.9,/,10X,5HCPXX=,1PE16.9,/)
IF (CPX.LF.CPIN.AND.CPX.GE.CPXX) GO TO 7
WRITE (JWRITE,5)

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5 FORMAT (12X,32HCPX > CPIN OR CPX < CPXX. STOP...////)
6 ICANCL=1
7 IF (CPXX.LE.CPX.AND.CPXX.GE.CPOUT) GO TO 9
8 WRITE (JWRITE,8)
9 FORMAT (12X,34HCPXX > CPX OR CPXX < CPOUT. STOP...////)
10 GO TO 6
11 ADJUST EFFECTIVE ORIFICE AREA EFFECT
12 IPASS=IPASS+1
13 IF (IPASS.GT.1) GO TO 14
14 PNET=DEPT*(778.0*HVF*SFC-1.0)
15 IF (PNET) 10,10,12
16 WRITE (JWRITE,11) PNET
17 FCFORMAT (12X,23HDEPT*(778.0*HVF*SFC-1) =.1PE16.9./)
18 IF (PNET.LT.0.0) GO TO 6
19 GO TO 14
20 TR=PNET/(ROE*32.2*AIN*CPHA*778.0*INF*VINF*SQR(CPIN-CPX))+1.0
21 TR=SQR(1.0/TR)
22 ECA=EOA*TR
23 WRITE (JWRITE,13) TR,ECA
24 FORMAT (9X,58HADJUSTMENT DUE TO HEATING OF FLOW: TEMPERATURE RATIO
25 =.1PE16.9./,44X,23HEFFECTIVE ORIFICE AREA=.1PE16.9./)
26 GO TO 2
27 CALCULATE NORMAL VELOCITIES
28 DC 24 I=1,NQE
29 ITEST=3
30 IF (IPN(I).EQ.0) GO TO 24
31 IF ((1+IPN(I))/ABS(IPN(I))).EQ.0) GO TO 15
32 GO TO 16
33 X1=CPX(I)-CPX
34 IF (X1.LT.0.0) ITEST=1
35 VNP(I)=-SQR(ABS(X1))
36 GO TO 17
37 X1=CPXX-CPX(I)
38 IF (X1.LT.0.0) ITEST=2
39 VNP(I)=SQR(ABS(X1))
40 GC TO (1A.20.22).ITEST
41 WRITE (JWRITE,19) I,VNP(I),I
42 FORMAT (10X,24HNORMAL VELOCITY AT PANEL.14.3H = .E14.7.10X.11HNOTE
43 1: (CP(.14.11H)-CPX )<0.0./)
44 GO TO 24
45 WRITE (JWRITE,21) I,VNP(I),I

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32 33 34 35 36 37 38 39 40 41 42 43 44
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PCH PCH PCH PCH PCH PCH PCH PCH PCH PCH PCH PCH PCH

ZZ(N,M)=ZP+ZORG
2 CONTINUE
3 LMN=LMN+MMAX
C**
3 CCNTINUE
4 PUNCH CARDS FOR NEW FUSELAGE
WRITE (JPUNCH,4) (XX(J,1),J=NMIN,NMAX)
DO 5 I=NMIN,NMAX
WRITE (JPUNCH,4) (YY(I,J),J=MMIN,MMAX)
WRITE (JPUNCH,4) (ZZ(I,J),J=MMIN,MMAX)
5 CCNTINUE
RETURN
END

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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26
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SUBROUTINE PFP5(MM,NN,AREAAV,AVDELS,AVXCG,CDFA)
C**
SUBROUTINE PFP5 COMPUTES ON-BODY STREAMLINES
C
DIMENSION XC1(650),YC1(650),XC2(650),YC2(650),XC3(650),XC4(650),YC
14(650),X3(650),Y3(650),Z3(650),X4(650),Y4(650),Z4(650),DMX(650),XL
17(75),YL(75),ZL(75),YC3(650),SF(5),XCR(5),YCR(5),STML(75),UABS(75),
18SKIN(650),DSTAR(650),NQTEST(5)
EQUIVALENCE (YC3(1),YC2(1)),(XL(1),XNH(1)),(YL(1),AQPH(1)),(ZL(1),
19ZNH(1))
COMMON /HOLD/XNH(650),ZNH(650),AQPH(650)
COMMON TITLF(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AQPH(650),REFA,REBODY,NQUAD,IWRITE,NP,KNEW
COMMON /VXY7/VX1(650),VY1(650),VZ1(650),VABS(650)
COMMON /BL/VOV(75),SS(75),VINP,VO,ROE,DELS(150),CFI(150),THT(150),
17STOTAL,KKK
COMMON /INDUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFIL5
COMMON /RING/VTX(3,650)
COMMON /CANCEL/ICANCL,NGDE
COMMON /NAMELIST /NAM1/NP,NQ,DMX/NAM2/II,NSTART,NEND,NDEL/NAM3/LL,MID,DIRT
18JI/NAM4/AF,UX,UY,UZ,CP,NQ,NCP,LNQ,JSTOP,J,JL,XLT,XL,YL,ZL/NAM
195/NQ,IQT,NR,NU,LXQ,UYQ,UZQ,UXR,UYR,UZR,UXU,UZU,UQ,VQ,CSR,UT,VT
1XXR,XYP,UR,YXR,YR,VR,UU,CSU,VU,XD,YD,ZD,XI,YI,ZI,YT,XR,YR/NAM6/
1XD,YD,ZD,XU,YT,ZT,YU,DEN,U1,U2,V1,V2,USL,VSL,UXP,UYP,UZP,VSQD/NAM7
1/DEN,CXY,CYY,CXX,CQ,NQ,XCR,YCR,SF,TEST/NAM8/N,XM,YM,SFM,AC,BC/NAM9
1/XNTP,YNTP,TESTP/NAM10/TEST,XNT,YNT,NAM11/UX,UY,UZ,CP,UABS/NAM12/J

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1L,J,J1,USL,VSL,UX,UY,UZ,VSQD,CORD,STML,CP,AF,LNQ/NAM13/KMOD,NTEST,
1NQ,NQTEST,M/NAM14/M,I,TEST,DS1,DS2,DS3,DS4,XLT,YLT,ZLT,ZSQ/NAM15/T
1EST,RC1,RC2,RC3,RC4/NAM16/TEST/NAM17/TEST/NAM18/TEST/NAM19/DIRT,J1
1JMIN/NAM20/JMAX,SSS,STML/NAM21/KEY,JJ,KK,JMIN/NAM22/XL,YL,ZL,UABS
1/NAM23/KEY,KK,JJ,JMAX/NAM24/JMN,JMX,AF,L/NAM25/J,L,STML,UABS,AF,MI
1D/NAM26/L,K,STML,UABS/NAM27/L,JMAX,JMIN,STML,XL,YL,ZL,UABS
COMMON /SIK/SN(650),VNP(650),IPN(650)
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C
1 WRITE (JWRITE,1)
1 FORMAT (1H1,///,35H0CALCULATION OF ON-BODY STREAMLINES)
NB=(NP+11)/12
NLIN=NQUAD
DO 2 I=1,NB
IFN=I*12
IS=IFN-11
READ PANEL GEOMETRY FROM TAPE
PFAD (KFILF)Q,((XC1(J),YC1(J),XC2(J),YC2(J),XC3(J),XC4(J),YC4(J),X3
1(J),Y3(J),Z3(J),X4(J),Y4(J),Z4(J),{SKIP,K=1,3},J=IS,IFN)
NQ=Q
IF (NQ.NE.IS) GO TO 68
2 CCNTINUE
NCD1=NP+1
NCD2=NOD1
IMRTS=IWRITE
IF (NODE.GT.NP)NOD2=0
IF (NOD2.LE.0) GO TO 3
NOD1=NOD2-2
NCD2=NOD2+2
IF (NCD1.LE.0)NJD1=1
IF (NOD2.GT.NP)NCD2=NP
FOR EACH QUAD, COMPUTE SQUARE OF THE RADIUS OF A CIRCLE ABOUT THE
CENTROID WHICH ENCLOSES THE QUAD WITH 1% TO SPARE
3 DC 4 I=1,NP
D1=((XC1(I)**2+YC1(I)**2)*1.01
D2=((XC2(I)**2+YC2(I)**2)*1.01
D3=((XC3(I)**2+YC3(I)**2)*1.01
D4=((XC4(I)**2+YC4(I)**2)*1.01
IF (I.GT.75) GO TO 4
XL(I)=0.0
YL(I)=0.0
ZL(I)=0.0
STML(I)=0.0

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DIRT=-1.
JI=-1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM3)
13 AF=1.
UX=0.
UY=0.
UZ=0.
CP=0.
STML(MID)=0.
NQ=LL
NCP=LL
LNQ=NG
XL(MID)=XCP(LL)
YL(MID)=YCP(LL)
ZL(MID)=ZCP(LL)
JSTOP=MID+3
J=MID
JL=J
XLT=(XL(J)-XCP(NQ))*X3(NQ)+(YL(J)-YCP(NQ))*Y3(NQ)+(ZL(J)-ZCP(NQ))*
1 Z3(NQ)
YL=(XL(J)-XCP(NQ))*X4(NQ)+(YL(J)-YCP(NQ))*Y4(NQ)+(ZL(J)-ZCP(NQ))*
1 Z4(NQ)
XL(J)=XLT*X3(NQ)+YLT*X4(NQ)+XCP(NQ)
YL(J)=XLT*Y3(NQ)+YLT*Y4(NQ)+YCP(NQ)
ZL(J)=XLT*Z3(NQ)+YLT*Z4(NQ)+ZCP(NQ)
IF (IWRITE.LT.0) WRITE (JWRITE,NAM4)
14 IGT=MOD(NQ,4)+1
GO TO (18,15,16,17),IGT
15 NR=NQ+1
NU=NQ+2
GO TO 19
16 NF=NG+2
NU=NQ-1
GO TO 19
17 NR=NG-2
NU=NQ+1
GC TO 19
18 NR=NG-1
NU=NQ-2
19 UXC=-(VXI*VXI(NQ))
UYQ=-(VXI*VXI(NQ))
UZQ=-(VXI*VZI(NQ))

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C***
UVR=-(VXI*VXI(NR))
UYR=-(VXI*VYI(NR))
UZR=-(VXI*VZI(NR))
UXU=-(VXI*VXI(NU))
UYU=-(VXI*VYI(NU))
UZU=-(VXI*VZI(NU))
TRANSFORM VELOCITIES TO QUAD. SYSTEM
UO=UXQ*X3(NQ)+UYQ*Y3(NQ)+UZQ*Z3(NQ)
VO=UXQ*X4(NQ)+UYQ*Y4(NQ)+UZQ*Z4(NQ)
CSR=1./((XNP(NQ)*XNP(NQ)+YNP(NQ)*YNP(NQ)+ZNP(NQ)*ZNP(NQ))
UT=UXR*X3(NR)+UYR*Y3(NR)+UZR*Z3(NR)
VT=(UXR*X4(NR)+UYR*Y4(NR)+UZR*Z4(NR))*CSR
XNR=(X3(NR)*X3(NQ)+Y3(NR)*Y3(NQ)+Z3(NR)*Z3(NQ))
XYR=(X4(NR)*X4(NQ)+Y4(NR)*Y4(NQ)+Z4(NR)*Z4(NQ))
UR=UT*XNR+VT*XYR
YXR=(X3(NR)*X4(NQ)+Y3(NR)*Y4(NQ)+Z3(NR)*Z4(NQ))
YXR=(X4(NR)*X4(NQ)+Y4(NR)*Y4(NQ)+Z4(NR)*Z4(NQ))
VR=UT*VXR+VT*YXR
UU=UXU*X3(NQ)+UYU*Y3(NQ)+UZU*Z3(NQ)
CSU=(XNP(NQ)*XNP(NU)+YNP(NQ)*YNP(NU)+ZNP(NQ)*ZNP(NU))/CSU
VU=(UXU*X4(NQ)+UYU*Y4(NQ)+UZU*Z4(NQ))*YTT*CSR+YTT)*CSR*.16666667
FIND RELATIVE COORDINATES OF NEIGHBORING QUADS.
XD=XCP(NR)-X3(NQ)
YD=YCP(NR)-Y3(NQ)
ZD=ZCP(NR)-Z3(NQ)
XT=XD*X3(NR)+YD*Y3(NR)+ZD*Z3(NR)
YT=XD*X4(NR)+YD*Y4(NR)+ZD*Z4(NR)
ZT=XD*XNP(NR)+YD*YNP(NR)+ZD*ZNP(NR)
YT=(-4.*SQRT(YT**2+ZT**2)+YTT*CSR+YTT)*CSR*.16666667
XR=XT*XNR+YT*XYR
YR=XT*YXR+YT*YXR
IF (IMRIF.LT.0) WRITF (JWRIF,NAMS)
XD=XCP(NU)-XCP(NQ)
YD=YCP(NU)-YCP(NQ)
ZD=ZCP(NU)-ZCP(NQ)
XU=XD*X3(NQ)+YD*Y3(NQ)+ZD*Z3(NQ)
YU=XD*X4(NQ)+YD*Y4(NQ)+ZD*Z4(NQ)
ZU=XD*XNP(NQ)+YD*YNP(NQ)+ZD*ZNP(NQ)
YU=(4.*SQRT(YT**2+ZT**2)+YTT*CSR+YTT)*CSR*.16666667
FIND COEFFICIENTS OF VELOCITY FUNCTIONS
DEN=1./((XR*YU-XU*YR)
U1=((UR-UQ)*YU-(LU-UQ)*YR)*DFN

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C\*\*\*

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C***
U2=-((UR-UQ)*XU-(UU-UQ)*XR)*DEN
V1=((VR-VQ)*YU-(VU-VQ)*YR)*DEN
V2=-((VR-VQ)*XU-(VU-VQ)*XR)*DEN
FIND VELOCITY AT STREAMLINE POINT
USL=UQ+U1*XLT+U2*YLT
VSL=VQ+V1*XLT+V2*YLT
UXP=USL*X3(NQ)+VSL*X4(NQ)
UYP=USL*Y3(NQ)+VSL*Y4(NQ)
UZP=USL*Z3(NQ)+VSL*Z4(NQ)
VSQD=USL**2+VSL**2
IF (IWRITE.LT.0) WRITE (JWRITE,NAM6)
DEN=VSQD*SQRT(VSQD)
FIND LOCAL STREAM FUNCTION
CXY=(U1*VQ**2-V2*UQ**2)/VSQD
CYV=U2-UQ*VQ*(U1+V2)/VSQD
CXX=U2-CYV-V1
CC=XLT*VQ-YLT*UQ-CXY*XLT-CYV*YLT**2-CXX*XLT**2
FIND STREAM FUNCTION AT CORNER POINTS
XCR(1)=XC1(NQ)
XCR(2)=XC2(NQ)
XCR(3)=XC3(NQ)
XCR(4)=XC4(NQ)
XCR(5)=XCR(1)
YCR(1)=YC1(NQ)
YCR(2)=YC2(NQ)
YCR(3)=YC3(NQ)
YCR(4)=YC4(NQ)
YCR(5)=YCR(1)
DO 20 N=1,4
20 SF(N)=CO-VQ*XCR(N)+UQ*YCR(N)+CXY*XCR(N)*YCR(N)+CYV*YCR(N)**2+CXX*X
1CR(N)**2
SF(5)=SF(1)
TEST=0.
IF (IWRITE.LT.0) WRITE (JWRITE,NAM7)
DO 23 N=1,4
IF (SF(N)*SF(N+1).GF.0.) GO TO 23
XM=(XCR(N)+XCR(N+1))*5
YM=(YCR(N)+YCR(N+1))*5
FIND INTERSECTION WITH SIDE OF QUAD.
SFM=CO-VQ*XM+UQ*YM+CXY*XM*YM+CYV*YM**2+CXX*XM**2
AC=2.*(SF(N)-2.*SFM+SF(N+1))
BC=3.*SF(N)-4.*SFM+SF(N+1)
C***

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IF (IWRITE.LT.0) WRITE (JWRITE,NAM8)
IF (AC.EQ.0) GO TO 21
SR=SQRT(BC**2-4.*AC*SF(N))
TP=(BC+SR)/(2.*AC)
IF (TP.LE.1.-AND.TP.GE.0.) GO TO 22
TP=(RC-SR)/(2.*AC)
IF (TP.LE.1.-AND.TP.GE.0.0) GO TO 22
21 IF (AC.EQ.0) GO TO 23
TP=SF(N)/BC
IF (TP.GT.1.-OR.TP.LT.0.0) GO TO 23
XNTP=(1.-TP)*XCR(N)+TP*XCR(N+1)
22 YNTP=(1.-TP)*YCR(N)+TP*YCR(N+1)
IF (IWRITE.LT.0) WRITE (JWRITE,NAM9)
TESTP=((XNTP-XLT)*UG+(YNTP-YLT)*VQ)*DIRT
IF (TESTP.LE.TEST) GO TO 23
TEST=TESTP
XNT=XNTP
YNT=YNTP
IF (IWRITE.LT.0) WRITE (JWRITE,NAM10)
23 CONTINUE
IF (TEST.EQ.0.) GO TO 34
AVERAGE LAST VELOCITY AND CURVATURE
UX=(UX+UXP)*AF
UY=(UY+UYP)*AF
UZ=(UZ+UZP)*AF
CP=1.-((UX**2+UY**2+UZ**2)
UABS(J)=SQRT(1.-CP)
IF (IWRITE.LT.0) WRITE (JWRITE,NAM11)
IF (J.GE.JSTOP) GO TO 35
C*** COMPUTE VELOCITY AT NEXT POINT
JL=J
J=J+JI
USL=UQ+XNT*U1+YNT*U2
VSL=VQ+XNT*V1+YNT*V2
UX=USL*X3(NQ)+VSL*X4(NQ)
UY=USL*Y3(NQ)+VSL*Y4(NQ)
UZ=USL*Z3(NQ)+VSL*Z4(NQ)
VSQD=USL**2+VSL**2
CCRD=SQRT((XNT-XLT)**2+(YNT-YLT)**2)*DIRT
STML(J)=STML(JL)+CORD
CF=1.-VSQD
UABS(J)=SQRT(1.-CF)

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AF=.5
LNQ=NQ
IF (IWRITE.LT.C) WRITE (JWRITE,NAM12)
XL(J)=XNT*X3(NQ)+YNT*X4(NQ)+XCP(NQ)
YL(J)=XNT*Y3(NQ)+YNT*Y4(NQ)+YCP(NQ)
ZL(J)=XNT*Z3(NQ)+YNT*Z4(NQ)+ZCP(NQ)
IF (J.LE.MINJ.OR.J.GE.MAXJ) GO TO 54
C*** PROCEDURE FOR FINDING NEXT QUAD. WAS MODIFIED SO THAT, DEPENDING
C*** ON THE DIRECTION. THERE ARE ONLY 5 POSSIBLE QUADS. TO TEST
KMOD=MOD(NQ,2)
NTEST=5
IF (DIRT) 26,24,29
24 WRITE (JWRITE,25) DIRT
25 FORMAT (I1,1X,7HDIRT = ,F10.7,26HPROGRAM TERMINATED IN PFP5)
ICANCL=1
RETURN
26 IF (KMOD) 27,28,27
C*** LAST QUAD. IS ODD & WE ARE TESTING AGAINST THE STREAM DIRECTION
27 NQTEST(1)=NQ-2*(MM-1)+1
NQTEST(2)=NQ+2
NQTEST(3)=NQ-2
NQTEST(4)=NQTEST(1)+2
NQTEST(5)=NQTEST(1)-2
IF (NQ.NE.NLINM1) GO TO 32
NQTEST(2)=NQTEST(5)
NTEST=3
GO TO 32
C*** LAST QUAD. IS EVEN & WE ARE TESTING AGAINST THE STREAM DIRECTION
28 NQTEST(1)=NQ-1
NQTEST(2)=NQ+2
NQTEST(3)=NQ-2
NQTEST(4)=NQ+1
NQTEST(5)=NQ-3
IF (NQ.GT.ILOWF3) GO TO 32
NQTEST(1)=NQTEST(2)
NQTEST(2)=NQTEST(3)
NTEST=2
IF (NQ.EQ.2) NTEST=1
GO TO 32
29 IF (KMOD) 30,31,30
C*** LAST QUAD IS ODD & WE ARE TESTING IN THE STREAM DIRECTION
30 NQTEST(1)=NQ+1

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NQTEST(2)=NQ+2
NQTEST(3)=NQ-2
NQTEST(4)=NQ+3
NQTEST(5)=NQ-1
IF (NQ.LT.IUPPER) GO TO 32
NTEST=2
NQTEST(1)=NQTEST(3)
IF (NQ.EQ.NLINM1)NTEST=1
GO TO 32
C** LAST QUAD IS EVEN & WE ARE TESTING IN THE STREAM DIRECTION
31 NQTEST(1)=NQ+2*(MM-1)-1
NQTEST(2)=NQ+2
NQTEST(3)=NQ-2
NQTEST(4)=NQTEST(1)+2
NQTEST(5)=NQTEST(1)-2
IF (NQ.NE.2) GO TO 32
NTEST=4
NQTEST(3)=NQTEST(5)
32 M=1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM13)
33 I=NQTEST(M)
NQ=I
TFST=(XL(J)-XCP(I))*2+(YL(J)-YCP(I))*2+(ZL(J)-ZCP(I))*2-DMX(I)
IF (TEST.GT.0.) GO TO 34
DS1=(XC1(I)-XC2(I))*2+(YC1(I)-YC2(I))*2
DS2=(XC2(I)-XC3(I))*2+(YC2(I)-YC3(I))*2
DS3=(XC3(I)-XC4(I))*2+(YC3(I)-YC4(I))*2
DS4=(XC4(I)-XC1(I))*2+(YC4(I)-YC1(I))*2
XL1=(XL(J)-XCP(I))*X3(I)+(YL(J)-YCP(I))*Y3(I)+(ZL(J)-ZCP(I))*Z3(I)
YL1=(YL(J)-XCP(I))*X4(I)+(YL(J)-YCP(I))*Y4(I)+(ZL(J)-ZCP(I))*Z4(I)
ZL1=(ZL(J)-XCP(I))*XNP(I)+(YL(J)-YCP(I))*YNP(I)+(ZL(J)-ZCP(I))*ZNP(I)
1(I)
ZSQ=ZLT*#2
IF (IWRITE.LT.0) WRITE (JWRITE,NAM14)
TEST=ZSQ-.1*DMX(I)
IF (TEST.GT.0.) GO TO 34
RC1=SQRT(ZSQ+(XL1-XC1(I))*#2+(YL1-YC1(I))*#2)
RC2=SQRT(ZSQ+(XL1-XC2(I))*#2+(YL1-YC2(I))*#2)
RC3=SQRT(ZSQ+(XL1-XC3(I))*#2+(YL1-YC3(I))*#2)
RC4=SQRT(ZSQ+(XL1-XC4(I))*#2+(YL1-YC4(I))*#2)
TEST=((RC1+RC2)*#2)-DS1*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM15)

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IF (TEST.LT.0.) GC TO 14
TEST=((RC2+RC3)*2)-DS2*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM16)
IF (TEST.LT.0.) GO TO 14
TEST=((RC3+RC4)*2)-DS3*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM17)
IF (TEST.LT.0.) GO TO 14
TEST=((RC4+RC1)*2)-DS4*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM18)
IF (TEST.LT.0.) GO TO 14
M=N+1
34 IF (M.LE.NTEST) GO TO 33
35 IF (DIRT.GT.0.) GC TO 36
C** CHANGE THE DIRECTION IN WHICH THE STREAMLINE IS TRACED
DIRT=1.
JI=1
JMIN=J
IF (IWRITE.LT.0) WRITE (JWRITE,NAM19)
GO TO 13
36 JMAX=J
SSS=STML(JMIN)
DO 37 J=JMIN,JMAX
37 STML(J)=STML(J)-SSS
IF (IWRITE.LT.0) WRITE (JWRITE,NAM20)
IF ((STML(JMIN+3)-STML(JMIN)).LT.8.*(STML(JMIN+1)-STML(JMIN))) GO
1 TO 39
KEY=1
JJ=JMIN
KK=JMIN+1
JMIN=JMIN+1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM21)
38 XL(KK)=(XL(JJ)+XL(KK))/2.0
YL(KK)=(YL(JJ)+YL(KK))/2.0
ZL(KK)=(ZL(JJ)+ZL(KK))/2.0
UABS(KK)=(UABS(JJ)+UABS(KK))/2.0
IF (IWRITE.LT.0) WRITE (JWRITE,NAM22)
IF (KEY.FQ.1) GO TO 39
GO TO 40
39 IF ((STML(JMAX)-STML(JMAX-3)).LT.8.*(STML(JMAX)-STML(JMAX-1))) GO
1 TO 40
KEY=2
KK=JMAX-1

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JJ=JMAX
JMAX=JMAX-1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM23)
GO TO 38
JMN=JMIN+1
JMX=JMAX-2
AF=1.
L=JMN
IF (IWRITE.LT.0) WRITE (JWRITE,NAM24)
IF (IWRITE.GT.1) GO TO 42
WRITE (JWRITE,41) NCP
FORMAT (///.37H0 LINE PASSING THROUGH QUADRILATERAL .14)
41 DO 46 J=JMN,JMX
42 IF ((STML(J+2)-STML(L-1)).LT.8.*(STML(J+1)-STML(L))) GO TO 45
IF (IWRITE.GT.1) GO TO 44
WRITE (JWRITE,43) XL(L),YL(L),ZL(L),XL(J+1),YL(J+1),ZL(J+1)
43 FORMAT (14H POINT DELETED.10X.3F12.5.10X.3F12.5)
44 STML(L)=(AF*STML(L)+STML(J+1))/(AF+1.)
XL(L)=(AF*XL(L)+XL(J+1))/(AF+1.)
YL(L)=(AF*YL(L)+YL(J+1))/(AF+1.)
ZL(L)=(AF*ZL(L)+ZL(J+1))/(AF+1.)
UABS(L)=(AF*UABS(L)+UABS(J+1))/(AF+1.0)
AF=AF+1.
IF (IWRITE.LT.0) WRITE (JWRITE,NAM25)
IF (L.LE.MID) MID=MID-1
GO TO 46
45 AF=1.
L=L+1
K=J+1
STML(L)=STML(K)
XL(L)=XL(K)
YL(L)=YL(K)
ZL(L)=ZL(K)
UABS(L)=UABS(K)
IF (IWRITE.LT.0) WRITE (JWRITE,NAM26)
46 CONTINUE
L=L+1
STML(L)=STML(JMAX)
XL(L)=XL(JMAX)
YL(L)=YL(JMAX)
ZL(L)=ZL(JMAX)
UABS(L)=UABS(JMAX)
  
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IF (IWRITE.LT.0) WRITE (JWRITE,NAM27)
JMAX=L
IF (IWRITE.GT.1) GO TO 48
WRITE (JWRITE,47)
47 FORMAT (3H0 1.6X.1HX.9X.1HY.9X.1HZ.13X.2HCP.8X.2HSL.7X.4HUABS)
48 K=0
LOHO=0
LOGO=0
IF ((JMAX-JMIN).LE.4) LOGO=1
DO 51 I=JMIN,JMAX
K=K+1
VOV(K)=UABS(I)
SS(K)=STML(I)
IF (LOGO.EQ.0) GO TO 49
SSTEST=1000.0
IF (K.GT.1) SSTEST=(SS(K)-SS(K-1))
IF (SSTEST.LF.0.0) LOHO=LOHO+1
IF (IWRITE.GT.1) GO TO 51
49 IF (IWRITE.GT.1) GO TO 51
C*** WRITE POINTS, VELOCITIES, & CP'S FOR THE STREAMLINE POINTS CALCULATED
CP=1.0-UABS(I)**2
WRITE (JWRITE,50) K,XL(I),YL(I),ZL(I),CP,STML(I),UABS(I)
50 FORMAT (1X,13,3F10.5,4X,3F10.5)
51 CONTINUE
IF (LOHO.GT.0) GO TO 52
CALL ROUTINE TO CALCULATE BOUNDARY LAYER OVER THE STREAMLINE
CALL BLCONT(K,IWRITE)
IF (ICANCL.NE.0) RETURN
K2=(MID-JMIN)*K+1
C*** HOLD THE DISPLACEMENT THICKNESS & THE WALL SHEAR VALUES AT THE
C*** CENTROID POINT FOR WHICH THE STREAMLINE WAS CALCULATED
SKIN(LL)=CFI(K2)
DSTAR(LL)=DELS(K2)
HSK=SKIN(LL)
HDS=DSTAR(LL)
GC TO 56
52 SKIN(LL)=HSK
DSTAR(LL)=HDS
WRITE (JWRITE,53) LL
53 FORMAT (1X,7.2X,6SHVALUES OF WALL SHEAR AND DISPLACEMENT THICKNESS
1 AT QUADRILATERAL, 13.40H WAS SET DUE TO STREAMLINE DIFFICULTIES..
1/)
GO TO 56

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54 WRITE (JWRITE,41) NCP
55 WRITE (JWRITE,55)
56 FORMAT (35H PROBABLE ERROR - LINE IS VERY LONG)
57 GC TO 35
58 CONTINUE
59 IWRITE=IWRITS
60 IF (II-2) 57,61,59
61 JEND=NEND-1
62 ESTIMATE DSTAR & SKIN FOR TRIANGLES AT THE NOSE AND TAIL OF BODY
63 DO 58 J=1,JEND,2
64 DSTAR(J)=DSTAR(J+1)/3.0
65 SKIN(J)=SKIN(J+1)/3.0
66 GO TO 61
67 JSTART=NSTART+1
68 DO 60 J=JSTART,NLIN,2
69 DSTAR(J)=DSTAR(J-1)
70 SKIN(J)=SKIN(J-1)
71 CONTINUE
72 END OF LOOP ON PANEL CENTROIDS EXCEPT TRIANGLES
73 WRITE (JWRITE,62)
74 FORMAT (///,1X,56H SUMMARY OF BOUNDARY LAYER INFORMATION FOR QUADRI
75 LATERALS//2X,5HNQUAD,6X,1HX,9X,1HY,9X,1HZ,11X,5H DSTAR,5X,4H SKIN//)
76 CDF=0.0
77 AREA=0.0
78 WRITE POINTS,DSTAR,& SKIN FOR EACH CENTROID. COMPUTE FRICTION CO
79 DC 64 J=1,NLIN
80 IF (SKIN(J).GT.900.0) SKIN(J)=0.0
81 WRITE (JWRITE,63) J,XCP(J),YCP(J),ZCP(J),DSTAR(J),SKIN(J)
82 FCFORMAT (4X,13,3F10.5,4X,2F10.5)
83 CDF=CDF-SKIN(J)*AQP(J)*VX1(J)/(0.5*VABS(J))
84 AREA=AREA+AQP(J)
85 CCNTINUE
86 AREA=AREA+AREA/NLIN
87 CCFA=2.0*CDF
88 CDF=CCFA/REFA
89 WRITE (JWRITE,65) CDF,REFA,REBODY,STOTAL
90 FCFORMAT (///,15X,25H FRICTION DRAG COEFFICIENT,/,13X,29(1H*),/17X,1
91 14H FRICTION CD = ,F11.5/,14X,17H REFERENCE AREA = ,F11.5/,13X,18H REY
92 INCLDS NUMBER = ,F11.4/17X,14H BODY LENGTH = ,F11.5/,13X,29(1H*),///
93 1)
94 REWIND KFILE3
95 REWIND KFILE4

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PF5 555  
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PF5 557  
PF5 558

```

REWIND KFILES
SUMA=0.0
AVXCG=0.0
AVAREA=0.0
AVDELS=0.0
NDC=NLIN-2*MM+4
CALCULATE AVERAGE DSTAR, AVERAGE PANEL AREA, AND AVERAGE X-ORDINATE
FOR THE THIRD STATION OF INPUT POINTS FROM THE END OF BODY. THESE
QUANTITIES ARE USED TO CALCULATE THE WAKE-BODY COORDINATES.
DO 66 I=ND0,NLIN,2
  AVXCG=AVXCG+XCP(I-1)*AQP(I-1)
  AVDELS=AVDELS+DSTAR(I-1)*AQP(I-1)
  AVAREA=AVAREA+AQP(I-1)
  SUMA=SUMA+AQP(I)
  AVDELS=AVDELS/AVAREA
  AVXCG=AVXCG/AVAREA
  SUMA=SUMA/(MM-1)
  AREA=AV*SQRT(AREA*AV*SUMA)
DO 67 I=1,NLIN
  XNH(I)=XNP(I)
  ZNH(I)=ZNP(I)
  AOPH(I)=AQP(I)
67 RETURN
68 WRITE (JWRITE,69) IS,NQ
69 FORMAT (14H TAPE 04 ERROR,2I4)
70 REWIND KFILE
70 RETURN
70 END

```

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```

SUBROUTINE BLCONT(KNP,IWRITE)
  BOUNDARY LAYER CONTROL ROUTINE WHICH CALLS LAMINR & TURB2, THE
  LAMINAR AND TURBULENT ROUTINES WHICH USE MOMENTUM INTEGRAL METHOD
  DIMENSION V(150),S(150),DUDS(150)
  COMMON /BOUND/TAW(150),HMEAN(150),NP
  COMMON /SPLN/VCOFF(4,75)
  COMMON /BL/VOV(75),SS(75),VIN,VO,ROE,DELS(150),CFI(150),THT(150),
  1 STOTAL,KKK
  COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE

```

```

15 COMMON /CANCEL/ICANCL,NODE
16
17 STRAN=.05
18 NP=KNP
19
20 SPLINE IS CALLED TO CURVE FIT THE STREAMLINE VALUES OF ABSOLUTE
21 VELOCITY VERSUS SURFACE DISTANCE FROM THE NCSE OF THE BODY
22 CALL SPLINE(NP,VOV,SS,0)
23 M=NP-1
24 SEND=SS(NP)
25 KKK=2
26 K=1
27 S(1)=SS(1)
28 V(1)=VOV(1)
29 DUDS(1)=VCOEF(3,1)
30 DO 1 I=1,M
31 H=(SS(I+1)-SS(I))/KKK
32 DC 1 J=1,KKK
33 K=K+1
34 S(K)=S(K-1)+H
35 V(K)=(VCOEF(1,1)*S(K)+VCOEF(2,1))*S(K)+VCOEF(3,1)*S(K)+VCOEF(4,1)
36
37 1 DUDS(K)=(3.0D0*VCOEF(1,1)*S(K)+2.0D0*VCOEF(2,1))*S(K)+VCOEF(3,1)
38 NPP=KKK*(NP-1)+1
39 CONTINUE
40 DC 2 I=1,NPP
41 S(I)=S(1)/STOTAL
42 DUDS(I)=DUDS(1)*STOTAL
43 CALL LAMINR(S,V,DUDS,STRAN,II,NPP,IWRITE)
44 IF (ICANCL.NE.0) RETURN
45 IF (I.EQ.NPP) GO TO 3
46 CALL TURB2(S,V,DUDS,SEND,II,NPP)
47 IF (IWRITE.GT.1) GO TO 5
48 WRITE (JWRITE,4)
49 FORMAT (/6X,1HS,13X,1HV,10X,4HDUDS,9X,5HHMEAN,8X,6HDELTA S,7X,6HTH
50 1FTAS,8X,3HTAW,9X,3HCFI/)
51 DO 6 I=1,NPP
52 S(I)=S(1)*STOTAL
53 V(I)=V(1)*VINP
54 DUDS(I)=DUDS(1)*VINP/STOTAL
55 DELS(I)=DELS(1)*STOTAL
56 IF (IWRITE.GT.1) RETURN

```

BLC	54
BLC	55
BLC	56
BLC	57
BLC	58
BLC	59

```

DO 7 I=1,NPP,KKK
7 WRITE (JWRITE,8) S(I),V(I),DUDS(I),HMEAN(I),DELS(I),THT(I),TAW(I),
1 CFI(I)
8 FORMAT (1X,8(F10.5,3X))
RETURN
END

```

```

C
SUBROUTINE LAMINR(X,UDEL,DUDX,XTRAN,II,NPP,IWRITE)
C*** CALCULATES LAMINAR BOUNDARY LAYER BY MOMENTUM INTEGRAL
C

```

```

DIMENSION X(150),UDEL(150),DUDX(150)
COMMON /BOUND/TAW(150),HMEAN(150),NP
COMMON /SPLN/VCOEF(4,75)
COMMON /BL/VOV(75),SS(75),VINP,VO,R3E,DELS(150),CFI(150),THT(150),
1STOTAL,KKK
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15
COMMON /CANCEL/ICANCL,NODE

```

```

II=1
H=X(II+1)-X(II)
IF (UDEL(II).LT.1.0E-06) GO TO 1
STARTING CONDITIONS ASSUMING FLAT PLATF
Z=0.0
THI(II)=0.0
DELS(II)=C.C
TAW(II)=5000.0
CFI(II)=1000.0
HMEAN(II)=2.554
II=2

```

[illegible]

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[illegible]

7.9



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      RETURN
      IF (IWRITE.GT.1) RETURN
      IK=II/KKK
      WRITE (JWRITE,9) TA(II),IK
      9 FORMAT (/,27H NEGATIVE VALUE OF TAWST = .E14.7,21H AT OR AFTER STA
      1 TION .13.19H ON THE STREAMLINE.,38H FOR MORE INFORMATION ON THE LO
      1 CATION.,/,108H OF LAMINAR SEPARATION USE IWRITE = 0 PRINT OPTION. T
      1 HE TURBULENT ROUTINE IS CALLED AT THE SEPARATION POINT.)
      RETURN
      END

```

LAM 76  
LAM 77  
LAM 78  
LAM 79  
LAM 80  
LAM 81  
LAM 82  
LAM 83  
LAM 84  
LAM 85

```

      SUBROUTINE FFK(AKD,FD,FID,F2D)
      C*** ROUTINE FOR NUMERICAL INTERPOLATION OF LAMINAR B.L. FUNCTIONS
      C
      DIMENSION AK(55),F(55),F1(55),F2(55)
      COMMON /INPUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
      15 COMMON /CANCEL/ICANCEL,NODE
      DATA AK/0.094815,0.094632,0.094083,0.093166,0.091882,0.090234,0.08
      18223,0.085855,0.083134,0.080068,0.076664,0.072930,0.068877,0.06451
      16,0.059857,0.054912,0.049697,0.044223,0.038506,0.032562,0.026405,0
      1,020054,0.013524,0.006833,0.000000,-0.006957,-0.014321,-0.021170,-
      13,028387,-0.035651,-0.042943,-0.050244,-0.057532,-0.064789,-0.0719
      195,-0.079129,-0.086171,-0.093104,-0.099906,-0.106558,-0.113043,-0.
      119341,-0.125434,-0.131304,-0.136935,-0.142309,-0.147411,-0.152224
      11,-0.156735,-0.160927,-0.164789,-0.168307,-0.171470,-0.174267,-0.17
      16687/
      DATA F/-0.094815,-0.093915,-0.091177,-0.086542,-0.079963,-0.071400
      1,-0.060818,-0.048195,-0.033512,-0.016759,0.002068,0.022964,0.04591
      19,0.070916,0.097532,0.126938,0.157897,0.190770,0.225538,0.262060,0
      1,300369,0.340371,0.391999,0.425181,0.469841,0.515896,0.563264,0.61
      11853,0.661571,0.712321,0.764004,0.816516,0.869752,0.923601,0.97795
      12,1.032691,1.087700,1.142862,1.198055,1.253157,1.308043,1.362589,1
      1,416665,1.470145,1.522902,1.574802,1.625719,1.675522,1.724079,1.77
      11259,1.816936,1.860975,1.903251,1.943633,1.981994/
      DATA F1/2.250000,2.250686,2.252684,2.255924,2.260349,2.265904,2.27
      12545,2.280231,2.288928,2.298609,2.309248,2.320828,2.333333,2.34675
      11,2.361073,2.376291,2.392406,2.409414,2.427320,2.446130,2.465849,2
      1,486485,2.508057,2.530574,2.554053,2.578518,2.603995,2.630480,2.65

```

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18031.2.686666.2.716418.2.747321.2.779412.2.812734.2.847327.2.88324
12.2.920529.2.959246.2.999447.3.041200.3.084570.3.129634.3.176471.3
1.225166.3.275810.3.328505.3.383357.3.440479.3.499999.3.562056.3.62
16788.3.694360.3.764940.3.838720.3.915905/
DATA F2/0.355556.0.355293.0.354515.0.353236.0.351470.0.349229.0.34
16528.0.343380.0.339800.0.335801.0.331397.0.326601.0.321428.0.31589
12.0.310005.0.303782.0.297237.0.290383.0.283234.0.275804.0.268107.0
1.260156.0.251966.0.243549.0.234921.0.226093.0.217082.0.207899.0.19
18559.0.189077.0.179464.0.169736.0.159906.0.149987.0.139995.0.12994
11.0.119841.0.109708.0.099555.0.089397.0.079247.0.069120.0.059028.0
1.048985.0.039007.0.029105.0.019294.0.009588.0.000000.0.009455.-0.
1018765.-0.027914.-0.036890.-0.045678.-0.054266/
IF (AKD.LE.AK(1)) GO TO 1
FD=F(1)
F1D=F1(1)
F2D=F2(1)
AKD=AK(1)
RETURN
1 IF (AKD.GT.AK(55)) GO TO 2
FD=F(55)
F1D=F1(55)
F2D=F2(55)
AKD=AK(55)
RETURN
2 DC 3 I=1.54
IF (AKD.LE.AK(1).AND.AK.GT.AK(I+1)) GO TO 5
3 CONTINUE
WRITE (JWRITE,4) AKD
4 FORMAT (1X,6HAKD = .E12.5,22H EXCEEDS ALLOWED RANGE)
1 CANCEL=1
RETURN
5 FD=F(1)+(F(I+1)-F(I))*(AKD-AK(I))/(AK(I+1)-AK(I))
F1D=F1(1)+(F1(I+1)-F1(I))*(AKD-AK(I))/(AK(I+1)-AK(I))
F2D=F2(1)+(F2(I+1)-F2(I))*(AKD-AK(I))/(AK(I+1)-AK(I))
RETURN
END

```

TRB 1  
TRB 2

SUBROUTINE TURB2(SUMS,UE,DUE DX,SEND,N1,NPP)

```

C**  ROUTINE FOR TURBULENT BOUNDARY LAYER USING MCMENTUM INTEGRAL
C
COMMON /BOUND/TAW(150),HMEAN(150),NP
COMMON /BL/VOV(75),SS(75),VINP,VO,ROE,DELS(150),CFI(150),THT(150),
1STOTAL,KKK
DIMENSION HVMEAN(2),SUMS(150),UE(150),DUEDX(150)

DC 1 L=N1,NPP
DUEDX(L)=VINP*DUEDX(L)/STOTAL
SUMS(L)=SUMS(L)+STOTAL
UE(L)=VINP*UE(L)
THT(N1)=THT(N1)+STOTAL
DELS(N1)=1.45*THT(N1)
C1=0.56
C2=1.667
C3=1.65
C4=0.246
C5=0.678
C6=0.268
HMEAN(N1)=1.45
HVMEAN(1)=1.269*HMEAN(N1)/(HMEAN(N1)-.379)
F1=3.+2.*C2
E2=1.+C2
E3=3.+3.*C2
T1=0.02*C1/C3*E2
IREG=N1+1
DO 7 I=IBFG,NPP
HMEAN(I)=0.0
HVMEAN(2)=0.0
UETR=(UE(I-1)/UE(I))*E3
UEINT=0.5*(SUMS(I)-SUMS(I-1))*UE(I)*UE(I-1)+UE(I-1)*E1
THT(I)=(THT(I-1))*F2*UFIR+T1*VO**C2/(UE(I))*E3*UEINT)**(1./E2)
TERMA=(0.02*C1)/(UE(I)*THT(I)/VO)**C2*1.1
T2=THT(I)/UE(I)*DUEDX(I)
HF=HMFAN(I-1)
HV=HVMEAN(I)
DO 6 J=1,6
TERMB=-HV*C4*10.0**(-C5*HH)*(UE(I)*THT(I)/VO)**(-C6)
TERMC=TERMB/2.
TERMD=(HH-1.1)*HV*T2
DHVDX=(TERMA+TERMB+TERMC)/THT(I-1)
HVTIR=HVMEAN(1)+DHVDX*(SUMS(I)-SUMS(I-1))

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TRB 44

```

45 IF (HVITR-1.85) 3.2.2
46 HVITR=1.85
47 IF (HVITR-1.55) 4.4.5
48 HVITR=1.55
49 HVITR=0.379*HVITR/(HVITR-1.269)
50 HVMEAN(2)=HVMEAN(2)+HVITR
51 HVMEAN(1)=HVMEAN(1)+HVITR
52 HV=HVITR
53 H=HVITR
54 HVMEAN(1)=HVMEAN(2)/6
55 HVMEAN(1)=HVMEAN(1)/6
56 DELS(1)=THI(1)*HMEAN(1)
57 CFI(1)=C4*10.0*(-C5*HMEAN(1))*(UE(1)*THI(1)/VO)*(-C6)*(UE(1)/VIN
58 1F)*2
59 TANI=CFI(1)*0.5*ROE*VIN*VINF
60 IF (SFND-SUMS(1)) 8.8.7
61 CCNTINUE
62 DO 9 L=N1,NP
63 DELS(L)=DELS(L)/STOTAL
64 TH(L)=TH(L)/STOTAL
65 DUEX(L)=DUEX(L)*STOTAL/VINF
66 SUMS(L)=SUMS(L)/STOTAL
67 UE(L)=UE(L)/VINF
68 RETURN
69 END

```

```

1 SUBROUTINE RGVRTX(XC,YC,ZC,X0,Y0,Z0,RD,NTHETA,THEIA,PHI,VVPHI,NRS,
2 INSRV,VX,VY,VZ,IM,NPTS)
3
4 C**
5 C** SUBROUTINE RGVRTX CALCULATES THE INDUCED VELOCITIES DUE TO THE
6 C** RING VORTICES
7
8 DIMENSION XC(40),YC(40),ZC(40),RD(40),NTHETA(40),THEIA(40),PHI(40)
9 1.NVPHI(40),NRS(40),UC(360),VC(360),TX(360),NPTS(40)
10
11 C**
12 C** DEFINE INITIAL PARAMETERS
13 PI=3.1415927
14 C=1.0/(4.0*PI)
15 VXX=0.0
16 VYY=0.0

```

```

C***
VZZ=0.0
SET UP LOOP OVER SYSTEMS OF VORTICES
DO 8 L=1,NSRV
  TINC=2.0*PI/FLOAT(NTHETA(L)-1)
  NR=NRS(L)
  ISFE=0
  IF (NPTS(L).EQ.0.AND.NRS(L).EQ.1) ISEE=1
  DC 7 M=1,NR
    DETERMINE RADIAL STATION AND CIRCULATION
    IF (ISEE.EQ.0) GO TO 1
    GAMMA=CIRC(L)
    R=RD(L)
    DR=R
    GO TO 2
  1 R=F(NR,M,RD(L),DR)
    XR=R/RD(L)
    GAMMA=G(L,XR)
    T=THETA(L)
    PHX=PHI(L)
    NTH=NTHEA(L)
    TEST FOR FLOW SIMPLICATION BY DOUBLET
    TEST=SQRT((X0-XC(L))**2+(Y0-YC(L))**2+(Z0-ZC(L))**2)
    FACTOR=1.5
    DISX=FACTOR*(2.0*RD(L))
    IF (TEST.LT.DISX) GO TO 3
    FACX=0.00932
    CALCULATE DOUBLET STRENGTH AND FLOW
    GAM=FACTX*GAMMA*NR**2
    CALL DBLET(NVPHI,R,T,PHX,GAM,L,X0,Y0,Z0,XC,YC,ZC,VX,VY,VZ)
    IM=1
    GO TO 6
  3 DC 5 I=1,NTH
    DEFINE PARAMETRIC EQNS FOR POINT ON VORTEX RING
    XI=XC(L)+R*SIN(T)*COS(PHX)
    ETA=YC(L)+R*SIN(T)*SIN(PHX)
    ZETA=ZC(L)+R*COS(T)
    DEFINE DERIVATIVES OF PARAMETRIC EQNS WRT T
    DXI=R*COS(T)*COS(PHX)
    DETA=R*COS(T)*SIN(PHX)
    DZETA=-R*SIN(T)
    INITIALIZE OR DEFINE PARAMETER
    TX(I)=T
  
```

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UC(I)=0.0
VC(I)=0.0
WC(I)=0.0
C**  CCMPUTE DISTANCE FROM FILAMENT TO ARBITRARY POINT
RHO=SQRT((XI-X0)**2+(ETA-Y0)**2+(ZETA-Z0)**2)
IF (RHO.LE.1.0E-10) GO TO 4
C**  COMPUTE VELOCITY CONTRIBUTIONS AROUND THE RING VORTEX UPON AN
C**  ARBITRARY POINT
DENOM=RHO**3*RD(L)/((C*DR)
UC(I)=(DETA*(Z0-ZETA)-DXI*(Y0-ETA))/DENOM*GAMMA
VC(I)=(DZETA*(X0-XI)-DXI*(Z0-ZETA))/DENOM*GAMMA
WC(I)=(DXI*(Y0-ETA)-DETA*(X0-XI))/DENOM*GAMMA
4 IF (I.EQ.NTH) GO TO 5
T=T+TINC
IF (NVPHI(L).NE.0)PHX=PHX+TINC
5 CONTINUE
C**  INTEGRATE TO FIND VX, VY, VZ
IM=0
CALL TRAP(NTH,IX,UC,VX)
CALL TRAP(NTH,IX,VC,VY)
CALL TRAP(NTH,IX,WC,VZ)
6 VXX=VXX+VX
VYY=VYY+VY
VZZ=VZZ+VZ
7 CONTINUE
8 CCNTINE TOTAL INDUCED VELOCITY COMPONENTS
C**  VX=VXX
VY=VYY
VZ=VZZ
MODIFY, IF NECESSARY, FOR PRECISION PROBLEMS
C**  VMX=ABS(VX)
IF (ABS(VY).GT.VMX)VMX=ABS(VY)
IF (ABS(VZ).GT.VMX)VMX=ABS(VZ)
FVMX=1.0E-4*VMX
IF (ABS(VX).LT.FVMX)VX=0.0
IF (ABS(VY).LT.FVMX)VY=0.0
IF (ABS(VZ).LT.FVMX)VZ=0.0
RETURN
END

```

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1 2 3 4 5 6 7 8 9 10 11  
F F F F F F F F F F F

C\*\*\*  
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C  
FUNCTION F(N,M,R,RD)  
FUNCTION F CALCULATES THE RADIAL STATION OF THE VORTEX RING  
RD=R/FLJAT(N)  
RX=R+RD  
DO 1 I=1,M  
1 RX=RX-RD  
F=RX  
RETURN  
END

1 2 3 4 5 6 7 8 9  
G G G G G G G G G

C\*\*\*  
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C  
FUNCTION G(L,R)  
FUNCTION G COMPUTES THE CIRCULATION AS A FUNCTION OF RADIAL  
DISTANCE FROM THE VORTEX'S CENTER  
CALL GAMMA(L,R,B)  
G=B  
RETURN  
END

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CIR

C\*\*\*  
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C  
FUNCTION CIRC(L)  
FUNCTION CIRC SETS THE VORTEX STRENGTH  
COMMON /S2V/CIRCV(40)  
CIRC=CIRCV(L)  
RETURN  
END

1 2 3  
SPN  
SPN  
SPN

C\*\*\*  
C  
SUBROUTINE SPLINE(N,Y,X,IC)  
THIS SUBROUTINE PERFORMS A SPLINE FIT ON THE TABULATED

```

C***      DATA Y VS. X. THE SPLINE FIT PROVIDES A CURVE FIT OF THE
C***      TABULATED DATA THAT HAS A CONTINUOUS FIRST DERIVATIVE. THE
C***      FORM OF THE CURVE FIT IS
C***      Y = AA(1,1)*X**3 + AA(2,1)*X**2
C***      + AA(3,1)*X + AA(4,1)
C***      FOR
C***      N      X(1) <= X <= X(I+1).
C***      Y      - NUMBER OF TABULATED DATA POINTS
C***      X      - TABULATED FUNCTION VALUES
C***      AA      - TABULATED ARGUMENT VALUES
C***      - ARRAY OF COEFFICIENTS OF THE CUBIC POLYNOMIAL
C***      SPLINE FIT. DIMENSIONS OF AA ARE 4 BY N-1.
C***      REFERENCE FOR THIS METHOD IS
C***      J.H. AHLBERG, ET AL. ACADEMIC PRESS, NEW YORK, 1967
C***      DIMENSION H(75), Q(75), U(75), X(N), Y(N), CF(40,4,50)
C***      COMMON /SPLN/AA(4,75)
C***
C***      NM1=N-1
C***      DO 1 I=1,NM1
C***      H(I)=X(I+1)-X(I)
C***      IF IC=0, SFT SECOND DERIVATIVE TO ZERO FOR LEFT HAND END CONDITION
C***      Q(1)=0.0
C***      U(1)=0.0
C***      IF (IC.FQ.0) GO TO 2
C***      MODIFIED LEFT HAND END CONDITION THAT ALLEVIATES THE NEED
C***      TO SPECIFY THE X-DERIVATIVE OF Y AT POINT 1
C***      Q(1)=-31.0/32.0
C***      H1=H(1)
C***      H2=H(2)
C***      H3=H(3)
C***      U(1)=Y(1)*(32.0*H1+42.0*H2+21.0*H3)/(H1+H2)/(H1+H2+H3)-Y(2)*(11.0*
C***      H1+42.0*H2+21.0*H3)/(H2+H3)/H2+Y(3)*H1*(11.0*H1+21.0*H2+H3)/(H1+
C***      H2)/H2/H3-Y(4)*H1*(11.0*H1+21.0*H2)/(H2+H3)/(H1+H2+H3)/H3
C***      U(1)=3.0*U(1)/H1/16.0
C***      GENERATE INTERNAL U(I) BY ALGORITHM GIVEN BY AHLBERG
C***      2 HM=H(1)
C***      YV=Y(2)
C***      YN=Y(1)
C***      DC 3 I=2,NM1
C***      HP=H(1)
C***      YP=Y(I+1)

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46 SPN 46
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55 SPN 55
56 SPN 56
57 SPN 57
58 SPN 58
59 SF 59
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84 SPN 84
85 SPN 85
86 SPN 86
87 SPN 87

D=3.0*((YP-YY)/HH-(YY-YM)/HM)/(HH+HM)
C=0.5*HH/(HH+HM)
A=0.5-C
P=A*Q(I-1)+1.0
Q(I)=-C/P
U(I)=(D-A*U(I-1))/P
HM=HH
YM=YY
3 YY=YP
*** MODIFIED RIGHT HAND END CONDITION THAT ALLEVIATES THE NEED
*** TO SPECIFY THE X-DERIVATIVE OF Y AT POINT N
A=31.0/32.0
P=A*Q(N-1)+1.0
H1=H(NM1)
H2=H(NM1-1)
H3=H(NM1-2)
D=Y(N)*(32.0*H1+42.0*H2+21.0*H3)/(H1+H2)/(H1+H2+H3)-Y(NM1)*(11.0*H
11+42.0*H2+21.0*H3)/(H2+H3)/H2+Y(NM1-1)*H1*(11.0*H1+21.0*(H2+H3))/
1H1+H2)/H2/H3-Y(NM1-2)*H1*(11.0*H1+21.0*H2)/(H2+H3)/(H1+H2+H3)/H3
D=3.0*D/H1/16.0
U(N)=(D-A*U(N-1))/P
SOLVE FOR THE SPLINE COEFFICIENTS CORRESPONDING TO AHLBERG'S
M(0) TO M(N) AND STORE THEM IN THE U(I).
DO 4 J=1,NM1
I=N-J
4 U(I)=Q(I)*U(I+1)+U(I)
*** FORM THE AA(J,I) COEFFICIENTS FOR THE CONVENTIONAL FORM OF
*** A CUBIC POLYNOMIAL FROM THE U(I)
UU=U(I)
XX=X(I)
YY=Y(I)
DO 5 I=1,NM1
UP=U(I+1)
XP=X(I+1)
YP=Y(I+1)
HM=H(I)
AA(1,I)=(UP-UU)/HH/6.0
AA(2,I)=3.5*(XP*UU-XX*UP)/HH
AA(3,I)=9.5*(UP*XX*XX-UU*XP*XP)/HH+(UU-UP)*HH/6.0+(YP-YY)/HH
AA(4,I)=(UU*XP*XP-UP*XX*XX)/HH/6.0+(UF*XX-UU*XP)*HH/6.0+(YY*
1XP-YP*XX)/HH
XX=XP

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SPN 106

TRP 1  
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TRP 18

```

UU=UP
5 YY=YP
  IF (IC.EQ.0) GO TO 7
  DO 6 I=1,NM1
    DO 6 J=1,4
      CF(IC,J,I)=AA(J,I)
  7 RETURN

C
  ENTRY GAMMA(IC,T,Z)
  IF (T.GT.X(1)) GO TO 8
  I=1
  GO TO 10
  8 DO 9 I=1,NM1
    IF (X(I).LE.T.AND.X(I+1).GT.T) GO TO 10
  9 CCNTINUE
  I=NM1
  10 Z=((CF(IC,1,I)*T+CF(IC,2,I))*I+CF(IC,3,I))*I+CF(IC,4,I)
  RETURN
  END

```

```

SUBROUTINE TRAP(ND,X,DY,Y)
C*** SUBROUTINE TRAP PERFORMS TRAPEZOIDAL INTEGRATION
C
C
C DIMENSION X(ND),DY(ND)
C
C*** INITIALIZE PARAMETER
S2=0.0
IF (ND-1) 4,3,1
C*** INTEGRATE OVER INTERVAL AND SUM
  1 DC 2 I=2,ND
    S1=S2
    S2=S2+0.5*(X(I)-X(I-1))*(DY(I)+DY(I-1))
  2 CCNTINUE
  3 Y=S2
  4 RETURN
  END

```

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1 DBL  
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39 DBL

```

SUBROUTINE DBLET(N,R,T,PHX,GAM,L,X0,Y0,Z0,XC,YC,ZC,VX,VY,VZ)
SUBROUTINE DBLET CALCULATES DOUBLET FLOW
DIMENSION N(40),XC(40),YC(40),ZC(40)
PI=3.1415927
DETERMINE DOUBLET AXIS VECTOR
X1=R*SIN(T)*COS(PHX)
Y1=R*SIN(T)*SIN(PHX)
Z1=R*COS(T)
PI2=0.5*PI
X2=R*SIN(T+PI2)*COS(PHX+N(L)*PI2)
Y2=R*SIN(T+PI2)*SIN(PHX+N(L)*PI2)
Z2=R*COS(T+PI2)
X3=Y1*Z2-Z1*Y2
Y3=Z1*X2-X1*Z2
Z3=X1*Y2-Y1*X2
RD=SQRT(X3**2+Y3**2+Z3**2)
X3=X3/RD
Y3=Y3/RD
Z3=Z3/RD
DETERMINE DOUBLET STRENGTH VECTOR COMPONENTS
XMU=GAM*X3
YMU=GAM*Y3
ZMU=GAM*Z3
PI4=-0.5*PI2
DETERMINE DOUBLET-TO-ARBITRARY POINT VECTOR
X1=X0-XC(L)
Y1=Y0-YC(L)
Z1=Z0-ZC(L)
DETERMINE VELOCITY COMPONENTS
RD=X1**2+Y1**2+Z1**2
F=PI4/RD**1.5
VX=F*XMU*(1.0-3.0*X1**2/RD)
VY=F*YMU*(1.0-3.0*Y1**2/RD)
VZ=F*ZMU*(1.0-3.0*Z1**2/RD)
RETURN
END

```

```

1 SUBROUTINE SPACE(NSRV,SVV,XCV,NMIN,NMAX,X,MNAX,XCRP,AEXP,XRM,ISPAC
2 1E,FXMR,XMR)
3 SPC
4 C*** SUBROUTINE SPACE CALCULATES VORTEX LOCATION VIA EXPONENTIAL
5 C*** FUNCTION
6 C
7 DIMENSION SVV(31,2),XCV(40),X(650),XCRP(2),AEXP(2)
8 SPC
9 C
10 MAX=(NMAX-1)*(MMAX-1)
11 NMAXM1=NMAX-1
12 SPC
13 C*** SET MAXIMUM RADIUS
14 RMX=RXMR
15 C
16 C*** GUESS A LOCATION
17 J=1
18 IF (XCV(JV-1).LT.XMR)J=2
19 XCV(JV)=XCV(JV-1)-XCRP(J)
20 LPT=1
21 SPC
22 C*** SCAN N-STATIONS
23 DO 2 JN=NMIN,NMAXM1
24 LC1=JN
25 IF (XCV(JV).LE.X(LPT).AND.XCV(JV).GE.X(LPT+MMAX)) GO TO 3
26 LPT=LPT+MMAX
27 IF (ISPAC.EQ.2) GO TO 4
28 JV=JV-1
29 GO TO 5
30 C*** COMPUTE EXPONENTIAL LOCATION
31 RXTL=(X(LPT)-XCV(JV))/(X(LPT)-X(LPT+MMAX))
32 R=SVV(LC1,2)+RXTL*(SVV(LC2,2)-SVV(LC1,2))
33 XCV(JV)=XCV(JV-1)-XCRP(J)*EXP(-AEXP(J))*(R-RMX)/RMX
34 IF (XCV(JV).LE.X(MAX).AND.ISPACE.EQ.1.OR.JV.EQ.40) GO TO 5
35 GO TO 1
36 F=0.0
37 XCV(JV)=XCV(JV-1)-XCRP(J)*EXP(-AEXP(J))*(R-RMX)/RMX
38 IF (XCV(JV).GT.XRM.AND.JV.LT.40) GO TO 1
39 NSRV=JV
40 RETURN
41 END

```

# SAMPLE INPUT - FLOWBODY

13  
BEST CESSNA 182 WITH M=21 AND N=29 YIELDING 550 PANELS -- FUSELAGE ONLY 155.0F0  
160.00E0 0.00016E0 0.002378E0 .240E0  
18000E+05 .252525E-06 110000E+06  
520.0E0 0.50E0 2 0 0

1.0 500 1 2 3.5 4.0 -0.3 -0.05 -18.0 4 21  
12.8 3.00 3.00 2.5 3.0 90.0 360 0 0  
0.16 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0  
0.05 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5  
0.15 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5 5.0  
0.25 2.0 2.5 3.0 3.5 4.0 4.5 5.0 5.5 6.0  
0.35 2.5 3.0 3.5 4.0 4.5 5.0 5.5 6.0 6.5  
0.45 3.0 3.5 4.0 4.5 5.0 5.5 6.0 6.5 7.0  
0.55 3.5 4.0 4.5 5.0 5.5 6.0 6.5 7.0 7.5  
0.65 4.0 4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0  
0.75 4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5  
0.85 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0  
0.95 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5  
1.0 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

CIRCULATION DISTRIBUTION

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12.2045000 0.0000000 -0.4271002 1 2 3 1 1  
12.2045000 0.0000000 -0.4271002 1 3 4 1 1  
12.2045000 0.0000000 -0.4271002 1 4 5 1 1  
12.2045000 0.0000000 -0.4271002 1 5 6 1 1  
12.2045000 0.0000000 -0.4271002 1 6 1 1 1

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12.2085000	0.0000000	-0.4271002	9
12.2085000	0.0000000	-0.4271002	10
12.2085000	0.0000000	-0.4271002	11
12.2085000	0.0000000	-0.4271002	12
12.2085000	0.0000000	-0.4271002	13
12.2085000	0.0000000	-0.4271002	14
12.2085000	0.0000000	-0.4271002	15
12.2085000	0.0000000	-0.4271002	16
12.2085000	0.0000000	-0.4271002	17
12.2085000	0.0000000	-0.4271002	18
12.2085000	0.0000000	-0.4271002	19
12.2085000	0.0000000	-0.4271002	20
12.2085000	0.0000000	-0.4271002	21
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11.5418000	0.3583000	-1.5279990	3
11.5418000	0.5146000	-1.4439990	4
11.5418000	0.6708000	-1.3499990	5
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11.5418000	0.9688000	-1.1270990	7
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11.5418000	1.2433000	-0.8456990	9
11.5418000	1.3616000	-0.6520090	10
11.5418000	1.5707990	-0.4271002	11
11.5418000	1.5625000	-0.0728990	12
11.5418000	1.4917000	0.3223990	13
11.5418000	1.3291990	0.5229000	14
11.5418000	1.1062000	0.0729000	15
11.5418000	0.8833000	0.7566002	16
11.5418000	0.6667000	0.7708990	17
11.5418000	0.4437000	0.7771000	18
11.5418000	0.2167000	0.7813005	19
11.5418000	0.0000000	-0.7813005	20
10.8755000	0.0000000	-1.9229990	1
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10.8755000	0.6625000	-1.7103000	4
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10.8755000	1.0854000	-1.3542000	6

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10.8755000	1.6457990	-0.5103998	1
10.8755000	1.6667000	-0.2521000	1
10.8755000	1.6562300	0.0187998	1
10.8755000	1.6042300	0.2979002	1
10.8755000	1.4792000	0.5521002	1
10.8755000	1.2561990	0.7396002	1
10.8755000	1.0207990	0.8354006	1
10.8755000	0.7708000	0.8646002	1
10.8755000	0.5146000	0.8853998	1
10.8755000	0.2500000	0.8979006	1
10.8755000	0.0000000	0.9063005	1
10.8755000	0.0000000	-2.1146000	1
10.8755000	0.2437000	-2.1146000	1
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10.8755000	0.7646000	-2.0562000	1
10.8755000	1.3375000	-1.9812000	1
10.8755000	1.2749000	-1.8374990	1
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10.8755000	1.6183000	-1.3750000	1
10.8755000	1.6833000	-1.1041000	1
10.8755000	1.7124000	-0.8228000	1
10.8755000	1.7292000	-0.5521002	1
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10.8755000	0.8292000	0.9313002	1
10.8755000	0.5583000	0.9688005	1
10.8755000	0.2750000	0.9979000	1
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7-7045030	1.6499990	-1.8604000	6	1
7-7045030	1.8322990	-1.5311990	7	1
7-7045030	1.9483000	-1.1771000	8	1
7-7045030	1.9167000	-0.8228958	9	1
7-7045030	1.9167000	-0.5321000	10	1
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ORIGINAL PAGE 14  
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**SAMPLE OUTPUT - FLOWBODY**

[illegible]

# DESIGNATION OF NORMAL VELOCITY ON QUADRANTS

1	2	1	2	PANEL	1	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
2	3	1	2	PANEL	2	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
3	4	1	2	PANEL	3	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
4	5	1	2	PANEL	4	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
5	6	1	2	PANEL	5	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
6	7	1	2	PANEL	6	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
7	8	1	2	PANEL	7	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
8	9	1	2	PANEL	8	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
9	10	1	2	PANEL	9	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
10	11	1	2	PANEL	10	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
11	12	1	2	PANEL	11	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
12	13	1	2	PANEL	12	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
13	14	1	2	PANEL	13	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
14	15	1	2	PANEL	14	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
15	16	1	2	PANEL	15	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
16	17	1	2	PANEL	16	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
17	18	1	2	PANEL	17	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
18	19	1	2	PANEL	18	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
19	20	1	2	PANEL	19	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.
20	21	1	2	PANEL	20	HAS BEEN DESIGNATED TO HAVE A NEGATIVE INWARD NORMAL COMPONENT OF VELOCITY.

PROBABLY ERROR IN INPUT - BUILD ANGLE = 10.143

## INWARD VELOCITY BY RING VERTICES AT ORIGINAL BODY PANEL CENTROID

PANEL NUMBER	PANEL CENTROID LOCATION	VELOCITY COMPONENTS
1	2	3
1	1.184170E+01	0.189711E+02
2	1.184170E+01	1.020017E+02
3	1.184170E+01	1.000220E+02
4	1.184170E+01	2.000000E+01
5	1.184170E+01	2.000000E+01
6	1.184170E+01	2.000000E+01
7	1.184170E+01	2.000000E+01
8	1.184170E+01	2.000000E+01
9	1.184170E+01	2.000000E+01
10	1.184170E+01	2.000000E+01
11	1.184170E+01	2.000000E+01
12	1.184170E+01	2.000000E+01
13	1.184170E+01	2.000000E+01
14	1.184170E+01	2.000000E+01
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21	1.184170E+01	2.000000E+01
22	1.184170E+01	2.000000E+01
23	1.184170E+01	2.000000E+01
24	1.184170E+01	2.000000E+01
25	1.184170E+01	2.000000E+01

## SOURCE DENSITY SOLUTION

ONLY GEOMETRY IS WITH PANEL AND BODY YIELDING TO PANELS -- PUSHLAGE ONLY

1 VELOCITY=1.0 2 VELOCITY=0.0 3 VELOCITY=0.0

### ITERATIVE MATRIX SOLUTION INFORMATION

ITERATION	SUM OF CHANGES	A	B1	B2
1	0.100000E+01			
2	0.100000E+01			
3	0.100000E+01			
4	0.100000E+01			
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21	0.100000E+01			
22	0.100000E+01			
23	0.100000E+01			
24	0.100000E+01			
25	0.100000E+01			

A EXTRAPOLATION  
0.100000E+01 0.100000E+01 0.100000E+01

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COMPUTATION OF VELOCITIES AND PRESSURE COEFFICIENTS AT THE PANEL CENTROID

**BEST DESIGN FOR WITH MORE AND MORE TILTING BOX PANELS - PACKAGE ONLY**

PAGE 2

[illegible][illegible]

### RESERVE LIST AND SPAG COMPONENTS

[illegible]

DT	100	200	300	400	500	600	700	800	900	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	2000	2100	2200	2300	2400	2500	2600	2700	2800	2900	3000	3100	3200	3300	3400	3500	3600	3700	3800	3900	4000	4100	4200	4300	4400	4500	4600	4700	4800	4900	5000	5100	5200	5300	5400	5500	5600	5700	5800	5900	6000	6100	6200	6300	6400	6500	6600	6700	6800	6900	7000	7100	7200	7300	7400	7500	7600	7700	7800	7900	8000	8100	8200	8300	8400	8500	8600	8700	8800	8900	9000	9100	9200	9300	9400	9500	9600	9700	9800	9900	10000	10100	10200	10300	10400	10500	10600	10700	10800	10900	11000	11100	11200	11300	11400	11500	11600	11700	11800	11900	12000	12100	12200	12300	12400	12500	12600	12700	12800	12900	13000	13100	13200	13300	13400	13500	13600	13700	13800	13900	14000	14100	14200	14300	14400	14500	14600	14700	14800	14900	15000	15100	15200	15300	15400	15500	15600	15700	15800	15900	16000	16100	16200	16300	16400	16500	16600	16700	16800	16900	17000	17100	17200	17300	17400	17500	17600	17700	17800	17900	18000	18100	18200	18300	18400	18500	18600	18700	18800	18900	19000	19100	19200	19300	19400	19500	19600	19700	19800	19900	20000	20100	20200	20300	20400	20500	20600	20700	20800	20900	21000	21100	21200	21300	21400	21500	21600	21700	21800	21900	22000	22100	22200	22300	22400	22500	22600	22700	22800	22900	23000	23100	23200	23300	23400	23500	23600	23700	23800	23900	24000	24100	24200	24300	24400	24500	24600	24700	24800	24900	25000	25100	25200	25300	25400	25500	25600	25700	25800	25900	26000	26100	26200	26300	26400	26500	26600	26700	26800	26900	27000	27100	27200	27300	27400	27500	27600	27700	27800	27900	28000	28100	28200	28300	28400	28500	28600	28700	28800	28900	29000	29100	29200	29300	29400	29500	29600	29700	29800	29900	30000	30100	30200	30300	30400	30500	30600	30700	30800	30900	31000	31100	31200	31300	31400	31500	31600	31700	31800	31900	32000	32100	32200	32300	32400	32500	32600	32700	32800	32900	33000	33100	33200	33300	33400	33500	33600	33700	33800	33900	34000	34100	34200	34300	34400	34500	34600	34700	34800	34900	35000	35100	35200	35300	35400	35500	35600	35700	35800	35900	36000	36100	36200	36300	36400	36500	36600	36700	36800	36900	37000	37100	37200	37300	37400	37500	37600	37700	37800	37900	38000	38100	38200	38300	38400	38500	38600	38700	38800	38900	39000	39100	39200	39300	39400	39500	39600	39700	39800	39900	40000	40100	40200	40300	40400	40500	40600	40700	40800	40900	41000	41100	41200	41300	41400	41500	41600	41700	41800	4190
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901	-0.01207	0.07009	0.00418	-0.00499	0.17281	-0.05906	-0.07739	0.182	-0.0079066	0.0150609	0.01
902	-0.01061	0.00909	0.00712	-0.00210	0.01701	-0.01290	-0.00000	0.131	-0.0369364	0.0113708	0.01
925	-0.00192	0.00191	0.00712	-0.00197	0.10197	-0.00700	-0.00000	0.107	-0.1019060	0.0110000	0.01
904	-0.10321	0.00208	0.00702	-0.00726	0.10128	-0.00331	-0.00702	0.137	-0.0070200	0.0100000	0.01
905	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
906	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
907	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
908	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
909	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
910	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
911	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
912	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
913	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
914	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
915	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
916	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
917	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
918	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
919	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
920	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
921	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
922	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
923	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
924	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
925	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
926	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
927	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
928	-0.00000	0.00000	0.00000	0.00000	0.00000	-0.00000	-0.00000	0.000	-0.0000000	0.0000000	0.00
929	-0.00000	0.									

\*\*\* CALCULATION OF INTERIOR PRESSURE COEFFICIENTS AND NORMAL VELOCITIES \*\*\*  
 AVERAGE CP ON INLET PANELS = 7.022220E-01 INLET AREA = 7.750770E-01  
 AVERAGE CP ON EXHAUST PANELS = 1.000072E-01 EXHAUST AREA = 1.000072E-01  
 CPE = 0.000072E-01  
 CPHE = 1.000072E-01  
 ADJUSTMENT FOR HEATING OF FLOOR TEMPERATURE RATIO = 7.700000E-01  
 EFFECTIVE EXHAUST AREA = 1.070000E-01

CPE = 0.000000E-01  
 CPHE = 1.000000E-01  
 NORMAL VELOCITY AT PANEL 1 = -0.100012E+00  
 NORMAL VELOCITY AT PANEL 5 = -0.201021E+00  
 NORMAL VELOCITY AT PANEL 7 = -0.200030E+00  
 NORMAL VELOCITY AT PANEL 9 = -0.210017E+00  
 NORMAL VELOCITY AT PANEL 11 = -0.270070E+00  
 NORMAL VELOCITY AT PANEL 12 = -0.121047E+00  
 NORMAL VELOCITY AT PANEL 15 = -0.270030E+00  
 NORMAL VELOCITY AT PANEL 115 = 0.000000E+00  
 NORMAL VELOCITY AT PANEL 117 = 0.370000E+00  
 NORMAL VELOCITY AT PANEL 119 = 0.301001E+00

ORIGINAL PAGE IS  
 OF POOR-QUALITY

# STRESS DENSITY SOLUTION

REST CASES (NO BATH MODE) AND MODS YIELDING 500 PANELS - FUSELAGE ONLY

X VELOCITY=1.0 Y VELOCITY=0.0 Z VELOCITY=0.0

## ITERATIVE MATRIX SOLUTION INFORMATION

ITERATION	SUM OF CHANGES	A	B1	B2
1	0.02070E+01			
2	0.02070E+01			
3	0.02070E+01			
4	0.02070E+01			
5	0.02070E+01			
6	0.02070E+01			
7	0.02070E+01			
8	0.02070E+01			
9	0.02070E+01			
10	0.02070E+01			
11	0.02070E+01			
12	0.02070E+01			
13	0.02070E+01			
14	0.02070E+01			
15	0.02070E+01			
16	0.02070E+01			
17	0.02070E+01			
18	0.02070E+01			
19	0.02070E+01			
20	0.02070E+01			
21	0.02070E+01			
22	0.02070E+01			
23	0.02070E+01			
24	0.02070E+01			
25	0.02070E+01			
26	0.02070E+01			
27	0.02070E+01			
28	0.02070E+01			
29	0.02070E+01			
30	0.02070E+01			
31	0.02070E+01			
32	0.02070E+01			
33	0.02070E+01			
34	0.02070E+01			
35	0.02070E+01			
36	0.02070E+01			
37	0.02070E+01			
38	0.02070E+01			
39	0.02070E+01			
40	0.02070E+01			
41	0.02070E+01			
42	0.02070E+01			
43	0.02070E+01			
44	0.02070E+01			
45	0.02070E+01			
46	0.02070E+01			
47	0.02070E+01			
48	0.02070E+01			
49	0.02070E+01			
50	0.02070E+01			
51	0.02070E+01			
52	0.02070E+01			
53	0.02070E+01			
54	0.02070E+01			
55	0.02070E+01			
56	0.02070E+01			
57	0.02070E+01			
58	0.02070E+01			
59	0.02070E+01			
60	0.02070E+01			
61	0.02070E+01			
62	0.02070E+01			
63	0.02070E+01			
64	0.02070E+01			
65	0.02070E+01			
66	0.02070E+01			
67	0.02070E+01			
68	0.02070E+01			
69	0.02070E+01			
70	0.02070E+01			
71	0.02070E+01			
72	0.02070E+01			
73	0.02070E+01			
74	0.02070E+01			
75	0.02070E+01			
76	0.02070E+01			
77	0.02070E+01			
78	0.02070E+01			
79	0.02070E+01			
80	0.02070E+01			
81	0.02070E+01			
82	0.02070E+01			
83	0.02070E+01			
84	0.02070E+01			
85	0.02070E+01			
86	0.02070E+01			
87	0.02070E+01			
88	0.02070E+01			
89	0.02070E+01			
90	0.02070E+01			
91	0.02070E+01			
92	0.02070E+01			
93	0.02070E+01			
94	0.02070E+01			
95	0.02070E+01			
96	0.02070E+01			
97	0.02070E+01			
98	0.02070E+01			
99	0.02070E+01			
100	0.02070E+01			

## COMPUTATION OF VELOCITIES AND PRESSURE COEFFICIENTS AT THE PANEL CENTERS

REST CASES (NO BATH MODE) AND MODS YIELDING 500 PANELS - FUSELAGE ONLY

PAGE 1

NO.	XC	YC	ZC	UX	UY	UZ	ABS.V	CP	SOURCE	V NORMAL	AREA
01	11.00170	0.00110	-1.00012	-0.00022	0.10007	-0.10030	0.00700	7.00000	1.00000	-0.00000	0.1110E+00
02	11.00000	0.10000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	-0.10000	1.00000	-0.00000	0.1000E+00
03	11.00170	0.10000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
04	11.00000	0.20000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
05	11.00170	0.20000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
06	11.00000	0.30000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
07	11.00170	0.30000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
08	11.00000	0.40000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
09	11.00170	0.40000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
10	11.00000	0.50000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
11	11.00170	0.50000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
12	11.00000	0.60000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
13	11.00170	0.60000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
14	11.00000	0.70000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
15	11.00170	0.70000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
16	11.00000	0.80000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
17	11.00170	0.80000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
18	11.00000	0.90000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
19	11.00170	0.90000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
20	11.00000	1.00000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
21	11.00170	1.00000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
22	11.00000	1.10000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
23	11.00170	1.10000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
24	11.00000	1.20000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
25	11.00170	1.20000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
26	11.00000	1.30000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
27	11.00170	1.30000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
28	11.00000	1.40000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
29	11.00170	1.40000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
30	11.00000	1.50000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
31	11.00170	1.50000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
32	11.00000	1.60000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
33	11.00170	1.60000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
34	11.00000	1.70000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
35	11.00170	1.70000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
36	11.00000	1.80000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
37	11.00170	1.80000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
38	11.00000	1.90000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
39	11.00170	1.90000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
40	11.00000	2.00000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
41	11.00170	2.00000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
42	11.00000	2.10000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
43	11.00170	2.10000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
44	11.00000	2.20000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
45	11.00170	2.20000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
46	11.00000	2.30000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
47	11.00170	2.30000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
48	11.00000	2.40000	-1.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	1.00000	-0.00000	0.1000E+00
49	11.00170	2.40000									



ORIGINAL PAGE IS  
OF POOR QUALITY

# PRESSURE LIST AND DRAG COEFFICIENTS

\*\*\*\*\*  
PRESSURE CL = 0.00200  
PRESSURE CR = 0.01700  
APPROXIMATE AREA = 174.0000  
SPYNOUS NUMBER = 0.2279E+00  
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ST	SYM	SYM	SYM	CP	VSXMM	VSYMM	VZSMM	ASPH	ZOCPOASPHS2MM	ZOCPOASPHS1MM	ST
1	0.77020	0.00277	-0.00002	0.00000	-0.00022	0.00100	0.00070	0.111	-0.0010792	0.0000100	1
2	0.77007	0.00001	-0.01012	-0.10700	-0.20000	0.00010	0.00020	0.100	0.0000200	-0.0100000	2
3	0.77000	0.01200	-0.20000	0.07000	-0.22113	0.27722	0.00300	0.100	-0.0010200	0.0000000	3
4	0.77000	0.00000	-0.00170	-0.12220	-0.01221	0.00001	0.00221	0.100	0.0000000	-0.0100000	4
5	0.00000	0.20000	-0.07000	0.22200	-0.77741	0.00000	0.02110	0.101	-0.0100000	0.0000000	5
6	0.00000	0.20000	-0.00000	-0.00010	-0.00010	0.00000	0.00000	0.100	0.0000000	-0.0000000	6
7	0.00000	0.00000	-0.10000	0.00000	-0.00000	0.00000	0.00000	0.100	-0.0100000	0.0000000	7
8	0.00000	0.00000	-0.77722	-0.01200	-0.00000	0.00173	-0.20000	0.100	0.0000000	-0.0010000	8
9	0.00000	-0.00000	-0.00270	0.27700	-0.00000	-0.00000	0.00000	0.101	-0.0000000	0.0000000	9
10	0.00000	0.00000	-0.00000	0.01200	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	10
11	0.00000	0.00000	-0.00000	0.20013	-0.70000	0.00000	-0.00000	0.113	-0.0000000	0.0000000	11
12	0.00000	0.00000	-0.00000	-0.01000	-0.01000	0.00000	0.00000	0.100	0.0000000	-0.0000000	12
13	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.112	-0.0000000	0.0000000	13
14	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	0.0000000	-0.0000000	14
15	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	15
16	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	16
17	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	17
18	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	18
19	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	19
20	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	20
21	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	21
22	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	22
23	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	23
24	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	24
25	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	25

26	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	26
27	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	27
28	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	28
29	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	29
30	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	30
31	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	31
32	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	32
33	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	33
34	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	34
35	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	35
36	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	36
37	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	37
38	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	38
39	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	39
40	0.00000	0.00000	-0.00000	-0.00000	-0.00000	0.00000	0.00000	0.100	-0.0000000	0.0000000	40

## CALCULATION OF DRAG BY STREAMLINES

DRAG COEFFICIENTS FOR EACH PANEL AND WIND YIELDING 500 PANELS -- FUSelage ONLY  
DRAG V INFINITE -- 1.0000000. COMPUTE 500 STREAMLINES STARTING AT EACH PANEL CENTROID POINT

## LINE PASSING THROUGH QUADRILATERAL 2

1	2	3	4	CP	SL	WIND
1	11.00000	0.00000	-1.00000	0.00000	0.0	0.00000
2	11.00000	0.00000	-1.00000	-0.00000	0.00000	1.00000
3	10.00000	0.00000	-1.00000	-0.00000	0.00000	1.00000
4	10.00000	0.00000	-1.00000	-0.00000	1.00000	1.00000
5	0.00000	0.00000	-1.00000	-0.00000	1.00000	1.00000

## TRANSITION AT 0.00000 PER STEP NUMBER 0

S	V	WIND	MEAN	WIND	MEAN	WIND	MEAN
0.0	100.00000	0.00000	0.00000	0.0	0.0	1000.00000	1000.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

## LINE PASSING THROUGH QUADRILATERAL 4

1	2	3	4	CP	SL	WIND
1	11.00000	0.00000	-1.00000	0.00000	0.0	0.00000
2	11.00000	0.00000	-1.00000	-0.00000	0.00000	1.00000
3	10.00000	0.00000	-1.00000	-0.00000	0.00000	1.00000
4	10.00000	0.00000	-1.00000	-0.00000	1.00000	1.00000
5	0.00000	0.00000	-1.00000	-0.00000	1.00000	1.00000

## TRANSITION AT 0.00000 PER STEP NUMBER 0

S	V	WIND	MEAN	WIND	MEAN	WIND	MEAN
0.0	100.00000	0.00000	0.00000	0.0	0.0	1000.00000	1000.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.00000	100.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

ORIGINAL PAGE IS  
OF POOR QUALITY

LINE PASSING THROUGH QUADRILATERAL 339

			Z	GP	U005
1	11a10470	0.02760	0.01791	-0.14072	0.0
2	10a10700	0.01974	0.00980	-0.22300	0.07007
3	10a10700	0.01974	0.00980	0.00000	1.20010
4	0.00000	0.00000	1.00000	0.00000	0.00000
5	0.00000	0.00000	1.00000	0.17000	0.00000
6	0.07722	0.00906	1.10791	0.00000	0.00000
7	0.01107	0.00232	1.00007	0.00000	0.00000
8	0.00000	0.00000	-0.00001	0.00000	0.00000
9	7a10000	0.00001	0.01012	-0.00000	0.00000
10	0.00000	0.00000	0.00000	-0.00000	0.00000
11	0.00000	0.00000	0.00000	-0.00000	0.00000
12	0.00000	0.00000	0.00000	-0.00000	0.00000
13	0.00000	0.00000	0.00000	-0.00000	0.00000
14	0.00000	0.00000	0.00000	-0.00000	0.00000
15	0.00000	0.00000	0.00000	-0.00000	0.00000
16	0.00000	0.00000	0.00000	-0.00000	0.00000
17	1a02300	0.00000	0.00000	-0.00000	0.00000
18	0.00000	0.00000	0.00000	-0.00000	0.00000
19	0.00000	0.00000	0.00000	-0.00000	0.00000
20	0.00000	0.00000	0.00000	-0.00000	0.00000
21	0.00000	0.00000	0.00000	-0.00000	0.00000
22	0.00000	0.00000	0.00000	-0.00000	0.00000
23	0.00000	0.00000	0.00000	-0.00000	0.00000
24	0.00000	0.00000	0.00000	-0.00000	0.00000
25	0.00000	0.00000	0.00000	-0.00000	0.00000
26	0.00000	0.00000	0.00000	-0.00000	0.00000
27	0.00000	0.00000	0.00000	-0.00000	0.00000
28	0.00000	0.00000	0.00000	-0.00000	0.00000
29	0.00000	0.00000	0.00000	-0.00000	0.00000
30	0.00000	0.00000	0.00000	-0.00000	0.00000
31	0.00000	0.00000	0.00000	-0.00000	0.00000
32	0.00000	0.00000	0.00000	-0.00000	0.00000
33	0.00000	0.00000	0.00000	-0.00000	0.00000
34	0.00000	0.00000	0.00000	-0.00000	0.00000
35	0.00000	0.00000	0.00000	-0.00000	0.00000
36	0.00000	0.00000	0.00000	-0.00000	0.00000
37	0.00000	0.00000	0.00000	-0.00000	0.00000
38	0.00000	0.00000	0.00000	-0.00000	0.00000
39	0.00000	0.00000	0.00000	-0.00000	0.00000
40	0.00000	0.00000	0.00000	-0.00000	0.00000
41	0.00000	0.00000	0.00000	-0.00000	0.00000
42	0.00000	0.00000	0.00000	-0.00000	0.00000
43	0.00000	0.00000	0.00000	-0.00000	0.00000
44	0.00000	0.00000	0.00000	-0.00000	0.00000
45	0.00000	0.00000	0.00000	-0.00000	0.00000
46	0.00000	0.00000	0.00000	-0.00000	0.00000
47	0.00000	0.00000	0.00000	-0.00000	0.00000
48	0.00000	0.00000	0.00000	-0.00000	0.00000
49	0.00000	0.00000	0.00000	-0.00000	0.00000
50	0.00000	0.00000	0.00000	-0.00000	0.00000
51	0.00000	0.00000	0.00000	-0.00000	0.00000
52	0.00000	0.00000	0.00000	-0.00000	0.00000
53	0.00000	0.00000	0.00000	-0.00000	0.00000
54	0.00000	0.00000	0.00000	-0.00000	0.00000
55	0.00000	0.00000	0.00000	-0.00000	0.00000
56	0.00000	0.00000	0		

TRANSITION AT 4 0 0.00001 PER STEP NUMBER 2

[illegible]

## SUMMARY OF SEWAGE TREATMENT LAYER INSPECTION FOR GUARD LAYERS

CHAS	B		OSTAD	SAID	
1	11:01:170	0.001100	-0.222123	0.000070	0.213057
2	11:01:020	0.000002	-0.777440	0.000000	0.001170
3	11:01:170	0.011003	-0.140002	0.000000	0.000000
4	11:01:000	0.007000	-0.133000	0.000000	0.001173
5	11:01:010	0.000000	-0.150000	0.000010	0.000120
6	11:01:001	0.000000	-0.150000	0.000000	0.000000
7	11:01:170	0.001103	-0.077600	0.000025	0.203000
8	11:01:020	0.000007	-0.000000	0.000070	0.301103
9	11:01:170	0.000000	-0.000000	0.000000	0.000000
10	11:01:000	0.000000	-0.077102	0.000001	0.000000
11	11:01:170	0.000003	-0.033002	0.000000	0.007000
12	11:01:000	0.000003	-0.303007	0.000073	0.001100
13	11:01:000	0.000000	-0.000000	0.000000	0.000000
14	11:01:030	0.011000	-0.117070	0.000102	0.000127
15	11:01:170	0.000007	-0.040002	0.000027	0.001000
16	11:01:000	0.000000	-0.011023	0.000002	0.001100
17	11:01:170	0.000000	-0.000000	0.000000	0.000000
18	11:01:000	0.000000	-0.011120	0.000100	0.000010
19	11:01:170	0.000000	-0.001010	0.000000	0.000000
20	11:01:000	0.000000	-0.000000	0.000000	0.000000
21	11:01:170	0.000011	-0.000000	0.000000	0.000000
22	11:01:001	0.000003	-0.203000	0.000000	-0.000000
23	11:01:170	0.000000	-0.170007	0.000000	0.000000
24	11:01:001	0.011000	-0.011000	0.000000	0.000000
25	11:01:170	0.011002	-0.010002	0.000027	0.000027

001	-0.00000	0.00000	0.70201	0.02400	0.00000
002	-10.00000	0.00000	0.00000	0.00000	0.00000
003	-0.00000	0.00000	0.00000	0.00000	0.00000
004	-12.00000	0.00000	0.00000	0.00000	0.00000
005	-0.00000	0.00000	0.00000	0.00000	0.00000
006	-10.00000	0.00000	0.00000	0.00000	0.00000
007	-0.00000	0.00000	0.00000	0.00000	0.00000
008	-12.00000	0.00000	0.00000	0.00000	0.00000
009	-0.00000	0.00000	0.00000	0.00000	0.00000
010	-10.00000	0.00000	0.00000	0.00000	0.00000
011	-0.00000	0.00000	0.00000	0.00000	0.00000
012	-12.00000	0.00000	0.00000	0.00000	0.00000
013	-0.00000	0.00000	0.00000	0.00000	0.00000
014	-10.00000	0.00000	0.00000	0.00000	0.00000
015	-0.00000	0.00000	0.00000	0.00000	0.00000
016	-12.00000	0.00000	0.00000	0.00000	0.00000
017	-0.00000	0.00000	0.00000	0.00000	0.00000
018	-10.00000	0.00000	0.00000	0.00000	0.00000
019	-0.00000	0.00000	0.00000	0.00000	0.00000
020	-12.00000	0.00000	0.00000	0.00000	0.00000

**PRICING WAS SUFFICIENT?**

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*****
PRTICM C#      0.01020
RPT RPTC# 0000  176.83000
RPT RPTC# 00    0.00000+00
          *****
          P3.74020
*****

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**DECLASS AUTHORITY DERIVED FROM:**

\*\*\*\*\*  
 AVERAGE LENGTH = 0.00700    AVERAGE PANEL AREA = 0.17500    AVERAGE H-CENTROID = 0.00000    END OF RUN AT 2 0 12.225-1

00571074 1000

N	B1	B2	B3	B4	B5	B6	B7	B8	B9	B10	B11	B12	B13	B14	B15	B16	B17	B18	B19	B20	B21	B22	B23	B24	B25	B26	B27	B28	B29	B30	B31	B32	B33	B34	B35	B36	B37	B38	B39	B40	B41	B42	B43	B44	B45	B46	B47	B48	B49	B50	B51	B52	B53	B54	B55	B56	B57	B58	B59	B60	B61	B62	B63	B64	B65	B66	B67	B68	B69	B70	B71	B72	B73	B74	B75	B76	B77	B78	B79	B80	B81	B82	B83	B84	B85	B86	B87	B88	B89	B90	B91	B92	B93	B94	B95	B96	B97	B98	B99	B100																																																																																																	
UNENDING LTRM TRIM SHAP.																																																																																																																																																																																																					
1	-0.770000E+01	-0.770000E+01	-0.011122E+01	-0.011122E+01	-0.022222E+01	-0.022222E+01	-0.033333E+01	-0.033333E+01	-0.044444E+01	-0.044444E+01	-0.055555E+01	-0.055555E+01	-0.066666E+01	-0.066666E+01	-0.077777E+01	-0.077777E+01	-0.088888E+01	-0.088888E+01	-0.099999E+01	-0.099999E+01	-0.111111E+01	-0.111111E+01	-0.122222E+01	-0.122222E+01	-0.133333E+01	-0.133333E+01	-0.144444E+01	-0.144444E+01	-0.155555E+01	-0.155555E+01	-0.166666E+01	-0.166666E+01	-0.177777E+01	-0.177777E+01	-0.188888E+01	-0.188888E+01	-0.199999E+01	-0.199999E+01	-0.211111E+01	-0.211111E+01	-0.222222E+01	-0.222222E+01	-0.233333E+01	-0.233333E+01	-0.244444E+01	-0.244444E+01	-0.255555E+01	-0.255555E+01	-0.266666E+01	-0.266666E+01	-0.277777E+01	-0.277777E+01	-0.288888E+01	-0.288888E+01	-0.299999E+01	-0.299999E+01	-0.311111E+01	-0.311111E+01	-0.322222E+01	-0.322222E+01	-0.333333E+01	-0.333333E+01	-0.344444E+01	-0.344444E+01	-0.355555E+01	-0.355555E+01	-0.366666E+01	-0.366666E+01	-0.377777E+01	-0.377777E+01	-0.388888E+01	-0.388888E+01	-0.399999E+01	-0.399999E+01	-0.411111E+01	-0.411111E+01	-0.422222E+01	-0.422222E+01	-0.433333E+01	-0.433333E+01	-0.444444E+01	-0.444444E+01	-0.455555E+01	-0.455555E+01	-0.466666E+01	-0.466666E+01	-0.477777E+01	-0.477777E+01	-0.488888E+01	-0.488888E+01	-0.499999E+01	-0.499999E+01	-0.511111E+01	-0.511111E+01	-0.522222E+01	-0.522222E+01	-0.533333E+01	-0.533333E+01	-0.544444E+01	-0.544444E+01	-0.555555E+01	-0.555555E+01	-0.566666E+01	-0.566666E+01	-0.577777E+01	-0.577777E+01	-0.588888E+01	-0.588888E+01	-0.599999E+01	-0.599999E+01	-0.611111E+01	-0.611111E+01	-0.622222E+01	-0.622222E+01	-0.633333E+01	-0.633333E+01	-0.644444E+01	-0.644444E+01	-0.655555E+01	-0.655555E+01	-0.666666E+01	-0.666666E+01	-0.677777E+01	-0.677777E+01	-0.688888E+01	-0.688888E+01	-0.699999E+01	-0.699999E+01	-0.711111E+01	-0.711111E+01	-0.722222E+01	-0.722222E+01	-0.733333E+01	-0.733333E+01	-0.744444E+01	-0.744444E+01	-0.755555E+01	-0.755555E+01	-0.766666E+01	-0.766666E+01	-0.777777E+01	-0.777777E+01	-0.788888E+01	-0.788888E+01	-0.799999E+01	-0.799999E+01	-0.811111E+01	-0.811111E+01	-0.822222E+01	-0.822222E+01	-0.833333E+01	-0.833333E+01	-0.844444E+01	-0.844444E+01	-0.855555E+01	-0.855555E+01	-0.866666E+01	-0.866666E+01	-0.877777E+01	-0.877777E+01	-0.888888E+01	-0.888888E+01	-0.899999E+01	-0.899999E+01	-0.911111E+01	-0.911111E+01	-0.922222E+01	-0.922222E+01	-0.933333E+01	-0.933333E+01	-0.944444E+01	-0.944444E+01	-0.955555E+01	-0.955555E+01	-0.966666E+01	-0.966666E+01	-0.977777E+01	-0.977777E+01	-0.988888E+01	-0.988888E+01	-0.999999E+01	-0.999999E+01	-1.011111E+01	-1.011111E+01	-1.022222E+01	-1.022222E+01	-1.033333E+01	-1.033333E+01	-1.044444E+01	-1.044444E+01	-1.055555E+01	-1.055555E+01	-1.066666E+01	-1.066666E+01	-1.077777E+01	-1.077777E+01	-1.08888

N	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	00	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	00	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	00	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	00	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	00	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	00	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63
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STANDARD ERROR IN INPUT = 0.0116 ANGLE = 29.121

INCREASED VELOCITY AT RING VERTICES AT WAKE-BOAT PANEL, CENTRIGES:

[illegible]

000	1.01512700E-01	2.02332000E-01	-2.18100222E-01	-1.19020160E-01	-1.12490000E-03	7.29603370E-03
001	1.12091127E-01	1.78100000E-01	-1.00000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
002	1.13774007E-01	2.03062712E-01	-1.16264002E-01	-1.19055470E-01	-2.06077153E-03	2.07111202E-03
003	1.15092127E-01	2.16100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
004	1.16209127E-01	2.28100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
005	1.17120127E-01	2.39100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
006	1.17936127E-01	2.49100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
007	1.18679127E-01	2.58100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
008	1.19359127E-01	2.66100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
009	1.20000127E-01	2.73100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
010	1.20609127E-01	2.79100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
011	1.21196127E-01	2.84100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
012	1.21761127E-01	2.88100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
013	1.22304127E-01	2.91100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
014	1.22826127E-01	2.93100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
015	1.23328127E-01	2.95100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
016	1.23810127E-01	2.96100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
017	1.24273127E-01	2.97100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
018	1.24718127E-01	2.98100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
019	1.25146127E-01	2.99100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
020	1.25558127E-01	3.00100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
021	1.25955127E-01	3.01100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
022	1.26338127E-01	3.02100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
023	1.26707127E-01	3.03100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
024	1.27063127E-01	3.04100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
025	1.27407127E-01	3.05100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
026	1.27739127E-01	3.06100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
027	1.28060127E-01	3.07100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
028	1.28370127E-01	3.08100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
029	1.28670127E-01	3.09100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
030	1.28960127E-01	3.10100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E-01
031	1.29240127E-01	3.11100000E-01	-1.10000000E-01	-1.00000000E-01	-1.00000000E-01	1.00000000E

**BEST GROUP: 122 WITH 1021 AND 4020. VILLAINS 200 PANELS - FIVE-AGE ONLY**

```
U VELOCITY=1.0      V VELOCITY= 0.0      Z VELOCITY= 0.0.-
```

ITERATIVE MATRIX SOLVING INFORMATION

1787471000	DATA OF CHANNELS	4	31	99
1	0.00000000			
2	0.00000000			
3	0.00000000			
4	0.00000000			
5	0.00000000			
6	0.00000000			
7	0.00000000			
8	0.00000000			
9	0.00000000			
10	0.00000000			
11	0.00000000			
12	0.00000000			
13	0.00000000			
14	0.00000000			
15	0.00000000			
16	0.00000000			
17	0.00000000			
18	0.00000000			
19	0.00000000			
20	0.00000000			
21	0.00000000			
22	0.00000000			
23	0.00000000			
24	0.00000000			
25	0.00000000			
26	0.00000000			
27	0.00000000			
28	0.00000000			
29	0.00000000			
30	0.00000000			
31	0.00000000			
32	0.00000000			
33	0.00000000			
34	0.00000000			
35	0.00000000			
36	0.00000000			
37	0.00000000			
38	0.00000000			
39	0.00000000			
40	0.00000000			
41	0.00000000			
42	0.00000000			
43	0.00000000			
44	0.00000000			
45	0.00000000			
46	0.00000000			
47	0.00000000			
48	0.00000000			
49	0.00000000			
50	0.00000000			
51	0.00000000			
52	0.00000000			
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79	0.00000000			
80	0.00000000			
81	0.00000000			
82	0.00000000			
83	0.00000000			
84	0.00000000			
85	0.00000000			
86	0.00000000			
87	0.00000000			
88	0.00000000			

EXPLANATION OF VELOCITIES AND AVERAGE COEFFICIENTS AT THE PANEL CENTERS

PUT CEMENT 102 WITH 4021 AND 4022 VIBRATING 200 POUNDS -- FIVE-ONE ONE-7

PAGE 4

[illegible][illegible]

**RESOURCES LIST AND ROAD SURVEILLANCE**

[illegible]

ORIGINAL PAGE IS  
OF POOR QUALITY

[illegible][illegible]

**TOTAL BODY EFFICIENCY**

```

*****
TOTAL BODY CL = 0.00197
TOTAL BODY CD = 0.02020
REPORTING AREA = 174.00000
DETAILS OF NUMBER = 0.23749000
PLOT LENGTH = 23.74024
*****

```

## USER'S INSTRUCTIONS - GRIDPLOT PROGRAM

The program is written in FORTRAN IV and is designed to execute in single \_\_\_\_\_ precision on an IBM 370/165 computer with an average execution time of 1 minute for each data set. An average execution requires approximately 320,000 bytes of core storage. The program accepts multiple data sets. \_\_\_\_\_

Given a data set describing the half-body\* under consideration, the program may be instructed to perform the following:

- (a) Generate a properly-indexed data set with additional body (M,N) stations,
- (b) Modify the input data by a simple averaging technique, a linear-interpolation technique, and/or user-specified data-point change information,
- (c) Plot various orthographic, perspective, and/or stereoscopic views of the input data and/or the modified data,
- (d) Refine the grid network by either an equal-line augmentation scheme or a user-specified line augmentation scheme,
- (e) Punch properly-indexed data sets of the input and/or modified data set(s) for input into the NCSU PLOT program of NASA CR-2523 and/or into the FLOWBODY program of this report, and
- (f) Convert the data into different units.

---

\* Since the body is considered to be symmetrical about the X-Z plane, only half of the body is needed to describe the entire body.

The program requires the specification of the following input in the indicated order: \_\_\_\_\_

CARD 1:

- (a) The maximum number N of N-stations present in any input data set to be tried:

N is a right-adjusted positive integer number occupying columns 1-5.

- (b) The maximum number M of M-stations present in any input data set to be tried:

M is a right-adjusted positive integer number occupying columns 6-10.

- (c) The maximum number NADD of additional N-stations present in any input data set to be tried:

NADD is a right-adjusted positive integer number occupying columns 11-15.

- (d) The maximum number MADD of additional M-stations present in any input data set to be tried:

MADD is a right-adjusted positive integer number occupying columns 16-20.

- (e) The horizontal (x-direction) length PXL of the plotting picture:

PXL is a single-precision floating-point number occupying columns 21-30 in an F10.0 field. The units of PXL must be appropriate to the installation. At NCSU, PXL must be in inches.

- (f) The width (y-direction) PYL of the plotting picture:

PYL is a single-precision floating-point number occupying columns 31-40 in a F10.0 field. The units of PYL must be appropriate to the installation. At NCSU, PYL must be in inches.

Important: Only one "Card 1" is permitted per execution.

CARD 2:

- (a) The read unit number IDS:

IDS is a right-adjusted integer number occupying columns 1-5 and specifying that the data is to be read from cards, magnetic tape, disk, etc. The user must supply the suitable job control cards for the tape and/or disk reads. The IDS parameter controls only the reading of CARD 3, CARD 4, and the Body Description cards.

- (b) The desired number INPTM of additional interior M-stations: —

INPTM is a right-adjusted integer number occupying columns 6-10. INPTM may be negative, zero, or positive. If INPTM is negative, no grid refinement of the M-station is performed. If INPTM is zero, no equal-line augmentation is performed but allows for refinement by the user-specified line-augmentation scheme. If INPTM is positive, the equal-line augmentation scheme may (to be explained later) be used with the number of additional M-stations between each two successive input M-stations equal to INPTM.

- (c) The desired number INPTN of additional interior N-stations:

INPTN is a right-adjusted integer number occupying columns 11-15. INPTN may be negative, zero, or positive. If INPTN is



negative, no grid refinement of the N-stations is performed. If INPTN is zero, no equal-line augmentation is performed but allows for refinement by the user-specified line-augmentation scheme. If INPTN is positive, the equal-line augmentation scheme may (to be explained later) be used with the number of additional N-stations between each two successive input M-stations equal to INPTN.

(d) The punch option IPUNCH:

IPUNCH is a right-adjusted nonnegative integer number, occupying columns 16-20, that specifies the punching of the data set with the additional body (M,N) stations. If IPUNCH = 0, no cards are punched. If IPUNCH = 1, cards are punched.

(e) The input-data plot option IPLOT1:

ILOT1 is a right-adjusted nonnegative integer number occupying columns 21-25. If ILOT1 = 0, no plots are produced. If ILOT1 = 1, plots are produced.

(f) The modified-data plot option ILOT2:

ILOT2 is a right-adjusted nonnegative integer number occupying columns 26-30. If ILOT2 = 0, no plots are produced. If ILOT2 = 1, plots are produced.

(g) The input-data punch option LPCH1:

LPCH1 is a right-adjusted nonnegative integer number, occupying columns 31-35, that specifies the punching of the input data in a compatible form for the PLOT program given in NASA CR-2523 [Reference 3]. If LPCH1 = 0, no cards are punched. If LPCH1 = 1, cards are punched.

(h) The modified-data punch option LPCH2: —

LPCH2 is a right-adjusted nonnegative integer number, occupying columns 36-40, that specifies the punching of the modified data in a compatible form for the PLOT program given in NASA CR-2523 [Reference 3]. If LPCH2 = 0, no cards are punched. If LPCH2 = 1, cards are punched.

(i) The write option IWRITE: —

IWRITE is a right-adjusted nonnegative integer number, occupying columns 41-45, that specifies the amount of desired output. If IWRITE = 0, maximum printout is produced. If IWRITE = 2, minimum printout is produced. If IWRITE = 1, the amount of printout is between the minimum and maximum.

(j) The conversion factor CF: —

CF is a single-precision floating-point number, occupying columns 51-60 in an F10.0 field, that may be used to convert the data of CARD 5 through CARD (K + 4) from one set of units to another.

CARD 3:

The title array TITLE:

The 80 characters of the array TITLE are used for identifying output. The reading of TITLE is controlled by the read unit number IDS.

CARD 4:

The number NQE of quadrilaterals of the input half-body data: —

NQE is a right-adjusted integer number occupying columns 1-4. The reading of NQE is controlled by the read unit number IDS.

## \*\* Body Description Cards \*\*

Each card contains the information to specify one half-body point. Each card contains

Columns	FORTTRAN Name	Description
1-12	XI	x-coordinate
13-24	YI	y-coordinate
25-36	ZI	z-coordinate
37-40	NI	N-station index (See Figure 4)
41-44	MI	M-station index (See Figure 4)
45-48	NS	Body number

XI, YI, and ZI are single-precision floating-point numbers in F-fields. NI, MI, and NS are right-adjusted integer numbers. NS should be a constant for a given data set, which must be greater than zero but not equal to 1000. A blank card must be supplied at the end of these cards to signal the end of the body description cards. The reading of the body description cards are controlled by the read unit number IDS.

## \*\* Point Modification Cards \*\*

### 1. Additional Input Point Change Information:

A single card contains the information to change one input point to the given values.

Columns	FORTTRAN Name	Description
1-20	XP	New X-value at (N,M)
21-40	YP	New Y-value at (N,M)
41-60	ZP	New Z-value at (N,M)
61-65	N	Reference N-station ( $\leq$ max NI)
66-70	M	Reference M-station ( $\leq$ max MI)

XP, YP, and ZP are single-precision floating-point numbers in F-fields. N and M are right-adjusted integer numbers that denote the N and M station for the application of XP, YP, and ZP. A blank card must be supplied to serve either of two purposes. If no additional point change information is to be supplied, the blank card terminates the attempt to read more cards. If point

change information is supplied, the blank card signals the end of this information.

## 2. Simple Averaging of Points or Linear Interpolation:

A single card contains the information to change one input point in a prescribed manner. The user may specify a two-point average, four-point average, two-point linear interpolation, or four-point linear interpolation.

Columns	FORTRAN Name	Description
1-5	M1	1st reference M-station $[0 \leq M1 \leq \max(MI)]$
6-10	M2	2nd reference M-station $[1 \leq M2 \leq \max(MI)+1]$
11-15	N1	1st reference N-station $[0 \leq N1 \leq \max(NI)]$
16-20	N2	2nd reference N-station $[1 \leq N2 \leq \max(NI)+1]$
21-25	IMETH	Method: IMETH = 0 $\rightarrow$ simple average IMETH = 1 $\rightarrow$ linear interpolation

It should be noted that points are changed by the order in which the data cards are encountered. It must be true that

$$|M2 - M1| = 0 \text{ or } 2$$

and

$$|N2 - N1| = 0 \text{ or } 2.$$

Consider a representative (plane) portion of the grid of the original input data below. Suppose it is desired to modify the original input point (e).

Three schemes of each method are available (See Figure 5):

1. Two-point scheme of the points (a) and (c):  $M2 = (m+1)$ ,  $M1 = (m-1)$ ,  
 $N2 = (n+2)$ ,  $N1 = (n)$
2. Two-point scheme of the points (b) and (d):  $M2 = (m+2)$ ,  $M1 = (m)$ ,  
 $N2 = (n+1)$ ,  $N1 = (n+1)$
3. Four-point scheme of the points (a), (b), (c), and (d):  $M2 = (m+2)$ ,  
 $M1 = (m)$ ,  $N2 = (n+2)$ ,  $N1 = (n)$ .

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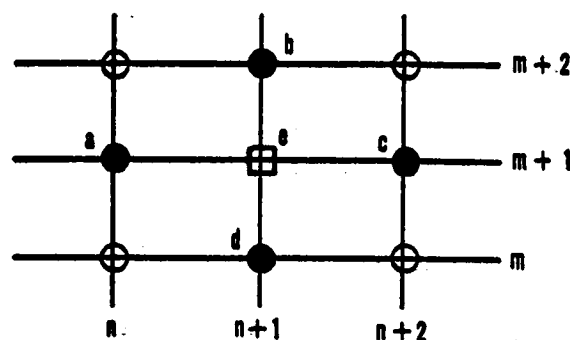


Figure 5: Illustration of points used in averaging and interpolating schemes

M2, M1, N2, and N1 are right-adjusted integer numbers. A blank card must be supplied to serve either of two purposes. If no averaging (or linear interpolation) information is to be supplied, the blank card terminates the attempt to read more cards. If averaging (or linear interpolation) information is supplied, the blank card signals the end of this information.

#### **\*\* Console Message LABEL Card \*\***

The 80 characters of the array LABEL is used to provide information to the operator on the console typewriter about specific forms for plotting. Important: Only one LABEL card is permitted per execution.

#### **\*\* Plot Cards \*\***

A single card contains all the necessary information for one plot. The available options and the necessary input for each are described in the succeeding sections. Reading of these cards are controlled by nonzero values of IPLOT1 and/or IPLOT2. Although the various plot cards, applicable to both the input and modified data, are presently discussed, only the plot card(s) pertaining to the plotting of the input data (i.e., if IPLOT1  $\neq$  0) must be included at this time.

Orthographic projections. - For orthographic projections, the card should be set up as follows (See Figure 6):

Columns	FORTRAN Name	Description
1	HORZ	"X", "Y", or "Z" for horizontal axis
3	VERT	"X", "Y", or "Z" for vertical axis
5 to 7	TEST1	Word "OUT" for deletion of hidden lines; otherwise, leave blank
8 to 12	PHI	Roll angle, degrees (See Figure 7)
13 to 17	THETA	Pitch angle, degrees (See Figure 7)
18 to 22	PSI	Yaw angle, degrees (See Figure 7)
48 to 52	PLOTSZ	PLOTSZ determines the size of plot (scale factor is computed using PLOTSZ and maximum dimension of configuration)
53 to 55	TYPE	Word "ORT"
72	KODE	If KODE = 0, continue reading plot cards If KODE = 1, after processing this plot, continue with the remaining non-plotting portion of the program

An attempt is made to center the given-configuration within the specified field. If the desired plot size is greater than 28 inches, centering is attempted within 28 inches so care must be taken in choosing the view. Minimum values are adjusted so that body axis lines with no rotation angles coincide with grid lines on the plotter paper. Therefore, the plotter pen should always be positioned exactly 1 inch from the side of the plotting space and on the intersection of heavy grid lines at the start of plotting.

Plan, front, and side views (stacked). - For plan, front, and side views, the card should be set up as follows (See Figure 8):

Columns	FORTRAN Name	Description
8 to 12	PHI	y-origin on paper of plan view, inches
13 to 17	THETA	y-origin on paper of side view, inches
18 to 22	PSI	y-origin on paper of front view, inches

Columns	FORTRAN Name	Description
48 to 52	PLOTSZ	PLOTSZ determines size of plot (a scale factor is computed using PLOTSZ and maximum dimension of configuration)
53 to 55	TYPE	Word "VU3"
72	KODE	If KODE = 0, continue reading plot cards If KODE = 1, after processing this plot, continue with the remaining non-plotting portion of the program

Perspective views. - For perspective views, the card should be set up as follows (See Figure 9):

Columns	FORTRAN Name	Description
8 to 12	PHI	x of view point (location of viewer) in data coordinate system
13 to 17	THETA	y of view point in data coordinate system
18 to 22	PSI	z of view point in data coordinate system
23 to 27	XF	x of focal point (determines direction and focus) in data coordinate system
28 to 32	YF	y of focal point in data coordinate system
33 to 37	ZF	z of focal point in data coordinate system
38 to 42	DIST	Distance from eye to viewing plane, inches
43 to 47	FMAG	Viewing-plane magnification factor; it controls size of projected image
48 to 52	PLOTSZ	Diameter of viewing plane, inches; DIST and PLOTSZ together determine a cone which is field of vision; PLOTSZ value is also relative to type of viewer which is to be used.
53 to 55	TYPE	Word "PER"
72	KODE	If KODE = 0, continue reading plot cards If KODE = 1, after processing this plot, continue with the remaining non-plotting portion of the program

Stereo frames suitable for viewing in a stereoscope. - For stereo frames suitable for viewing in a stereoscope, the input is identical to that for the perspective views except that the word "STE" is used in columns 53 to 55. (See Figure 10). \_\_\_\_\_

IMPORTANT: If  $IPL0T1 \neq 0$ , at least one plot card must be supplied. Similarly, if  $IPL0T2 \neq 0$ , at least one plot card must be supplied.

#### \*\* User-Specified Line-Augmentation Cards \*\*

A single card contains the information to specify additional M-lines or N-lines between the "referenced" input M- or N-line.

Columns	FORTRAN Name	Description
1-4	NAME	Line of reference (M or N or END)
6-10	K1	Reference line number
11-15	NL	Number of additional lines

NAME is a character array, occupying columns 1-4 in an A4 field. If NAME = M, the number NL of additional lines is supplied between M-line (K1) and M-line (K1+1). If NAME = N, the number NL of additional lines is supplied between N-line (K1) and N-line (K1+1). Cards of this type is continued until NAME = END is encountered. Since NAME is a character array, the specification of M, N, or END must be left-adjusted.

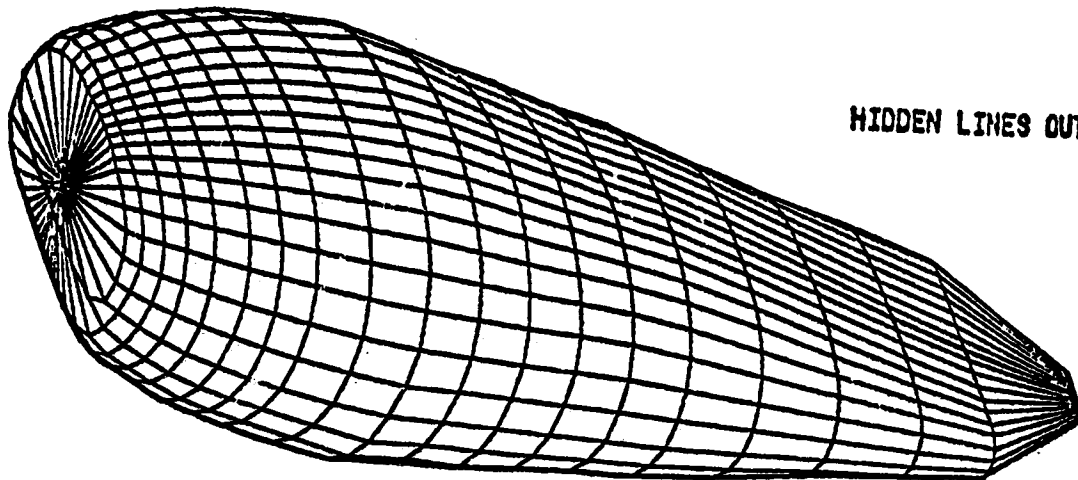
#### \*\* Plot Cards for Modified Data \*\*

The plot cards described earlier must be now included for the plotting of the modified body, if and only if  $IPL0T2 \neq 0$ .



Specification of the cards above represent a complete set of data for a particular body. Additional data sets are programmed similarly starting again at CARD 2. A blank card should be supplied at the end of the last data set to terminate the program.

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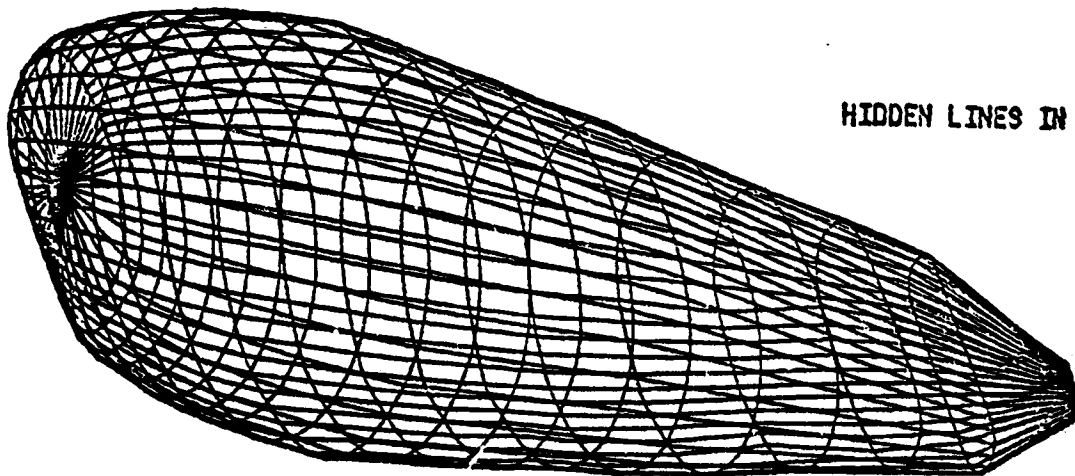
HIDDEN LINES OUT

NEW FAT NACELLE FOR LESS DRAG WITH N=21 AND M=21 YIELDING 400 PANELS —

X Z OUT 45. 10. 30.

6.0 ORT

0



HIDDEN LINES IN

NEW FAT NACELLE FOR LESS DRAG WITH N=21 AND M=21 YIELDING 400 PANELS —

X Z 45. 10. 30. \_\_\_\_\_

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Figure 6: Example of orthographic projection

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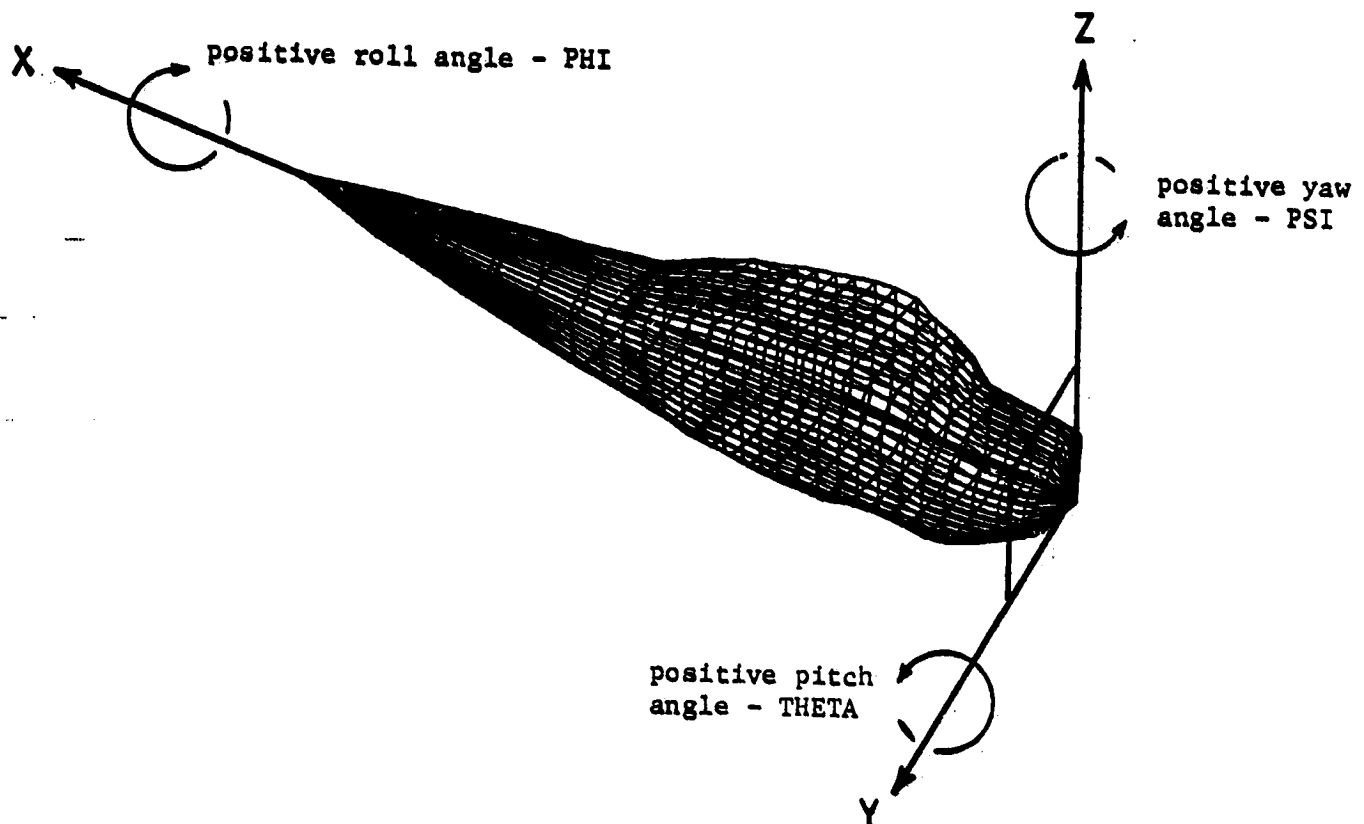
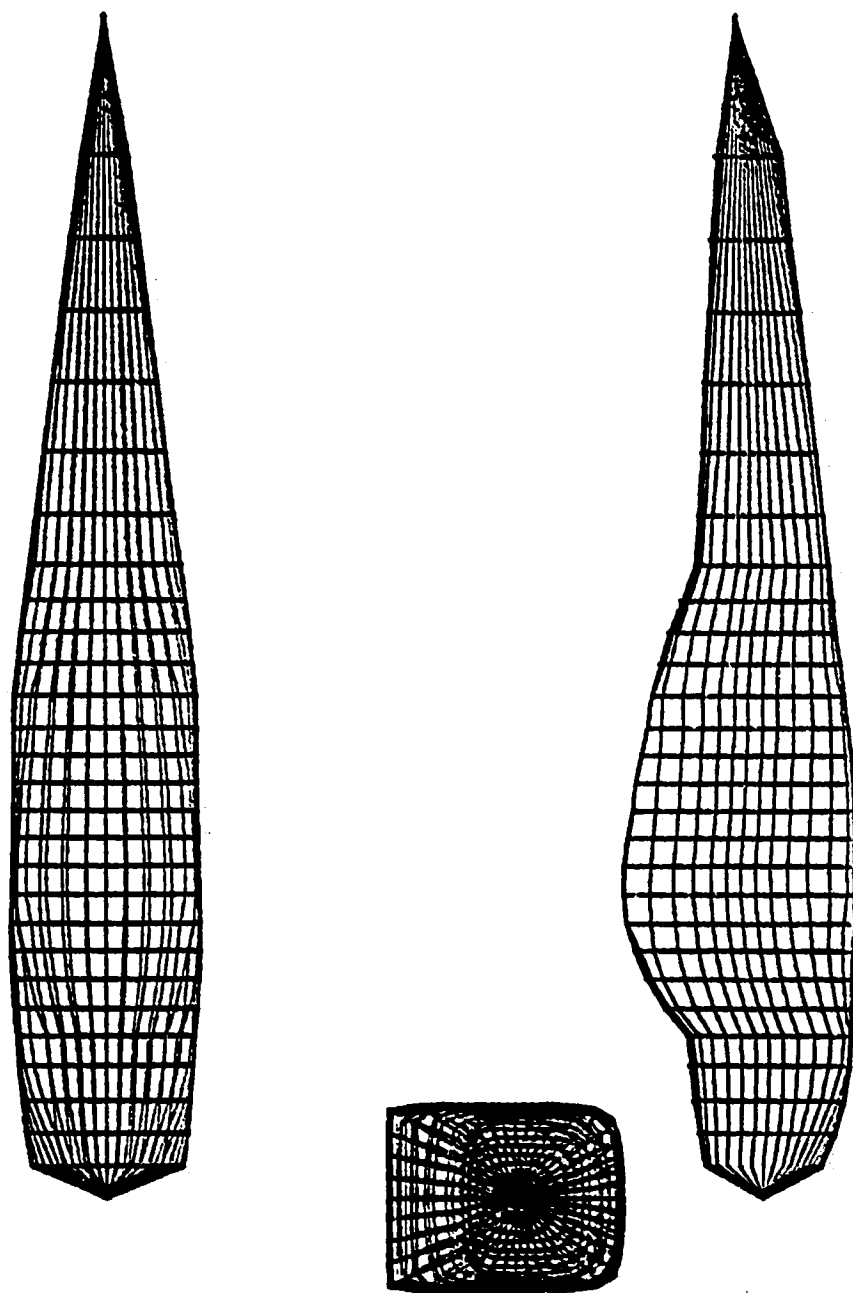


Figure 7: Orientation of body with respect to body reference axes for plotting angles —

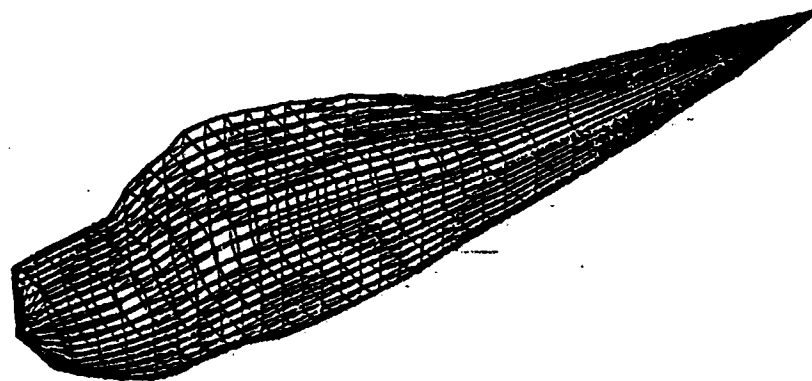
BEST CESSNA 182 WITH  $M=21$  AND  $N=29$



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Figure 8: Example of 3-view plot

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BEST CESSNA 182 WITH M=21 AND N=29 YIELDING 560 PANELS -- FUSELAGE ONLY

-20. -50. 50. 12. 0.0 0.0 14. 1.0 8.0 PER 1

Figure 9: Example of perspective view

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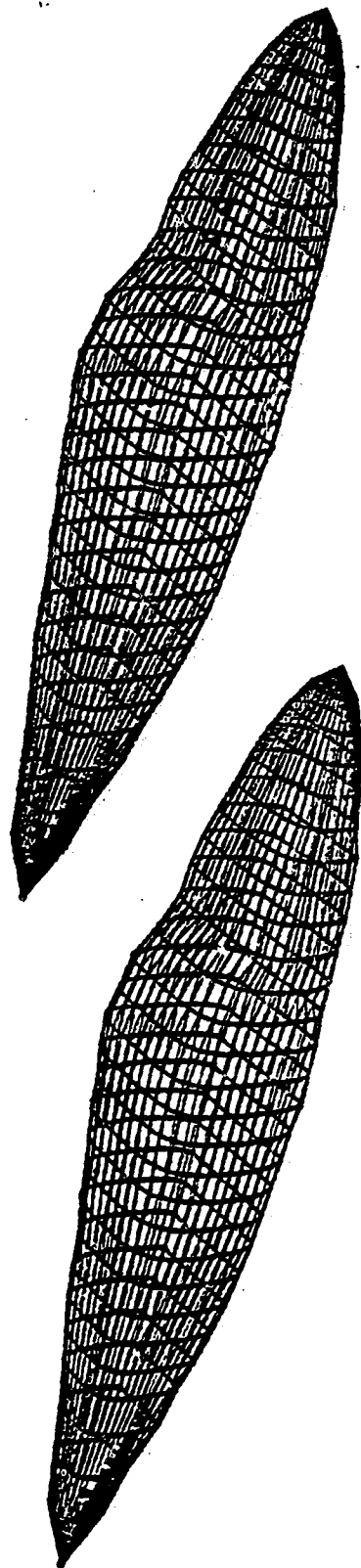


Figure 10: Example of stereo frames of stereoscopic view

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3 FORMAT (9I5,5X,F10.5)
  ICAN=0
  IF (CF.EQ.0.0E0)CF=1.0E0
  IF ((IDS.GT.0.AND.IDS.NE.JPUNCH).AND.(IDS.NE.JWRITE.AND.IDS.NE.KFI
1 1L1).AND.(IDS.NE.KFILE2.AND.IDS.NE.KFILE3).AND.IDS.NE.KFILE4) GO TO
1 5
  IF (IDS.LE.0) GO TO 97
  WRITE (JWRITE,4)
4 FORMAT (1X,///.3X,28HERROR IN IDS ... TERMINATING.//)
  GO TO 97
5 INPTN=IABS(INPTN)
  INPTM=IABS(INPTM)
  INPTNS=INPTN
  INPTMS=INPTM
  READ (IDS,6) (TITLE(I),I=1,20)
6 FORMAT (20A4)
  WRITE (JWRITE,7) (TITLE(I),I=1,20)
7 FORMAT (1H1,///.5X,8HINPUT**.,//.10X,20A4,/)
  WRITE (JWRITE,9) IDS,INPTM,INPTN,IPUNCH,IPLGT1,IPLOT2,LPOCH1,LPOCH2.
1 IWRITE,CF
8 FORMAT (1X,/,10X,4HIDS=,13,3X,6HINPTM=,13,4X,6HINPTN=,13,4X,7HIPUN
1CH=,13,4X,7HIPLOT1=,13,3X,7HIPLOT2=,13,/,10X,6HLPCH1=,13,2X,6HLPCH
12=,13,3X,7HIWRITE=,13,3X,3HCF=,E16.9,/)
  READ (IDS,9) NQE
9 FORMAT (14)
  WRITE (JWRITE,10) NQE
10 FORMAT (10X,25HNUMBER OF QUADRILATERALS.,14,/)
  IF (IWRITE.EQ.0) WRITE (JWRITE,11)
11 FORMAT (15X,2HX1,12X,2HY1,12X,2HZ1,8X,2HNI,5X,2HMI,5X,2HNS,/)
12 READ (IDS,12) XI,YI,ZI,NI,MI,NS
  FORMAT (3F12.8,3I4)
  NMAX=MI
  NMIN=MI
  NMAX=NI
  NMIN=NI
  NSS=NS
  L=1
  GO TO 14
13 READ (IDS,12) XI,YI,ZI,NI,MI,NS
  IF (NSS.NSS) GO TO 16
  L=L+1
14 IF (IWRITE.EQ.0) WRITE (JWRITE,15) XI,YI,ZI,NI,MI,NS

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15 FORMAT (10X,3(F12.8,2X),3(15.2X))
P(NI,MI,1)=XI*CF
P(NI,MI,2)=YI*CF
P(NI,MI,3)=ZI*CF
MMAX=MAXO(MMAX,MI)
MMIN=MINO(MMIN,MI)
NMAX=MAXO(NMAX,NI)
NMIN=MINO(NMIN,NI)
GC TO 13
16 NC=(MMAX-MMIN)*(NMAX-NMIN)
IF (NO.EQ.NOE) GO TO 18
WRITE (JWRITE,17) NO,NC
17 FORMAT (1X,/,5X,30HNUMBER OF QUADRILATERALS READ(.14,56H) DOES N
10T EQUAL THE NUMBER OF SPECIFIED QUADRILATERALS(.14,1H))
ICAN=1
GO TO 96
C** INPUT READING COMPLETED, CHECK FOR ERRORS
18 IF ((MMAX.EQ.(2*(MMAX/2)).OR.MMAX.LT.4).OR.(MMIN.EQ.(2*(MMIN/2)).
1OR.MMIN.LE.1)).OR.((NMAX.EQ.(2*(NMAX/2)).OR.NMAX.LT.4).OR.(NMIN.EQ
1.(2*(NMIN/2)).OR.NMIN.LE.1))) GO TO 19
GO TO 21
19 WRITE (JWRITE,20) MMAX,MMIN,NMAX,NMIN
20 FORMAT (1X,/,5X,23HERROR DETECTED IN INPUT,3X,6HMMAX =.13,3X,6HMM
1IN =.13,/,31X,6HNMAX =.13,3X,6HNMIN =.13)
ICAN=1
GO TO 56
C** ENACT POINT MODIFICATIONS
21 CALL PNT1(J1,J2,P,JREAD,JWRITE,CF)
CALL PNT2(J1,J2,P,JREAD,JWRITE,MMAX,NMAX)
IF (NCCUNT.NE.1) GO TO 23
IF (IPLJTI.EQ.0.AND.IPLOT2.EQ.0) GO TO 23
CALL PICSIZ(PXL,PYL)
READ (JREAD,22) (LABEL(NN),NN=1,80)
22 FCFORMAT (30A1)
CALL PENMSG(LABEL)
23 IF (IPLOT1.EQ.0.AND.LPCHI.EQ.0) GO TO 38
LCODE=1
CONVERT TC PLOT AXIS SYSTEM
ZMAX=-1000.0
ZMIN=1000.0
DO 24 NN=1,NMAX
XFUS(NN)=P(1,1,1)-P(NN,1,1)

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WRITE (JWRITE,30) (XFUS(NN),NN=1,NMAX)
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37 P(NN.MM,3)=P(NN.MM,3)-ZORG
38 IF (INPTM.LT.0.AND.INPTN.LT.0.AND.IPLOT2.EQ.0.AND.LPCH2.EQ.0) GO TO 96
CALL TEST(MAC1,MAC2,MP,NP,J1,J2,KM1,KM2,KN1,KN2,NMAX,NMAX)
KN=NMAX
IF ((INPTM.EQ.0.AND.INPTN.EQ.0).AND.(MAC1.EQ.0.AND.MAC2.EQ.0)) GO TO 79
C*** FOR EACH N-STATION, CURVE FIT THE M-STATIONS
IBP1=0
IBP2=0
K=0
DO 54 N=1,NMAX
IF (N.EQ.1.OR.N.EQ.NMAX) GO TO 39
GO TO 46
39 IF (MAC1.NE.0) GO TO 40
NPTS=MMAX+(NMAX-1)*INPTM
GO TO 41
40 NPTS=MAC1
C*** FOR FIRST AND LAST N-STATIONS
41 DO 42 M=1,NPTS
42 Q(N,M,1)=P(N,1,1)
IQ=1
IP=1
Q(N,IQ,2)=P(N,IP,2)
Q(N,IQ,3)=P(N,IP,3)
43 IQMX=IQ+1+INPTM
IP=IP+1
IF (IP.GT.MMAX) GO TO 54
IF (MAC1.EQ.0) GO TO 44
ICD=0
IF ((IP-1).GE.KM1)ICD=1
IF (ICD.EQ.0)INPTM=MP(IP-1,1)
IF (ICD.EQ.1)INPTM=MP(IP-KM1,2)
IF (ICD.EQ.0)IBP1=IBP1+INPTM
IF (ICD.EQ.1)IBP2=IBP2+INPTM
IQMX=IQ+1+INPTM
44 X1=(P(N,IP,2)-P(N,IP-1,2))/FLOAT(INPTM+1)
X2=(P(N,IP,3)-P(N,IP-1,3))/FLOAT(INPTM+1)
IQF1=IQ+1
DC 45 ML=IQF1,IQMX
Q(N,ML,2)=Q(N,ML-1,2)+X1
45 Q(N,ML,3)=Q(N,ML-1,3)+X2

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46 IQ=IQMX
   GO TO 43
   IF (MMAX.LI.7) MID=MMAX
   KNS=MID+(MID-1)*INPTMS
   SLP1=P(N,1,2)/P(N,1,3)
   SLP2=(P(N,MID,2)-P(N,1,2))/(P(N,MID,3)-P(N,1,3))
   A=ATAN((SLP2-SLP1)/(1.0+SLP1*SLP2))
   M1=1
   M2=MID
   ICCDE=0
   MADD=0
   MD=0
   Y0=P(N,MID,2)
   Z0=P(N,MID,3)
47 DO 48 M=M1,M2
   Z(M+MADD)=(P(N,M,3)-Z0)*COS(A)+(P(N,M,2)-Y0)*SIN(A)
   Y(M+MADD)=(P(N,M,2)-Y0)*COS(A)-(P(N,M,3)-Z0)*SIN(A)
48 CONTINUE
   IF (MAC1.EQ.0) GO TO 49
   KNS=KM2+IBP2
   IF (ICDEF.EQ.3) KNS=KM1+IBP1
49 CALL PCS(MID,Y,Z,XN,YN,INPTM,KN,C,D,DIAG,JWRITE,J4,J3,MAC1,MP,J1,K
1)
   IF (KN.NE.KNS) GO TO 50
   GO TO 52
50 WRITE (JWRITE,51) N,ICDEF,KNS
51 FORMAT (1X,52HPCS DID NOT FIND CORRECT NO. OF POINTS AT N-STATION
1,13,12H WITH ICDEF=.12,/.1X,6HFOUND .13,18+ POINTS(SHOULD BE .13,1
1H))
   GO TO 96
52 DO 53 M=1,KN
   Q(N,M+MD,1)=P(N,1,1)
   Q(N,M+MD,2)=XN(M)*SIN(A)+YN(M)*COS(A)+Y0
   Q(N,M+MD,3)=XN(M)*COS(A)-YN(M)*SIN(A)+Z0
53 CONTINUE
   IF (ICDEF.NE.0.OR.MID.EQ.MMAX) GO TO 54
   SLP1=P(N,MMAX,2)/P(N,MMAX,3)
   SLP2=(P(N,MMAX,2)-P(N,MID,2))/(P(N,MMAX,3)-P(N,MID,3))
   A=ATAN((SLP2-SLP1)/(1.0+SLP1*SLP2))
   ICCDE=1
   M1=MID

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M2=MMAX
MADD=1-MID
MD=KN-1
GO TO 47
54 INPTM=INPTMS
C** SET INITIAL AND FINAL VALUES
DO 55 LL=1,2
N=1
IF (LL.EQ.2) N=NMAX
DO 55 N=1,NPTS
DO 55 JJ=1,3
BS(LL,M,JJ)=Q(N,M,JJ)
NMAX=NPTS
C** FOR EACH M-STATION. CURVE FIT EACH SET OF N-STATICS
MID=(NMAX+1)/2
IF (NMAX.LI.7) MID=NMAX
KNS=MID+(MID-1)*INPTN
KS=NMAX+(NMAX-1)*INPTN
IF (MAC2.EQ.0) GO TO 57
K=1
IBP1=0
IBP2=0
JD2=NMAX
IF (NMAX.GE.7) JD2=(NMAX+1)/2
DO 56 J=1,NMAX
IF (J.LT.JD2) IBP1=IBP1+NP(J,1)
IF (J.GE.JD2) IBP2=IBP2+NP(J-JD2+1,2)
56 CONTINUE
DO 64 M=1,MMAX
X0=Q(MID,M,1)
Y0=Q(MID,M,2)
Z0=Q(MID,M,3)
SAX=0.0
ICGDE=0
M1=1
M2=MID
MADD=0
MD=0
57 SLP1=(Q(M1,M,2)-Q(M2,M,2))/(Q(M1,M,1)-Q(M2,M,1))
SLP2=(Q(M1,M,3)-Q(M2,M,3))/(Q(M1,M,1)-Q(M2,M,1))
ALP1=ATAN((SLP1-SAX)/(1.0+SAX*SLP1))
ALP2=ATAN((SLP2-SAX)/(1.0+SAX*SLP2))
58

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59 DO 59 N=M1,M2
   IP=M2+M1-N
   X(N+MADD)=(Q(IP,M,1)-X0)*COS(ALP1)+(Q(IP,M,2)-Y0)*SIN(ALP1)
   Y(N+MADD)=(Q(IP,M,2)-Y0)*COS(ALP1)-(Q(IP,M,1)-X0)*SIN(ALP1)
59 CONTINUE
   IF (MAC2.EQ.0) GO TO 60
   KNS=KN2+IBP2
   IF (ICODE.EQ.0) KNS=KN1+IBP1
60 CALL PCS(MID,Y,X,XN,YN,INPTN,KN,C,D,DIAG,JWRITE,J4,J3,MAC2,NP,J2,K
1)
   IF (KN.NE.KNS) GO TO 77
   DO 61 N=1,KN
   IP=KN+1-N+MD
   R(IP,M,1)=XN(N)*COS(ALP1)-YN(N)*SIN(ALP1)+X0
61 R(IP,M,2)=XN(N)*SIN(ALP1)+YN(N)*COS(ALP1)+Y0
   DO 62 N=M1,M2
   IP=N2+M1-N
   X(N+MADD)=(Q(IP,M,1)-X0)*COS(ALP2)+(Q(IP,M,3)-Z0)*SIN(ALP2)
   Z(N+MADD)=(Q(IP,M,3)-Z0)*COS(ALP2)-(Q(IP,M,1)-X0)*SIN(ALP2)
62 CONTINUE
   CALL PCS(MID,Z,X,XN,YN,INPTN,KN,C,D,DIAG,JWRITE,J4,J3,MAC2,NP,J2,K
1)
   IF (KN.NE.KNS) GO TO 77
   DO 63 N=1,KN
   IP=KN+1-N+MD
   R(IP,M,3)=XN(N)*SIN(ALP2)+YN(N)*COS(ALP2)+Z0
63 CONTINUE
   IF (ICODE.EC.1.OR.MID.EQ.NMAX) GO TO 64
   ICODE=1
   H1=41
   M2=MMAX
   MADD=1-MID
   MD=KN-1
   GO TO 58
64 CONTINUE
   KN=KS
   IF (MAC2.EQ.0) GO TO 65
   KN=MAC2
65 DO 67 LL=1,2
   N=1
   IF (LL.EQ.2) N=KN
   DO 66 N=1,MMAX

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66 R(N,M,JJ)=BS(LL,M,JJ)
67 CONTINUE
DO 76 N=1,KN
  X0=0.0
  DO 68 M=1,MMAX
    XJ=X0+R(N,M,1)
    CONTINUE
    X0=X0/FL0AT(MMAX)
    IF (N.EQ.1) GO TO 70
    IF (X0.LT.F(N-1,1,1)) GO TO 70
    XJ=XJ.3
    LK=0
    DO 69 M=1,MMAX
      IF (R(N,M,1).GT.R(N-1,1,1)) GO TO 69
      LK=LK+1
      XJ=XJ+R(N,M,1)
    CONTINUE
    IF (LK.EQ.0) ICAN=1
    IF (ICAN.EQ.1) GO TO 72
    XJ=XJ/FLCAT(LK)
    DO 71 M=1,MMAX
      R(N,M,1)=XJ
    CONTINUE
    IF (XJ.GT.R(N-1,1,1)) GO TO 72
    GO TO 76
  NM1=N-1
  IF (ICAN.EQ.1) GO TO 74
  WRITE (JWRITE,73) N,NM1
  73 FORMAT (1X,///.10X.29H AVERAGE X-VALUE AT N-STATION .12.46H IS GREATER THAN AVERAGE X-VALUE AT N-STATION .12.38H. MUST BE LESS THAN 100 EXACTLY EQUAL.//)
  GO TO 96
  74 WRITE (JWRITE,75) N,NM1
  75 FORMAT (1X,///.10X.25H ALL COMPUTED X-VALUES AT N-STATION .12.51H ARE GREATER THAN THE AVERAGE X-VALUE AT N-STATION .12.//)
  GO TO 96
  76 CONTINUE
  GO TO 81
  77 WRITE (JWRITE,73) M,ICLDE,KN,KN
  78 FORMAT (1X,52HPCS DID NOT FIND CORRECT NO. OF POINTS AT M-STATION .1.13.12H WITH ICODE=.12.7.1X.6HFOUND .13.18H PCPOINTS(SHOULD BE .13.1

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1H))
  ICAN=1
  GO TO 96
79 DO 80 N=1,KN
  DC 80 M=1,MMAX
  DO 80 J=1,3
80 R(N,M,J)=P(N,M,J)
C** NOW PRINT RESULTS
81 NNCE=(MMAX-1)*(KN-1)
  IF (IWRITE.NE.2) WRITE (JWRITE,82) MMAX,KN,NNCE
82 FORMAT (1H1,/,5X,11HNEW DATA**/,5X,6HMMAX =,13,3X,6HNNCE =,13,
12X,5H--->,15,15H QUADRILATERALS,/,15X,2HX1,12X,2HZ1,8X,
12HN1,5X,2HW1,5X,2HNS,/)
  IF (IPUNCH.NE.0) WRITE (JPUNCH,83) NNCE
83 FORMAT (14)
  NS=1
  DO 85 N=1,KN
  DO 85 M=1,MMAX
  DO 84 J=1,3
84 IF (ABS(R(N,M,J)).LT.1.0E-04)R(N,M,J)=0.0E0
  IF (IWRITE.NE.2) WRITE (JWRITE,15) (R(N,M,J),J=1,3),N,M,NS
  IF (IPUNCH.NE.0) WRITE (JPUNCH,12) (R(N,M,J),J=1,3),N,M,NS
85 CONTINUE
  IF (IPLUT2.EQ.0.AND.LPCH2.EQ.0) GO TO 96
  LCGL=2
  CONVERT TO PLOT AXIS SYSTEM
  ZMAX=-1000.0
  ZMIN=1000.0
  DO 87 NN=1,KN
  XFUS(NN)=R(1,1,1)-R(NN,1,1)
  DO 86 MM=1,MMAX
  IF (MM.GT.1.AND.MM.LT.MMAX) GO TO 86
  IF (ZMAX.LT.R(NN,MM,3))ZMAX=R(NN,MM,3)
  IF (ZMIN.GT.R(NN,MM,3))ZMIN=R(NN,MM,3)
86 CONTINUE
87 CONTINUE
  ZORG=ABS(ZMIN)+ABS(ZMAX)
  DO 88 NN=1,KN
  DO 88 MM=1,MMAX
  R(NN,MM,3)=R(NN,MM,3)+ZORG
88 R(NN,MM,3)=R(NN,MM,3)+ZORG
C** NEW DATA
  IF (LPCH2.EQ.0) GO TO 92

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WRITE (JPUNCH,26) (XAME2(I),I=1,4)
WRITE (JPUNCH,27) (XFUS(NN),NN=1,KN)
DO 89 NN=1,KN
  WRITE (JPUNCH,27) (R(NN,MM,2),MM=1,MMAX)
  IF (IWRITE.GT.1) GO TO 92
  WRITE (JWRITE,90)
90 FORMAT (1X,///,10X,14HNEW PLOT DATA:.,//)
  WRITE (JWRITE,30) (XFUS(NN),NN=1,KN)
  DC 91 NN=1,KN
  WRITE (JWRITE,30) (R(NN,MM,2),MM=1,MMAX)
  WRITE (JWRITE,31)
  WRITE (JWRITE,30) (R(NN,MM,3),MM=1,MMAX)
91 WRITE (JWRITE,31)
92 IF (IPLOT2.EQ.0) GO TO 94
  REWIND KFILE4
  WRITE (KFILE4) (XFUS(NN),NN=1,KN)
  DO 93 NN=1,KN
    WRITE (KFILE4) (R(NN,MM,2),MM=1,MMAX)
    WRITE (KFILE4) (R(NN,MM,3),MM=1,MMAX)
93 WRITE (JWRITE,35)
  CALL XYZPLT(MMAX,KN,XFUS,SFUS)
  C*** RESET Z-VALUES
94 DO 95 NN=1,KN
95 DO 95 MM=1,MMAX
95 R(NN,MM,3)=R(NN,MM,2)-ZCRG
96 IF (IPLOT1.NE.0.OR.IPLOT2.NE.0) NCOUNT=NCOUNT+1
  IF (IDS.NE.JREAD) REWIND IDS
  GO TO 2
  NCOUNT=NCOUNT+1
97 IF (NCOUNT.GT.1) CALL PICSIZ(0.0,0.0)
  STOP
  END

```

SUBROUTINE PNT1(J2,J1,R,JREAD,JWRITE,CF)  
 C\*\*\* POINT MODIFICATION BY ADDITIONAL INPUT POINT CHANGE INFORMATION  
 C  
 DIMENSION R(J1,J2,3)

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K=0
1 READ (JREAD,2) XP,YP,ZP,N,M
2 FORMAT (3F20.0,2I5)
  IF (N.LE.0.OR.M.LE.0) GO TO 5
  K=K+1
  IF (K.EQ.1) WRITE (JWRITE,3)
3 FORMAT (1X,///.5X,63HPPOINT MODIFICATION BY ADDITIONAL INPUT POINT
  1 CHANGE INFORMATION.//.15X,2HX1.12X,2HY1.12X,2HZ1.8X,2HNI.5X,2HMI./
  1)
  WRITE (JWRITE,4) XP,YP,ZP,N,M
  4 FORMAT (10X,3(F12.8,2X),2(15,2X))
  R(N,M,1)=XP*CF
  R(N,M,2)=YP*CF
  R(N,M,3)=ZP*CF
  GO TO 1
5 RETURN
  FND

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SUBROUTINE PNT2(J2,J1,R,JREAD,JWRITE,MMAX,NMAX)
  POINT MODIFICATION BY SIMPLE AVERAGE OR LINEAR INTERPOLATION
  DIMENSION R(J1,J2,3)
  K=0
  ICCDF1=0
  ICCDF2=0
  1 READ (JREAD,2) M1,M2,N1,N2,IMETH
  2 FORMAT (5I5)
  IF ((M1.LE.0.AND.M2.LE.0).AND.(N1.LE.0.AND.N2.LE.0)) GO TO 31
  IF ((M1.LE.0.OR.M2.LE.0).OR.(N1.LE.0.OR.N2.LE.0)) GO TO 1
  N=K+1
  IF (K.EQ.1) WRITE (JWRITE,3)
  3 FORMAT (1X,///.5X,38HPPOINT MODIFICATION BY SPECIFIED METHOD)
  JS=42
  IF (M1.LE.M2) GO TO 4
  42=M1
  M1=JS
  JS=N2

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IF (N1.LE.N2) GO TO 5
N2=N1
N1=JS
5 L1=M2-M1
  IF (M2-MMAX-1) 6,6,1
  6 IF (1-M1) 7,7,1
  7 IF (N2-MMAX-1) 8,8,1
  8 IF (1-N1) 9,9,1
  9 IF ((L1.EQ.1-OR.L1.GT.2).OR.(L2.EQ.1-OR.L2.GT.2)).J+.L1.EQ.0.AND
    1.L2.FG.0) GO TO 1
  IF (1METH.LT.0)1METH=0
  IF (1METH.GT.1)1METH=1
  AYN=0.OEO
  AZN=0.OEO
  AZM=0.OEO
  IM=1METH+1
  IF (L1.NE.0.AND.L2.NE.0) GO TO 19
  IF (L1.EQ.0.AND.L2.NE.0) GO TO 13
  IF (M2.GT.MMAX) GO TO 10
  IF (M1.L1.1) GO TO 11
  AYM=(R(N1,M1,2)+R(N1,M2,2))/2.OEO
  AZM=(R(N1,M1,3)+R(N1,M2,3))/2.OEO
  GO TO 12
10 AYM=R(N1,M1+1,2)
  AZM=R(N1,M1,3)
  GO TO 12
11 AYM=R(N1,M2-1,2)
  AZM=R(N1,M2,3)
12 N=N1
  M=M1+1
  D=1.OEO
  GO TO 28
13 GC TO (14,15),IM
14 AYN=(R(N1,M1,2)+R(N2,M1,2))/2.OEO
  AZN=(R(N1,M1,3)+R(N2,M1,3))/2.OEO
  GC TO 18
15 IF (N2.GT.NMAX) GO TO 16
  IF (N1.LT.1) GO TO 17
  A=(R(N1,M1,2)-R(N2,M1,2))/(R(N1,M1,1)-R(N2,M1,1))
  B=(R(N1,M1,2)-A*R(N1,M1,1))

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      AYN=A*(R(N1+1,M1,1))+B
      A=(R(N1,M1,3)-R(N2,M1,3))/(R(N1,M1,1))-R(N2,M1,1)
      B=(N1,M1,3)-A*(R(N1,M1,1)
      AZN=A*(R(N1+1,M1,1))+B
      GO TO 18
16  AYN=R(N1,M1,2)
      AZN=R(N1,M1,3)
      ICODE1=1
      GC TO 18
17  AYN=R(N2,M1,2)
      AZN=R(N2,M1,3)
      ICODE2=1
18  N=N1+1
      M=M1
      D=1.OF0
      GC TO 28
19  IF (M2.GT.MMAX) GO TO 20
      IF (M1.LT.1) GO TO 21
      AYM=(R(N1+1,M1,2)+R(N1+1,M2,2))/2.OE0
      AZM=(R(N1+1,M1,3)+R(N1+1,M2,3))/2.OE0
      GO TO 22
20  AYN=R(N1+1,M1+1,2)
      AZM=R(N1+1,M1,3)
      GC TO 22
21  AYM=R(N1+1,M2-1,2)
      AZM=R(N1+1,M2,3)
      GO TO (23,24).IM
22  IF (N2.GT.NMAX) GO TO 25
23  IF (N1.LT.1) GO TO 26
      AYN=(R(N1,M1+1,2)+R(N2,M1+1,2))/2.OE0
      AZN=(R(N1,M1+1,3)+R(N2,M1+1,3))/2.OE0
      GO TO 27
24  IF (N2.GT.NMAX) GO TO 25
      IF (N1.LT.1) GO TO 26
      A=(R(N1,M1+1,2)-R(N2,M1+1,2))/(R(N1,M1+1,1))-R(N2,M1+1,1)
      B=(R(N1,M1+1,2)-A*(R(N1,M1+1,1)
      AYN=A*(R(N1+1,M1+1,1))+B
      A=(R(N1,M1+1,3)-R(N2,M1+1,3))/(R(N1,M1+1,1))-R(N2,M1+1,1)
      B=(R(N1,M1+1,3)-A*(R(N1,M1+1,1)
      AZN=A*(R(N1+1,M1+1,1))+B
      GO TO 27
25  AYN=R(N1,M1+1,2)

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AZN=R(N1,M1+1,3)
ICODE1=1
GO TO 27
26 AYN=R(N2,M1+1,2)
   AZN=R(N2,M1+1,3)
   ICODE2=1
27 N=N1+1
   M=M1+1
   D=2.0E0
   AVY=(AYM+AYN)/D
   AVZ=(AZM+AZN)/D
   IF (IMETH.EQ.0) WRITE (JWRITE,29) N,M,R(N,M,2),AVY,R(N,M,3),AVZ
29 FORMAT (1X,/,5X,POINT(N=,12,/,M=,12,/,Y=,1PE14,7,/,-->,1PE14
1.7,/,22X,7=,1PE14,7,/,-->,1PE14,7,5X,14F5IMPLE AVERAGE)
   IF (IMETH.EQ.1) WRITE (JWRITE,30) N,M,R(N,M,2),AVY,R(N,M,3),AVZ
30 FORMAT (1X,/,5X,POINT(N=,12,/,M=,12,/,Y=,1PE14,7,/,-->,1PE14
1.7,/,22X,7=,1PE14,7,/,-->,1PE14,7,5X,20HLINER INTERPOLATION)
   R(N,M,2)=AVY
   R(N,M,3)=AVZ
   GO TO 1
31 IF (ICODE2.NE.0) WRITE (JWRITE,32)
32 FORMAT (1X,///,5X,67HWARNING...DATA NOT COMPATIBLE AS INPUT TO 'FL
LOWBODY: PROGRAM DUE TO,/,15X,39HPOINT MODIFICATION(S) AT FRONT OF
1BCDY.)
   IF (ICODE1.NE.0) WRITE (JWRITE,33)
33 FORMAT (1X,///,5X,67HWARNING...DATA NOT COMPATIBLE AS INPUT TO 'FL
LOWBODY: PROGRAM DUE TO,/,15X,38HPOINT MODIFICATION(S) AT REAR OF B
1OEY.)
   RETURN
END

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SUBROUTINE TEST(M1,M2,MF,NP,J1,J2,KM1,KM2,KN1,KN2,MX,NX)

SUBROUTINE TEST ALLOWS THE SPECIFICATION OF ARBITRARY ADDITIONAL STATIONS

DIMENSION MP(J1,2),NP(J2,2)

COMMON /INPUT/JREAD,JWRITE,JPUNCH,KK(5)

DATA W/4HM /,N/4HN /,MN/4HEND /

C\*\*\*  
C\*\*\*  
C

C

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```

C*** INITIALIZE PARAMETERS
M1=0
M2=0
KN1=0
KN2=0
KN1=0
KN2=0
L1=0
L2=0
WRITE (JWRITE,1)
1 FORMAT (1H1,/,13X,43H ADDITIONAL ARBITRARY STATION SPECIFICATIONS
1,/,10X,48H REFERENCE M-STATIONS N-STATIONS ,/,11X,
19H STATION ,18X,1H ,18X,1H ,/,19X,39H 1ST HALF 2ND HALF 1ST HALF
1 2ND HALF ,/)
DO 2 J=1,J1
1 MP(J,1)=0
2 MP(J,2)=0
DO 3 J=1,J2
NP(J,1)=0
3 NP(J,2)=0
4 IF (MX.GE.7) GO TO 4
KN1=MX
4 IF (NX.GE.7) GO TO 5
KN1=NX
5 IF (MX.LT.7) GO TO 6
KN1=(MX+1)/2
KN2=KN1
6 IF (NX.LT.7) GO TO 7
KN1=(NX+1)/2
KN2=KN1
READ DATA CARDS
7 READ (JREAD,8) NAME,K1,NL
8 FORMAT (A4,1X,2I5)
IF (NAME.EQ.MN) GO TO 11
IF (NAME.EQ.M) GO TO 9
IF (NAME.EQ.N) GO TO 10
GO TO 12
9 IF (K1.LE.0.OR.K1.GE.MX) GO TO 7
IF (K1.LT.KN1) MP(K1,1)=IABS(NL)
IF (K1.GE.KN1) MP(K1-KN1+1,2)=IABS(NL)
L1=L1+IABS(NL)
GO TO 7

```

10 TST  
11 TST  
12 TST  
13 TST  
14 TST  
15 TST  
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51 TST

```

10 IF (K1.LE.0.OR.K1.GE.NX) GO TO 7
   IF (K1.LI.KN1)NP(K1,1)=IABS(NL)
   IF (K1.GE.KN1)NP(K1-KN1+1,2)=IABS(NL)
   L2=L2+IABS(NL)
   GO TO 7
11 M1=4X+L1
   M2=NX+L2
   IF ((2*(M1/2)).EQ.M1.OR.(2*(M2/2)).EQ.M2) GO TO 14
   GO TO 16
12 WRITE (JWRITE,13)
13 FORMAT (1X,///,1X,57HERROR... DATA CARD IN TEST ROUTINE HAS NO DIR
   1ECTION LABEL,///)
   CALL EXIT
   RETURN
14 WRITE (JWRITE,15) M1,M2
15 FORMAT (1X,///,1X,38HWARNING... TOTAL NUMBER OF M-STATIONS(.13,16H
   1) CR N-STATIONS(.13,22H) IS NOT AN ODD NUMBER,///)
16 IF (M1.EQ.MX)M1=0
   IF (M2.EC.NX)M2=0
   K=KM1
   IF (KN1.GT.K)K=KN1
   DO 23 J=1,K
   IF (J.LE.KM1.AND.J.LE.KN1) GO TO 17
   IF (J.LE.KM1.AND.J.GT.KN1) GO TO 19
   IF (J.GT.KM1.AND.J.LF.KN1) GO TO 21
17 WRITE (JWRITE,18) J,MP(J,1),MP(J,2),NP(J,1),NP(J,2)
18 FORMAT (12X,13,7X,13,7X,13,6X,13,7X,13)
   GO TO 23
19 WRITE (JWRITE,20) J,MP(J,1),MP(J,2)
20 FORMAT (12X,13,7X,13,7X,13)
   GO TO 23
21 WRITE (JWRITE,22) J,MP(J,1),NP(J,2)
22 FORMAT (12X,13,26X,13,7X,13)
23 CONTINUE
   WRITE (JWRITE,24)
24 FORMAT (1X,///)
   RETURN
   END

```

SUBROUTINE PCS(K,F,X,XY,Y,INPTS,KN,C,D,DIAG,JWRITE,J4,J3,M1,N,J,KK PCS 1

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TST 53  
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TST 56  
TST 57  
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TST 59  
TST 60  
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TST 86  
TST 87  
TST 88  
TST 89

2 PCS  
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31 PCS  
32 PCS  
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35 PCS  
36 PCS  
37 PCS  
38 PCS  
39 PCS  
40 PCS  
41 PCS  
42 PCS  
43 PCS

```

1)
C*** CONTROL ROUTINE FOR PIECEWISE CUBIC SPLINE
C
C DIMENSION F(J4),X(J4),XY(J3),Y(J3),C(4,J4),C(J4),DIAG(J4),N(J,2)
COMMON /CODE/ICODE,IBP1,IBP2
C
KN=K+(K-1)*INPTS
JPID2=K
IF (M1.EQ.0) GO TO 1
IF (ICODE.EQ.0)KN=JPID2+IBP1
IF (ICODE.EQ.1)KN=JPID2+IBP2
1 IF (KN.EQ.K) GO TO 2
DE=1.0E-4
GO TO 4
2 DO 3 I=1,K
Y(I)=F(I)
3 XY(I)=X(I)
GO TO 9
4 C(2,1)=(F(2)-F(1))/(X(2)-X(1))
C(2,K)=(F(K)-F(K-1))/(X(K)-X(K-1))
DO 5 I=1,K
C(1,I)=F(I)
5 CALL SPLINE(K,X,C,D,DIAG,J4)
XX=X(1)
XXF=X(K)
XINC=0.0E0
M=C
L=1
6 M=M+1
IF (M.GT.KN) GO TO 10
XX=XX+XINC
IF (ABS(XX-XXH).LT.DF)XX=XXH
IF (XX.EQ.XXH) GO TO 7
IF (ABS(XX-X(L)).LT.DF)XX=X(L)
IF (ABS(XX-X(L+1)).LT.DF)XX=X(L+1)
IF (XX.EQ.X(L+1).AND.XX.NE.X(K))L=L+1
7 XY(M)=XX
Y(M)=DCUBIC(XX,X,C,K,J4)
IF (XX.EC.XXH) GO TO 9
IF (M1.EQ.0) GO TO 8
IF (M.EQ.0)INPTS=N(L,ICODE+1)

```



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44 PCS  
45 PCS  
46 PCS  
47 PCS  
48 PCS  
49 PCS  
50 PCS  
51 PCS  
52 PCS

1 SPL  
2 SPL  
3 SPL  
4 SPL  
5 SPL  
6 SPL  
7 SPL  
8 SPL  
9 SPL  
10 SPL  
11 SPL  
12 SPL  
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30 SPL

```

IF (KK.EQ.1.AND.(JP1D2-L).NE.0)INPTS=N(JP1D2-L,ICODE+1)
8 IF (L.LT.K)XINC=(X(L+1)-X(L))/(INPTS+1)
GO TO 6
9 RETURN
10 WRITE (JWRITE,11) M,KN
11 FORMAT (3X,16HERROR IN PCS: M=,I4.6H > KN=,I4)
12 CALL EXIT
RETURN
END

```

```

C
C***
C
C
SUBROUTINE SPLINE(NP1,XI,C,D,DIAG,J)
PIECEWISE CUBIC SPLINE
DIMENSION XI(J),C(4,J),D(J),DIAG(J)

```

```

D(1)=0.OE0
DIAG(1)=1.OE0
N=NP1-1
DO 1 M=2,NP1
D(M)=XI(M)-XI(M-1)
1 DIAG(M)=(C(1,M)-C(1,M-1))/D(M)
DO 2 M=2,N
C(2,M)=3.OE0*(D(M)+DIAG(M+1)+D(M+1)*DIAG(M))
2 DIAG(M)=2.OE0*(D(M)+D(M+1))
DO 3 M=2,N
G=-D(M+1)/DIAG(M-1)
DIAG(M)=DIAG(M)+G*D(M-1)
3 C(2,M)=C(2,M)+G*C(2,M-1)
NJ=NP1
DO 4 M=2,N
NJ=NJ-1
4 C(2,NJ)=C(2,NJ)-D(NJ)*C(2,NJ+1))/DIAG(NJ)
DO 5 I=1,N
DX=XI(I+1)-XI(I)
DF1=(C(1,I+1)-C(1,I))/DX
DF3=C(2,I)+C(2,I+1)-2.OE0*DF1
C(3,I)=(DF1-C(2,I)-DF3)/DX
5 C(4,I)=DF3/DX/DX
PF TURN

```

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SPL 31

1 PCB  
2 PCB  
3 PCB  
4 PCB  
5 PCB  
6 PCB  
7 PCB  
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9 PCB  
10 PCB  
11 PCB  
12 PCB  
13 PCB  
14 PCB  
15 PCB  
16 PCB  
17 PCB  
18 PCB  
19 PCB  
20 PCB  
21 PCB

END

FUNCTION PCUBIC(XBAR,XI,C,NP1,J)

C\*\*\* FUNCTION EVALUATION OF PIECEWISE CUBIC SPLINE

C DIMENSION XI(J),C(4,J)

C I=1

DX=XBAR-XI(I)

IF (DX) 1,4,3

1 IF (1.EQ.1) GO TO 4

I=I+1

DX=XBAR-XI(I)

IF (DX) 1,4,4

2 I=I+1

DX=DDX

3 IF (1.EQ.(NP1-1)) GO TO 4

DDX=XBAR-XI(I+1)

IF (DDX) 4,2,2

4 PCUBIC=C(1,I)+DX\*(C(2,I)+DX\*(C(3,I)+DX\*C(4,I)))

RETURN

END

SUBROUTINE XYZPLT(M,N,XFUS,SFUS)

1 XYZ  
2 XYZ  
3 XYZ  
4 XYZ  
5 XYZ  
6 XYZ  
7 XYZ  
8 XYZ  
9 XYZ  
10 XYZ  
11 XYZ  
12 XYZ  
13 XYZ  
14 XYZ

C\*\*\* CONTROL ROUTINE FOR CONFIGURATION PLOTS

C DIMENSION FIRST(7),XFUS(N),SFUS(N,M,2)

COMMON /PASS/ABC(20),ABCDE(20),HORZ,VERT,YEST1,PHI,THETA,PSI,XF,YF

1,ZF,DIST,FMAG,PLOTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,

1ZMID,BIGD,KODE,ISP

COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI

ITE

COMMON /PCODE/LCODE

COMMON /TRANS/TITLE(20)

DATA FIRST/4HNEW,4HBODY,4H WIT,4HH IM,4HPRCV,4HED G,4HRIID /.TAME/

14H

**15**    **xxvz**

```

DO 1 I=1,20
IF (LCODE.EQ.1)ABC(I)=TITLE(I)
IF (LCODE.EQ.2.AND.I.LE.7)ABC(I)=FIRST(I)
1 IF (LCODE.EQ.2.AND.I.GT.7)ABC(I)=TAME
WRITE (JWRITE,2) (ABC(I),I=1,20)
2 FORMAT (28X25HCONFIGURATION DESCRIPTION//1X20A//)
C*** INPUT CONFIGURATION DESCRIPTION AND INITIALIZE
CALL CBC10(M,N,XFUS,SFUS)
PLOT CONFIGURATION
C*** WRITE (JWRITE,3)
3 FORMAT (//36X9HPLOT DATA//)
4 READ (JREAD,5) (ABCDE(I),I=1,20)
5 FORMAT (20A4)
WRITE (KFILE3,5) (ABCDE(I),I=1,20)
REWIND KFILE3
READ (KFILE3,6) HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,ZF,DIST,FMAG,P
1 LCITSZ,TYPE,KODE
PCWIND KFILE3
6 FORMAT (2A2,A3,9F5.3,A3,16X,11)
WRITE (JWRITE,7) HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,ZF,DIST,FMAG,
1PLOTSZ,TYPE,KODE
7 FORMAT (1X,2A2,A3,9(1X,F10.5),A3,16X,11)
CALL CBC20(M,N)
IF (KODE.EQ.0) GO TO 4
WRITE (JWRITE,8)
8 FORMAT (1X,/,1X,127(.-))
RETURN
END

```

C	C	C	C	C	C	C	C	C	C
0	0	0	0	0	0	0	0	0	0
1	2	3	4	5	6	7	8	9	10

```

C
C***
SUBROUTINE CBC13(NRADX,NFORX,XFUS,XFUS,SFUS)
C
C      INPUTS AND INITIALIZES CONFIGURATION DESCRIPTION
C
COMMON /PASS/ABC(20),ABCDE(20),HORZ,ERT,TEST1,PHI,THETA,PSI,XF,YF
1,ZF,DIST,FMAG,PLOTS2,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
2,ZMID,BIGD,KODE,ISP
COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILF1,KFILE2,KFILF3,KFILE4,IWR1
1VE
DIMENSION XFUS(NFORX),SFUS(NFORX,NRADX,2)

```

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COMMON /AV/ALRT(212,3,2),VECRT(211,3)
COMMON /PCODE/LCODE

REWIND KFILE1
REWIND KFILE2
REWIND KFILE4
LREAD=KFILE1
IF (LCODE.NE.1) LREAD=KFILE4
NRAD=NRADX
NFUSOR=NFORX
N=NFUSCR
READ (LREAD)(XFUS(1),I=1,N)
IF (IWRITE.EQ.0) WRITE (JWRITE,1) (XFUS(1),I=1,N)
1 FORMAT (1X,F10.5,1X,F10.5,1X,F10.5,1X,F10.5,1X,F10.5,1X,F
110.5,1X,F10.5,1X,F10.5,1X,F10.5)
IF (IWRITE.EQ.0) WRITE (JWRITE,2)
2 FORMAT (1X,/)
DO 4 NN=1,N
DO 3 K=1,2
READ (LREAD)(SFUS(NN,MM,K),MM=1,NRAD)
IF (IWRITE.EQ.0) WRITE (JWRITE,1) (SFUS(NN,MM,K),MM=1,NRAD)
3 CONTINUE
IF (IWRITE.EQ.0) WRITE (JWRITE,2)
4 CONTINUE
XMIN=XFUS(1)
XMAX=XFUS(1)
YMAX=SFUS(1,1,1)
ZMIN=SFUS(1,1,2)
ZMAX=SFUS(1,1,2)
XMIN=AMIN1(XMIN,XFUS(1))
XMAX=AMAX1(XMAX,XFUS(NFUSOR))
DO 5 NN=1,NFUSOR
DO 5 NR=1,NRAD
YMAX=AMAX1(YMAX,SFUS(NN,NR,1))
ZMIN=AMIN1(ZMIN,SFUS(NN,NR,2))
ZMAX=AMAX1(ZMAX,SFUS(NN,NR,2))
5 SETUP 1ST LINE IN STREAMWISE DIRECTION
C**
NL1=NFUSOR-1
NAN=NRAD
DO 6 N=1,NFUSOR
ALPT(N,1,2)=XFUS(N)
ALPT(N,2,2)=SFUS(N,1,1)

```

156

ZMID=.5\*(ZMAX-ZMIN)+ZMIN  
 RETURN  
 END

SUBROUTINE SURCL(NPT)

C\*\*\* COMPUTES SURFACE UNIT NORMALS

C COMMON /AV/FLINE(212,3,2),FVEC(211,3)

C DO 2 N=2,NPT

T1X=FLINE(N,1,2)-FLINE(N-1,1,1)  
 T2X=FLINE(N-1,1,2)-FLINE(N,1,1)  
 T1Y=FLINE(N,2,2)-FLINE(N-1,2,1)  
 T2Y=FLINE(N-1,2,2)-FLINE(N,2,1)  
 T1Z=FLINE(N,3,2)-FLINE(N-1,3,1)  
 T2Z=FLINE(N-1,3,2)-FLINE(N,3,1)

XNX=T2Y\*T1Z-T1Y\*T2Z

YNY=T1X\*T2Z-T2X\*T1Z

ZNZ=T2X\*T1Y-T1X\*T2Y

FN=SQRT(XNX\*\*2+YNY\*\*2+ZNZ\*\*2)

IF (FN.EQ.0.) GO TO 1

FVEC(N,1,1)=XNX/FN

FVEC(N,1,2)=YNY/FN

FVEC(N,1,3)=ZNZ/FN

GO TO 2

1 FVEC(N-1,1,1)=0.

FVEC(N-1,2,1)=0.

FVEC(N-1,3,1)=0.

2 CONTINUE

RETURN

END

SUBROUTINE SURCC(NPT)

C\*\*\* COMPUTES SURFACE UNIT NORMALS

C COMMON /AV/FLINE(212,3,2),FVEC(211,3)

C10 95  
 C10 96  
 C10 97

SCL 1  
 SCL 2  
 SCL 3  
 SCL 4  
 SCL 5  
 SCL 6  
 SCL 7  
 SCL 8  
 SCL 9  
 SCL 10  
 SCL 11  
 SCL 12  
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 SCL 24  
 SCL 25  
 SCL 26  
 SCL 27  
 SCL 28

SCC 1  
 SCC 2  
 SCC 3  
 SCC 4  
 SCC 5

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6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28  
SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC SCC

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DO 2 N=2,NPT
T1X=FLINE(N,1,2)-FLINE(N-1,1,1)
T2X=FLINE(N,1,1)-FLINE(N-1,1,2)
T1Y=FLINE(N,2,2)-FLINE(N-1,2,1)
T2Y=FLINE(N,2,1)-FLINE(N-1,2,2)
T1Z=FLINE(N,3,2)-FLINE(N-1,3,1)
T2Z=FLINE(N,3,1)-FLINE(N-1,3,2)
XNX=T2Y*T1Z-T1Y*T2Z
YNY=T1X*T2Z-T2X*T1Z
ZNZ=T2X*T1Y-T1X*T2Y
FN=SQRT(XNX**2+YNY**2+ZNZ**2)
IF (FN.EQ.0.) GO TO 1
FVEC(N-1,1)=XNX/FN
FVEC(N-1,2)=YNY/FN
FVEC(N-1,3)=ZNZ/FN
GO TO 2
1 FVEC(N-1,1)=0.
FVEC(N-1,2)=0.
FVEC(N-1,3)=0.
2 CONTINUE
RETURN
END

```

C

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16  
C20 C20 C20 C20 C20 C20 C20 C20 C20 C20 C20 C20 C20 C20 C20 C20

```

SUBROUTINE CBC20(NRADX,NFORX)
C***
C CONTROL ROUTINE FOR VARIOUS TYPES OF PLOTS OF A BODY
C
COMMON /PASS/ABC(20),ABCDE(20),HORZ,VERT,TEST1,PHI,THETA,PS1,XF,YF
1,ZF,DIST,FMAG,PLOTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
12MID,BIGD,KODE,ISP
COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
11E
DIMENSION ORG(3)
DATA TYPEP/3HPER/,TYPES/3HSTE/,TYPEV/3HVU3/
DATA X1/I-X/,Y1/I-HY/,Z1/I-HZ/
C
REWIND KFILE2
C***
SAVE MIN AND MAX
KSAV=XMIN

```

C

C

C

C





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CALL CALPLT(0.,YORG,-3)
CALL CBC21(NRADX,NFORX)
REWIND KFILE
HORIZ=Y1
YORG=ORG(3)-ORG(2)
YMIN=FLOAT(IFIX(YSAV/SCALE))*SCALE
CALL CALPLT(0.,YORG,-3)
CALL CBC21(NRADX,NFORX)
X=FLOAT(IFIX(PLOTSZ+6.))
Y=1.-ORG(3)
GO TO 9
IF (TYPE.EQ.TYPES) GO TO 7
NOTATE ID CN PLOT
X=0.
NCHAR=FIX(11.*PLOTSZ)+3
IF (NCHAR.LE.80) GO TO 6
NDIF=(NCHAR-80)/2
X=FLOAT(NDIF)/11.
NCHAR=80
CALL NOTATE(X,.5..1,ABC,0.,NCHAR)
CALL NOTATE(X,0.,1,ABCDE,0.,NCHAR)
CALL CALPLT(0.,0.,-3)
IF (TYPE.EQ.TYPEP.OR.TYPE.EQ.TYPES) GO TO 8
ORTHOGRAPHIC
CALL CBC21(NRADX,NFORX)
X=FLOAT(IFIX(PLOTSZ+2.))
Y=-3.
GO TO 9
ISP=1
IF (TYPE.EQ.TYPES) ISP=2
PERSPECTIVE OR STEREO
CALL CBC22(NRADX,NFORX)
X=PLOTSZ+2.
IF (TYPE.EQ.TYPES) X=X+PLOTSZ
Y=-3.
END OF COMPLETE PLOT
CALL CALPLT(X,Y,-3)
RESTORE MIN AND MAX
XMIN=XSAV
YMIN=YSAB
ZMIN=ZSAV
XMAX=XMSAV

```

C20 101  
C20 102  
C20 103  
C20 104

[illegible]

YMAX=YMSAV  
ZMAX=ZMSAV  
RETURN  
END

SUBROUTINE CBC21 (NRADX,NFORX)

# CONTROL ROUTINE FOR ORTHOGRAPHIC PROJECTIONS

```
COMMON /PASS/ABC(20),ABCDE(20),HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,  
1,ZF,DIST,FMAG,PLOT SZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,  
12,MID,BIGD,KCDE,ISP  
DIMENSION C(3)  
COMMON /DPLY/ALINE(212,3),RLINE(212,2),RVEC(211,2),PLINE(212,2),A(  
12,3),NNUM(13)  
DATA XSEE/2HX /,YSEE/2HY /,XINTST/3HOUT/,CCNV/.017453293/  
DATA HVU3/3HVU3/
```

INITIALIZE

```

INITIALIZE
IITEST1=1
DMAX=BIGD
IITEST2=1
IF (XINIST.NE.TEST1) ITEST1=0
IF (PSI.EQ.0..AND.THETA.EQ.0..AND.PHI.EQ.0.) ITEST2=0
SCALF=DMAX/PLOTSZ
PHI=CCNV*PHI
THETA=CCNV*THETA
PSI=CCNV*PSI
IF (TYPE.EC.HVU3) GO TO 1
XDIS=XMAX-XMIN
YDIS=YMAX-YMIN
ZDIS=ZMAX-ZMIN
XFIX=.5*(DMAX-XDIS)
XMIN=XMIN-XFIX
XMAX=XMAX+XFIX
YFIX=.5*(DMAX-YDIS)
YMIN=YMIN-YFIX
YMAX=YMAX+YFIX
ZFIX=.5*(DMAX-ZDIS)
ZMIN=ZMIN-ZFIX

```

```

36 ZMAX=ZMAX+ZFIX
37 ADJUST MINIMUMS FOR GRID LINES
38 XMIN=FLOAT(IFIX(XMIN/SCALE))*SCALE
39 YMIN=FLOAT(IFIX(YMIN/SCALE))*SCALE
40 ZMIN=FLOAT(IFIX(ZMIN/SCALE))*SCALE
41
42 SETUP AXIS
43 SINPSI=SIN(PSI)
44 SINTE=SIN(THETA)
45 SINPHI=SIN(PHI)
46 CCOSPSI=CCS(PSI)
47 COSTHE=COS(THETA)
48 COSPHI=COS(PHI)
49 IF (XSEE.NF.HORZ) GO TO 3
50 USE X FOR HORIZONTAL VARIABLE
51 IF (ITEST2.EQ.0) GO TO 2
52 A(1,1)=COSTHE*CCOSPSI
53 A(1,2)=-SINPSI*COSPHI+SINTE*CCOSPSI*SINPHI
54 A(1,3)=SINPSI*GINPHI+SINTE*SINPSI*COSPHI
55
56 HMIN=XMIN
57 HMAX=XMAX
58 HMID=XMID
59 INCRZ=1
60 GO TO 7
61
62 IF (YSEE.NE.HORZ) GO TO 5
63 USE Y FOR HORIZONTAL VARIABLE
64 IF (ITEST2.EQ.0) GO TO 4
65 A(1,1)=CCS(PIE*SINPSI)
66 A(1,2)=CCOSPSI*CCOSPHI+SINTE*SINPSI*SINPHI
67 A(1,3)=-CCOSPSI*SINPHI+SINTE*SINPSI*COSPHI
68
69 HMIN=YMIN
70 HMAX=YMAX
71 HMID=YMID
72 INCPZ=2
73 GO TO 7
74
75 USE Z FOR HORIZONTAL VARIABLE
76 IF (ITEST2.EQ.0) GO TO 6
77 A(1,1)=-SINTE
78 A(1,2)=COSTHE*SINPHI
79 A(1,3)=COSTHE*COSPHI
80
81 HMIN=ZMIN
82 HMAX=ZMAX
83 HMID=ZMID

```

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```

      IHRZ=3
      7 IF (XSEE.NF.VERT) GO TO 9
      C** USE X FOR VERTICAL VARIABLE
      IF (ITEST2.EQ.0) GO TO 8
      A(2,1)=COSTHE*COSPSI
      A(2,2)=-SINPSI*COSPHI+SINHE*COSPSI*SINPHI
      A(2,3)=SINPSI*SINPHI+SINHE*COSPSI*COSPHI
      8 VMIN=XMIN
      VMAX=XMAX
      VMID=XMID
      IVERT=1
      GO TO 13
      9 IF (YSEE.NF.VERT) GO TO 11
      C** USE Y FOR VERTICAL VARIABLE
      IF (ITEST2.EQ.0) GO TO 10
      A(2,1)=COSTHE*SINPSI
      A(2,2)=COSPSI*COSPHI+SINHE*SINPSI*SINPHI
      A(2,3)=-COSPSI*SINPHI+SINHE*SINPSI*COSPHI
      10 VMIN=YMIN
      VMAX=YMAX
      VMID=YMID
      IVERT=2
      GO TO 13
      C** USE Z FOR VERTICAL VARIABLE
      11 IF (ITEST2.EQ.0) GO TO 12
      A(2,1)=-SINHE
      A(2,2)=CCSTHE*SINPHI
      A(2,3)=COSTHE*COSPHI
      12 VMIN=ZMIN
      VMAX=ZMAX
      VMID=ZMID
      IVERT=3
      C** CHECK PAPER PLATE
      13 IF (.NOT.((IHRZ.EQ.1.AND. IVERT.EQ.2).OR.( IVERT.EQ.1.AND. IHRZ.EQ.
      12))) GO TO 14
      ITEST=3
      C(1)=-SINTFF
      C(2)=COSTHE*SINPHI
      C(3)=COSTHE*COSPHI
      GO TO 16
      14 IF (.NOT.((IHRZ.EQ.1.AND. IVERT.EQ.3).OR.( IVERT.EQ.1.AND. IHRZ.EQ.
      13))) GO TO 15

```

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 C21 79  
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 C21 117  
 C21 118  
 C21 119

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```

I TEST=2
C(1)=COSTHE*SINPSI
C(2)=COSPSI*COSPHI+SINTHE*SINPSI*SINPHI
C(3)=-COSPSI*SINPHI+SINTHE*SINPSI*COSPHI
GO TO 16
15 ITEST=1
C(1)=COSTHE*COSPSI
C(2)=-SINPSI*COSPHI+SINTHE*COSPSI*SINPHI
C(3)=SINPSI*SINPHI+SINTHE*COSPSI*COSPHI
CENTER WITHIN PAGE SIZE IF SIZE GREATER THAN 28 INCHES
16 IF (PLTISZ.GT.28..AND.TYPE.NE.FVU3)VMIN=-13.*SCALE+FLOAT(IFIX(VMID
1/SCALE))*SCALE
ROTATE MIDPOINT TO PLACE ROTATED VIEW CORRECTLY
IF (ITEST2.FO.0) GO TO 17
AMID1=A(1,1)*XMID+A(1,2)*YMID+A(1,3)*ZMID
AMID2=A(2,1)*XMID+A(2,2)*YMID+A(2,3)*ZMID
HMIN=HMIN-HMID+AMID1
VMIN=VMIN-VMID+AMID2
BEGIN PLOTTING LINES
17 CALL PLOTIT(NRADX,NFORX,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN,
1/SCALE,C)
CALL PLOTIT(NFORX,NRADX,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN,
1/SCALE,C)
RETURN
END

```

```

SUBROUTINE PLOTIT(NL,NPT,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN,
1/SCALE,C)
1 2 3 4 5 6 7 8 9 10 11 12 13 14
PLT PLT PLT PLT PLT PLT PLT PLT PLT PLT PLT PLT PLT PLT
C*** READS LINES OF POINTS DEFINING A SURFACE FROM DISK, MANIPULATES IN
C*** SPECIFIED MANNER, AND PLOTS
C
COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
17E
DIMENSION VECR(211,3,2),VECLF(211,3,2),XLIN(214,2),C(3)
COMMON /DPLT/ALINF(212,3),RLINF(212,2),RVFC(211,2),PLINE(212,2),A(
12,3),NNUM(10)
NVFC=NPT-1
DO 31 N=1,NL

```

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PLT 56

```

IF (N.GT.1) GO TO 1
KODE=3
K1=2
K2=2
GO TO 4
1 KODE=1
K1=1
K2=2
DO 3 NV=1,NVEC
DO 2 N2=1,3
VECT(NV,N3,1)=VECT(NV,N3,2)
VECLF(NV,N3,1)=VECLF(NV,N3,2)
2 CONTINUE
3 CONTINUE
4 READ (KFILE2)((ALINE(NN,N3),NN=1,NPT),N3=1,3)
IF (N.NE.NL) GO TO 5
KODE=2
K1=1
K2=1
GO TO 7
5 READ (KFILE2)((VECT(NN,N3,2),NN=1,NVEC),N3=1,3)
DO 6 NN=1,NVEC
VECLF(NN,1,2)=VECT(NN,1,2)
VECLF(NN,2,2)=-VECT(NN,2,2)
6 VECLF(NN,3,2)=VECT(NN,3,2)
7 DO 30 NN2=1,2
C*** LOOP FOR RIGHT AND LEFT SIDE OF BODY
IF (NN2.EQ.1) GO TO 9
DO 8 NN=1,NPT
8 ALINE(NN,2)=-ALINE(NN,2)
9 IF (ITEST1.EQ.1) GO TO 14
IF (ITEST2.EQ.1) GO TO 11
C*** NO ROTATION OR VISIBILITY TEST
DO 10 NN=1,NPT
XLINE(NN,1)=ALINE(NN,1HCRZ)
XLINE(NN,2)=ALINE(NN,1VERT)
10 GO TO 13
C*** PUTATE BUT NO VISIBILITY TEST
11 CALL PIROT(NPT)
DO 12 NN=1,NPT
DO 12 N2=1,2
XLINE(NN,N2)=ALINE(NN,1,2)

```

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63	64	65
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69	70	71
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72	73	74
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75	76	77
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78	79	80
P	L	T
81	82	83
P	L	T
84	85	86
P	L	T
87	88	89
P	L	T
90	91	92
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93	94	95
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96	97	98
P	L	T

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```

26 RVEC(M,N2)=-RVEC(M,N2)
27 IF (NSET.EQ.0) GO TO 30
C*** SCALE AND PLOT
NIT=0
DO 29 NI=1,NSET
NN=NNUM(NI)
DO 28 NN1=1,NN
NIT=NIT+1
XLINE(NN1,1)=PLINE(NIT,1)
XLINE(NN1,2)=PLINE(NIT,2)
28 CONTINUE
XLINE(NN+1,1)=HMIN
XLINE(NN+1,2)=VMIN
XLINE(NN+2,1)=SCALE
XLINE(NN+2,2)=SCALE
CALL LINE(XLINE(1,1),XLINE(1,2),NN,1,0,0,0)
29 CONTINUE
30 CONTINUE
31 RETURN
END

```

```

SUBROUTINE VISTST(KODE,NPT,NSET)
C*** TESTS A LINE OF POINTS FOR VISIBILITY
C
COMMON /DPLT/ALINE(212,3),RLINE(212,2),RVEC(211,2),PLINE(212,2),A(
12,3),NNUM(13)
C
IWRITE=0
IF (NPT.EQ.81.OR.NPT.LG.85)IWRITE=1
NVEC=NPT-1
NPLT=0
NSET=0
ICOUNT=0
GO TO (1,2,3),KODE
1 N1=1
N2=2
GO TO 4
2 N1=1

```



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19 VIS  
20 VIS  
21 VIS  
22 VIS  
23 VIS  
24 VIS  
25 VIS  
26 VIS  
27 VIS  
28 VIS  
29 VIS  
30 VIS  
31 VIS  
32 VIS  
33 VIS  
34 VIS  
35 VIS  
36 VIS  
37 VIS  
38 VIS  
39 VIS  
40 VIS  
41 VIS  
42 VIS  
43 VIS  
44 VIS  
45 VIS  
46 VIS  
47 VIS  
48 VIS  
49 VIS  
50 VIS  
51 VIS  
52 VIS  
53 VIS

1 PTR  
2 PTR  
3 PTR  
4 PTR

```

N2=1
GO TO 4
3 N1=2
N2=2
4 DO 13 N=1,NPT
  IF (N.EQ.1) GO TO 6
  IF (N.EQ.NPT) GO TO 8
  DO 5 NN=1,N2
  IF ((RVEC(N-1,NN).GT.0.).OR.(RVEC(N,NN).GT.0.)) GO TO 12
5 CONTINUE
GO TO 10
6 DO 7 NN=1,N2
  IF (RVEC(1,NN).GT.0.) GO TO 12
7 CONTINUE
GO TO 10
8 DO 9 NN=1,N2
  IF (RVEC(NVFC,NN).GT.0.) GO TO 12
9 CONTINUE
POINT NOT VISIBLE
10 IF (ICOUNT.LE.1) GO TO 11
  NSET=NSET+1
  NNUM(NSET)=ICOUNT
  ICOUNT=0
  GO TO 13
11 POINT IS VISIBLE
  NPLT=NPLT+1
  ICOUNT=ICOUNT+1
  PLINE(NPLT,1)=RLINE(N,1)
  PLINE(NPLT,2)=RLINE(N,2)
12 CONTINUE
  IF (ICOUNT.LE.1) GO TO 14
  NSET=NSET+1
  NNUM(NSET)=ICOUNT
13 RETURN
14 END

```

SUBROUTINE PIRGT(NPT)  
ROTATES AND PROJECTS A SET OF 3-D POINTS

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```
COMMON /DPLT/ALINE(212,3),RLINE(212,2),RVEC(211,2),PLINE(212,2),A(
12,3),NNUM(10)
DO 2 N=1,NPT
  PLINE(N,1)=0.
  RLINE(N,2)=0.
  DO 1 I=1,2
    DO 1 J=1,3
      RLINE(N,1)=RLINE(N,1)+A(I,J)*ALINE(N,J)
1 CONTINUE
2 CONTINUE
  RETURN
  END
```

5 PTR  
6 PTR  
7 PTR  
8 PTR  
9 PTR  
10 PTR  
11 PTR  
12 PTR  
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14 PTR  
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16 PTR  
17 PTR

```
SUBROUTINE VECROT(NVEC,C,FVEC,RVEC)
  TRANSFORMS VECTORS
  DIMENSION C(3),FVEC(211,3),RVEC(211)
  DO 2 N=1,NVEC
    SUM=0.
    DO 1 NN=1,3
      SUM=SUM+C(NN)*FVEC(N,NN)
1 SUM=SUM+C(NN)*FVEC(N,NN)
2 RVEC(N)=SUM
  RETURN
  END
```

1 VEC  
2 VEC  
3 VEC  
4 VEC  
5 VEC  
6 VEC  
7 VEC  
8 VEC  
9 VEC  
10 VEC  
11 VEC  
12 VEC  
13 VEC

```
SUBROUTINE CBC22(NRADX,NFORX)
  CONTROL ROUTINE FOR PERSPECTIVE AND STEREO
  COMMON /PASS/ABC(20),ABCD(20),HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,
1,ZF,DIST,FMAG,PLCTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
2,ZMID,HICC,KODE,ISP
  COMMON /INCUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
  TE
  DIMENSION XINIT(2),YINIT(2),ZINIT(2)
```

1 C22  
2 C22  
3 C22  
4 C22  
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10 C22

```

C
11 XINIT(1)=PHI
12 XINIT(2)=XF
13 YINIT(1)=YHETA
14 YINIT(2)=YF
15 ZINIT(1)=PSI
16 ZINIT(2)=ZF
17 CALL STERPT(XINIT,YINIT,ZINIT,0.1,0.3,PLOTSZ,DIST,FMAG)
18 LOOP FOR RIGHT AND LEFT FRAMES
19 DO 1 IC=1,ISP
20 REWIND KFILE2
21 NCI=-IC
22 BEGIN PLOTTING LINES
23 CALL PLTIT3(NRADX,NFORX,PHI,THETA,PSI,XF,YF,ZF,PLOTSZ,DIST,FMAG,NC
24 11)
25 CALL PLTIT3(NFORX,NRADX,PHI,THETA,PSI,XF,YF,ZF,PLOTSZ,DIST,FMAG,NC
26 11)
27 1 CONTINUE
28 RETURN
29 END
30

```

```

1 SUBROUTINE STERPT(X,Y,Z,N,K,NC,IP,PAG,PLA,XPR)
2
3 PLOTS STEREO (PROGRAMMER - GEORGE C. SALLEY)
4
5 DIMENSION VP(3),TRAN(3),SANG(3),CANG(3),ADJ(3),PT(4),XLP(2),ZLP(2)
6 DIMENSION X(1),Y(1),Z(1)
7 DIMENSION PLX(4),PLY(4),PLZ(2)
8 DIMENSION PIX(4),PIY(4),PIZ(2)
9 DIMENSION ILP(4),IPL(4)
10 DATA PI,PI2,PI32,PI42/3.1415926,1.5707963,4.7123889,6.2831952/
11 DATA PAP/1.125/
12 DATA APG/0/
13 DATA NPT/1/
14 DATA FRAME/9.80/
15 DATA TJRN/11.01/
16
17 NC=1
18 KK=K
19 II=IP

```

[illegible]

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10 PANG=PI42-ATAN(((ABS(VY))/(VX)))
11 GO TO 15
12 IF (VY) 14,12,13
12 PANG=PI
13 GO TO 15
13 PANG=PI-ATAN((VY/(ABS(VX))))
14 GO TO 15
14 PANG=PI+ATAN(((ABS(VY))/(ABS(VX))))
15 PANG=PI32-PANG
15 UANG=PANG-VANG
15 RANG=UANG+(2.*VANG)
15 SANG(1)=SIN(UANG)
15 SANG(2)=SIN(RANG)
15 CANG(1)=COS(UANG)
15 CANG(2)=COS(RANG)
15 SANG(3)=VZ/VP(3)
15 CANG(3)=VP(2)/VP(3)
15 VP(3)=VPL
15 XLP(1)=0.
15 ZLP(1)=0.
15 XLP(2)=FRAME
15 ZLP(2)=0.
15 ADJ(1)=PLIM
15 ADJ(2)=PLIM
15 ADJ(3)=ADJ(2)+FRAME
15 IF (N) 60,60,22
16 M=IABS(NC)
16 L=M
17 IF (NPG+NC) 23,17,23
17 IF (2+NC) 60,19,18
18 NPG=2
18 GO TO 20
19 NPG=1
20 DO 21 I=1,L
20 CALL CALPLT(TURN,0.,-3)
21 CONTINUE
21 CALL CALPLT(XLP(M),ZLP(M),3)
22 M=1
22 L=2
23 DO 24 I=M,L
23 IF (NPG) 60,24,30
24 IF (NC) 25,29,29

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25 IF (NPT+NC) 30,26,30
26 IF (2+NC) 60,28,27
27 NPT=2
28 GO TO 29
29 NPT=1
29 CALL CALPLY(XLP(1),ZLP(1),3)
30 DO 58 J=1,N
  PT(1)=((X(NO)-TRAN(1))*CANG(1))-((Y(NO)-TRAN(2))*SANG(1))
  PT(4)=((X(NO)-TRAN(1))*SANG(1))+((Y(NO)-TRAN(2))*CANG(1))
  PT(2)=((PT(4)*CANG(3))-((Z(NO)-TRAN(3))*SANG(3)))
  PT(3)=((PT(4)*SANG(3))+((Z(NO)-TRAN(3))*CANG(3)))
  IF (PT(2)) 31,36,36
31 IF (ILP(1)) 60,32,35
32 IF (11-3) 33,34,60
33 VX=PLX(1)-PT(1)
  VY=PLY(1)-PT(2)
  VZ=PLZ(1)-PT(3)
  VP(1)=SQRT((VX**2)+(VY**2))
  VP(2)=SQRT((VZ**2)+(VP(1)**2))
  VPL=PLY(1)/(VY/VP(1))
  PT(4)=PLX(1)-((VX/VP(1))*VPL)
  PLX(1)=PT(1)
  PT(1)=PT(4)
  PLY(1)=PT(2)
  PT(2)=0.
  PT(4)=PLZ(1)-((VZ/VP(2))*VPL)
  PLZ(1)=PT(3)
  PT(3)=PT(4)
  ILP(1)=1
  GO TO 41
34 ILP(1)=1
35 PLX(1)=PT(1)
  PLY(1)=PT(2)
  PLZ(1)=PT(3)
  GO TO 54
36 IF (ILP(1)) 60,40,37
37 IF (11-3) 38,39,60
38 11=3
  IPL(1)=1
  PIX(1)=PT(1)
  PIY(1)=PT(2)
  PIZ(1)=PT(3)

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VX=PT(1)-PLX(1)
VY=PT(2)-PLY(1)
VZ=PT(3)-PLZ(1)
VP(1)=SORT((VX**2)+(VY**2))
VP(2)=SORT((VZ**2)+(VP(1)**2))
VPL=PT(2)/(VY/VP(1))
PT(2)=0
PT(1)=PT(1)-((VX/VP(1))*VPL)
PT(3)=PT(3)-((VZ/VP(2))*VPL)
39 ILP(1)=0
40 PLX(1)=PT(1)
41 PLY(1)=PT(2)
42 PLZ(1)=PT(3)
43 XP=(PT(1)+(PT(2)*(-PT(1))/(PT(2)+VP(3))))*SF
44 ZP=(PT(3)+(PT(2)*(-PT(3))/(PT(2)+VP(3))))*SF
45 VPL=SORT((XP**2)+(ZP**2))
46 IF (VPL-PLIM) 47,47,42
47 IF (ILP(1+2)) 60,43,46
48 IF (I1-3) 44,45,60
49 PLX(1+2)=XP
50 PLY(1+2)=ZP
51 XP=PLIM*(XP/VPL)
52 ZP=PLIM*(ZP/VPL)
53 ILP(1+2)=1
54 GO TO 53
55 ILP(1+2)=1
56 PLX(1+2)=XP
57 PLY(1+2)=ZP
58 IF (ILP(1+2)) 60,51,48
59 IF (I1-3) 49,53,63
60 I1=3
61 IPL(1+2)=1
62 PLX(1+2)=XP
63 PLY(1+2)=ZP
64 VPL=SORT((PLX(1+2)**2)+(PLY(1+2)**2))
65 XP=PLIM*(PLX(1+2)/VPL)
66 ZP=PLIM*(PLY(1+2)/VPL)
67 ILP(1+2)=0
68 GO TO 52
69 IF ((SORT((PLX(1+2)**2)+(PLY(1+2)**2)))-PLIM) 52,52,48
70 PLX(1+2)=XP

```

ORIGINAL PAGE IS  
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STE 188  
STE 189  
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STE 209  
STE 210

```

53  XPT=XPT+ADJ(I+1)
    YPT=YPT+ADJ(I)
    CALL CALPLT(XPT,YPT,II)
54  II=2
55  IF (IPL(I+2)) 60,56,55
    IPL(I+2)=0
    XP=PIX(I+2)
    ZP=PIY(I+2)
    GO TO 51
56  IF (IPL(I)) 60,58,57
57  IPL(I)=0
    PT(1)=PIX(I)
    PT(2)=PIY(I)
    PT(3)=PIZ(I)
    GO TO 40
58  NC=NC+KK
    XLP(I)=XPT
    ZLP(I)=YPT
    NN=1
59  II=IP
60  RETURN
    END

```

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SUBROUTINE PLTIT3(NL,NPT,PHI,THETA,PSI,XF,YF,ZF,PLOTSZ,DIST,FMAG,N
1CI)
C** READS LINES OF POINTS DEFINING A SURFACE FROM DISK
C
COMMON /INPUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
1TF
DIMENSION ALINE(214,3)
C
    ALINE(NPT+1,1)=PHI
    ALINE(NPT+2,1)=XF
    ALINE(NPT+1,2)=THETA
    ALINE(NPT+2,2)=YF
    ALINE(NPT+1,3)=PSI
    ALINE(NPT+2,3)=ZF
    DO 5 N=1,NL

```



```

C***      READ (KFILE2)((ALINE(NN,N3),NN=1,NPT),N3=1,3)
C***      IF (N.EQ.NL) GO TO 1
C***      SKIP VECTORS
C***      READ (KFILE2)VEC
C***      LOOP FOR RIGHT AND LEFT SIDE OF BODY
1 DO 4 NN2=1,2
  IF (NN2.EQ.1) GO TO 3
  DO 2 NN=1,NPT
    2 ALINE(NN,2)=-ALINE(NN,2)
  3 CALL STERPT(ALINE(1,1),ALINE(1,2),ALINE(1,3),NPT,1,NCI,3,PLOTSZ,DI
    1ST.FMAG)
  4 CCNTINUE
  5 CCNTINUE
  RETURN
  END

```

```

PL3 17
PL3 18
PL3 19
PL3 20
PL3 21
PL3 22
PL3 23
PL3 24
PL3 25
PL3 26
PL3 27
PL3 28
PL3 29
PL3 30
PL3 31

```

```

C***      SUBROUTINE CALPLT(A,B,I)
C***      IMPORTANT??
C***      THIS SUBROUTINE USES THE PLOTTER SOFTWARE AVAILABLE AT N. C. STATE
C***      UNIVERSITY (SUBROUTINES PLOT AND ORIGIN) TO REPRODUCE THE ACTIONS
C***      OF THE CALCOMP SOFTWARE SUBROUTINE CALPLT.
C***      IF THE USER DOES NOT HAVE THE ORIGINAL CALCOMP ROUTINE CALPLT
C***      AVAILABLE TO HIM, HE MUST WRITE A DUMMY SUBROUTINE, USING THE
C***      PLOTTER SOFTWARE AVAILABLE AT HIS INSTALLATION, WHICH WILL
C***      REPRODUCE THE ACTION OF CALPLT.
C***      DIMENSION A(1),B(1)
C***      IF (I.LT.0) GO TO 1
C***      J=1-2
C***      CALL PLOT(A,B,J)
C***      RETURN
C***      J=1ABS(I)
C***      J=J-2
C***      CALL PLJT(A,B,J)
C***      CALL ORIGIN(A,B,1,0)
C***      RETURN

```

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CAL 1
CAL 2
CAL 3
CAL 4
CAL 5
CAL 6
CAL 7
CAL 8
CAL 9
CAL 10
CAL 11
CAL 12
CAL 13
CAL 14
CAL 15
CAL 16
CAL 17
CAL 18
CAL 19
CAL 20
CAL 21
CAL 22
CAL 23
CAL 24

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CAL	25
NOT	1
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NOT	3
NOT	4
NOT	5
NOT	6
NOT	7
NOT	8
NOT	9
NOT	10
NOT	11
NOT	12
NOT	13
NOT	14
NOT	15
NOT	16
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NOT	18
NOT	19
NOT	20
NOT	21
NOT	22
NOT	23
NOT	24
NOT	25
NOT	26

[illegible]

INDEFINITE??

THIS SUBROUTINE USES THE PLOTTER SOFTWARE AVAILABLE AT N. C. STATE UNIVERSITY (SUBROUTINE PLOT) TO REPRODUCE THE ACTIONS OF THE CALCOMP SOFTWARE SUBROUTINE LINE.

IF THE USER DOES NOT HAVE THE ORIGINAL CALCOMP ROUTINE LINE

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AVAILABLE TO HIM, HE MUST WRITE A DUMMY SUBROUTINE, USING THE  
PLCTTER SOFTWARE AVAILABLE AT HIS INSTALLATION, WHICH WILL  
REPRODUCE THE ACTION OF LINE.

DIMENSION A(1),B(1),X(212),Y(212)

XMIN=A(I+1)  
XSCALE=A(I+2)  
YMIN=B(I+1)  
YSCALE=B(I+2)  
DO 1 II=1,1  
X(II)=(A(II)-XMIN)/XSCALE  
Y(II)=(B(II)-YMIN)/YSCALE  
1 CALL PLOT(X,Y,1)  
RETURN  
END

C\*\*  
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C

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OF POOR QUALITY

# SAMPLE INPUT - GRIDPLOT

29	21	63	63	599.0	11.5	0	1.0
11	1	0	0	1	0	0	0
CESENA 182	FUSELAGE	(N=29, M=21)	POINT	MODIFIED			
560							
12.20849609	0.0			-0.42710018	1	1	1
12.20849609	0.0			-0.42710018	1	2	1
12.20849609	0.0			-0.42710018	1	3	1
12.20849609	0.0			-0.42710018	1	4	1
12.20849609	0.0			-0.42710018	1	5	1
12.20849609	0.0			-0.42710018	1	6	1
12.20849609	0.0			-0.42710018	1	7	1
12.20849609	0.0			-0.42710018	1	8	1
12.20849609	0.0			-0.42710018	1	9	1
12.20849609	0.0			-0.42710018	1	10	1
12.20849609	0.0			-0.42710018	1	11	1
12.20849609	0.0			-0.42710018	1	12	1
12.20849609	0.0			-0.42710018	1	13	1
12.20849609	0.0			-0.42710018	1	14	1
12.20849609	0.0			-0.42710018	1	15	1
12.20849609	0.0			-0.42710018	1	16	1
12.20849609	0.0			-0.42710018	1	17	1
12.20849609	0.0			-0.42710018	1	18	1
12.20849609	0.0			-0.42710018	1	19	1
12.20849609	0.0			-0.42710018	1	20	1
12.20849609	0.0			-0.42710018	1	21	1
11.54179382	0.0			-1.63539696	1	22	1
11.54179382	0.0			-1.59789753	2	23	1
11.54179382	0.0			-1.52709770	2	24	1
11.54179382	0.0			-1.44369753	2	25	1
11.54179382	0.0			-1.34999657	2	26	1
11.54179382	0.0			-1.25209613	2	27	1
11.54179382	0.0			-1.12709713	2	28	1
11.54179382	0.0			-0.99579996	2	29	1
11.54179382	0.0			-0.84369946	2	30	1
11.54179382	0.0			-0.65209943	2	31	1
11.54179382	0.0			-0.42710018	2	32	1
11.54179382	0.0			-0.18540013	2	33	1

ORIGINAL PAGE IS  
OF POOR QUALITY

11.54179382	1.562499905	0.07289881	1	13
11.54179382	1.49169731	0.32289863	1	14
11.54179382	1.32915884	0.52289993	1	15
11.54179382	1.10619926	0.67290115	1	16
11.54179382	0.88330330	0.73960114	1	17
11.54179382	0.66670161	0.77089977	1	18
11.54179382	0.44370186	0.77710056	1	19
11.54179382	0.21670252	0.78129959	1	20
11.54179332	0.0	0.78129864	1	21
11.54179332	0.0	-1.87437125	1	22
11.54179332	0.0	-1.85611057	1	23
11.54179332	0.0	-1.81024837	1	24
11.54179332	0.0	-1.74978733	1	25
11.54179332	0.0	-1.66543198	1	26
11.54179332	0.0	-1.54464343	1	27
11.54179332	0.0	-1.37801647	1	28
11.54179332	0.0	-1.18529987	1	29
11.54179332	0.0	-0.97383112	1	30
11.54179332	0.0	-0.73745412	1	31
11.54179332	0.0	-0.48950773	1	32
11.54179332	0.0	-0.23327464	1	33
11.54179332	0.0	-0.03646851	1	34
11.54179332	0.0	0.307330814	1	35
11.54179332	0.0	0.54058963	1	36
11.54179332	0.0	0.71662617	1	37
11.54179332	0.0	0.81041336	1	38
11.54179332	0.0	0.85105801	1	39
11.54179332	0.0	0.87293301	1	40
11.54179332	0.0	0.88954067	1	41
11.54179332	0.0	0.89578819	1	42
11.54179332	0.0	-2.11459732	1	43
11.54179332	0.0	-2.11459827	1	44
11.54179332	0.0	-2.09309564	1	45
11.54179332	0.0	-2.05619621	1	46
11.54179332	0.0	-1.98119735	1	47
11.54179332	0.0	-1.83749676	1	48
11.54179332	0.0	-1.62919712	1	49
11.54179332	0.0	-1.37499905	1	50
11.54179332	0.0	-1.13409737	1	51
11.54179332	0.0	-0.82289904	1	52
11.54179332	0.0	-0.55210012	1	53
11.54179332	0.0	-0.28119946	1	54

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10.20849609	1.722899348	0.0	4	13	1
10.20849609	1.67499828	0.29170024	4	14	1
10.20849609	1.54789829	0.55830002	4	15	1
10.20849609	1.32289791	0.76039708	4	16	1
10.20849609	1.08749771	0.88130093	4	17	1
10.20849609	0.82220057	0.93130016	4	18	1
10.20849609	0.55330109	0.96879864	4	19	1
10.20849609	0.27500153	0.99789906	4	20	1
10.20849609	0.0	1.01339886	4	21	1
9.47949219	0.0	-2.20653439	5	1	1
9.47949219	0.26524454	-2.20542717	5	2	1
9.47949219	0.54416764	-2.18721867	5	3	1
9.47949219	0.83579701	-2.15273476	5	4	1
9.47949219	1.14577866	-2.08340359	5	5	1
9.47949219	1.41740608	-1.93233355	5	6	1
9.47949219	1.61756766	-1.68262959	5	7	1
9.47949219	1.72328186	-1.33718700	5	8	1
9.47949219	1.76175117	-1.08082676	5	9	1
9.47949219	1.77553558	-0.78628421	5	10	1
9.47949219	1.78421116	-0.50451654	5	11	1
9.47949219	1.78129768	-0.29580021	5	12	1
9.47949219	1.77709770	-0.00419952	5	13	1
9.47949219	1.73749823	0.29790026	5	14	1
9.47949219	1.61869312	0.58540034	5	15	1
9.47949219	1.39169788	0.80829787	5	16	1
9.47949219	1.14579964	0.94379997	5	17	1
9.47949219	0.88540164	1.06629807	5	18	1
9.47949219	0.59340156	1.04169750	5	19	1
9.47949219	0.29170134	1.06250133	5	20	1
9.47949219	0.0	1.05279959	5	21	1
8.87543328	0.0	-2.28270912	6	1	1
8.87543328	0.26309351	-2.28068352	6	2	1
8.87543328	0.53076197	-2.26470566	6	3	1
8.87543328	0.84478779	-2.23272228	6	4	1
8.87543328	1.23549366	-2.16308796	6	5	1
8.87543328	1.53539448	-2.01090934	6	6	1
8.87543328	1.73221207	-1.72690201	6	7	1
8.87543328	1.81355011	-1.39728332	6	8	1
8.87543328	1.82675457	-1.06154537	6	9	1
8.87543328	1.82776333	-0.75594687	6	10	1
8.87543328	1.82979193	-0.46503069	6	11	1
8.87543328	1.82579353	-0.18043518	6	12	1

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OF POOR QUALITY

8.87546828	1.82776833	0.11980814	6	13	1
8.87548828	1.80648994	0.44240475	6	14	1
8.87548823	1.74058628	0.77948773	6	15	1
8.87548828	1.45419788	0.86879939	6	16	1
8.87548828	1.15789986	1.01339791	6	17	1
8.87548828	0.92360775	1.07289791	6	18	1
8.87548828	0.61670130	1.09999847	6	19	1
8.87548828	0.30420119	1.12379906	6	20	1
8.87548828	0.0	1.13539886	6	21	1
8.31250000	0.0	-2.32221413	7	1	1
8.31250000	0.30934238	-2.32116604	7	2	1
8.31250000	0.63428217	-2.30083370	7	3	1
8.31250000	0.96966666	-2.25412846	7	4	1
8.31250000	1.31131812	-2.14426041	7	5	1
8.31250000	1.59068489	-1.93829727	7	6	1
8.31250000	1.78097320	-1.63248825	7	7	1
8.31250000	1.85184788	-1.29106236	7	8	1
8.31250000	1.87014583	-0.94641578	7	9	1
8.31250000	1.87067032	-0.63348174	7	10	1
8.31250000	1.87171841	-0.33618915	7	11	1
8.31250000	1.87171841	-0.04413338	7	12	1
8.31250000	1.87067032	0.26303864	7	13	1
8.31250000	1.85955729	0.59784329	7	14	1
8.31250000	1.82052954	0.96629173	7	15	1
8.31250000	1.69789791	1.31879616	7	16	1
8.31250000	1.49999366	1.45325735	7	17	1
8.31250000	1.05829706	1.53129763	7	18	1
8.31250000	0.71253254	1.56879616	7	19	1
8.31250000	0.34792224	1.58539963	7	20	1
8.31250000	0.0	1.59379364	7	21	1
7.73849609	0.0	-2.36459827	8	1	1
7.73849609	0.33750254	-2.36459732	8	2	1
7.73849609	0.69170105	-2.33959675	8	3	1
7.73849609	1.04999924	-2.27705675	8	4	1
7.73849609	1.39369965	-2.11869717	8	5	1
7.73849609	1.64999366	-1.36039539	8	6	1
7.73849609	1.83329868	-1.53119755	8	7	1
7.73849609	1.50829945	-1.17769732	8	8	1
7.73849609	1.91669941	-0.82239973	8	9	1
7.73849609	1.91669941	-0.50209981	8	10	1
7.73849609	1.91669941	-0.19789973	8	11	1
7.73849609	1.91669941	0.10210031	8	12	1

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7.70849609	1.91669941	0.41670342	8	13	1
7.70849609	1.91669941	0.76459897	8	14	1
7.70849609	1.90629864	1.16669846	8	15	1
7.70849609	1.82919788	1.61879635	8	16	1
7.70849609	1.54789925	1.84789658	8	17	1
7.70849609	1.18329906	1.91669846	8	18	1
7.70849609	0.79170342	1.95419598	8	19	1
7.70849609	0.38540173	1.96879768	8	20	1
7.70849609	0.0	1.96879864	8	21	1
7.70849609	0.0	-2.40619659	9	1	1
7.12519836	0.35930206	-2.39579678	9	2	1
7.12519836	0.73750222	-2.37499905	9	3	1
7.12519836	1.11869907	-2.30209732	9	4	1
7.12519836	1.45419884	-2.09999561	9	5	1
7.12519836	1.69789886	-1.80519717	9	6	1
7.12519836	1.86669922	-1.45209789	9	7	1
7.12519836	1.93329906	-1.08329868	9	8	1
7.12519836	1.53750000	-0.72910017	9	9	1
7.12519836	1.53749905	-0.40209949	9	10	1
7.12519836	1.53749905	-0.09369943	9	11	1
7.12519836	1.53749905	0.20839971	9	12	1
7.12519836	1.53749905	0.52710056	9	13	1
7.12519836	1.93749905	0.86329893	9	14	1
7.12519836	1.53750000	1.29789829	9	15	1
7.12519836	1.51669941	1.80629733	9	16	1
7.12519836	1.65629864	2.09379673	9	17	1
7.12519836	1.26035886	2.15629673	9	18	1
7.12519836	0.84380150	2.19789696	9	19	1
7.12519836	0.41040224	2.21249771	9	20	1
7.12519836	0.0	2.21879673	9	21	1
6.56250000	0.0	-2.42709732	10	1	1
6.56250000	0.37330187	-2.42079735	10	2	1
6.56250000	0.76670182	-2.40619659	10	3	1
6.56250000	1.16669941	-2.33749771	10	4	1
6.56250000	1.51459983	-2.11869521	10	5	1
6.56250000	1.76669788	-1.80629716	10	6	1
6.56250000	1.90419985	-1.42289829	10	7	1
6.56250000	1.53749705	-1.02289772	10	8	1
6.56250000	1.53750000	-0.66660017	10	9	1
6.56250000	1.53750000	-0.33959949	10	10	1
6.56250000	1.93750000	-0.03119946	10	11	1
6.56250000	1.93750000	0.27389965	10	12	1



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OF POOR QUALITY

6.56250000	1.93750000	0.58960356	10	13	1
6.56250000	1.93750000	0.94579887	10	14	1
6.56250000	1.93750000	1.36039829	10	15	1
6.56250000	1.91669750	1.86879730	10	16	1
6.56250000	1.73563576	2.25150967	10	17	1
6.56250000	1.33749866	2.36459637	10	18	1
6.56250000	0.48120276	2.36459637	10	19	1
6.56250000	0.42500114	2.36459732	10	20	1
6.56250000	0.0	2.40619755	11	21	1
6.56250000	0.0	-2.39789581	11	1	1
6.56250000	0.38540173	-2.38539696	11	2	1
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**TABLE OF CONTENTS, 1966**

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0-12000000	0-0	0-00000000	20	21	1

[illegible]

Figure 1 illustrates the experimental setup. A participant is seated at a table, looking at a screen. The screen displays a 3x3 grid of stimuli. The stimuli are represented by small circles with numbers inside. The participant is looking at the screen through a viewing device. The setup is labeled 'Experimental setup'.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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ADDITIONAL		ARBITRARY		STATION		SPECIFICATIONS	
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		1ST	2ND	1ST	2ND	1ST	2ND
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2		0	0	0	0	0	0
3		0	0	0	0	0	0
4		0	0	0	1	0	0
5		0	0	0	2	0	0
6		0	0	0	0	0	0
7		0	0	0	0	0	0
8		0	0	0	0	0	0
9		0	0	0	0	0	0
10		0	0	0	0	0	0
11		0	0	0	0	0	0
12		0	0	0	0	0	0
13		0	0	0	0	0	0
14		0	0	0	0	0	0
15		0	0	0	0	0	0
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NEW DATADISK

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**NOTES ON CONTRIBUTORS**

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CEPROM 102 FUELAGE. 'M=20. 'm=211. POINT IDENTIFIED

### 6.9 INT



**NEW BODY WITH IMPROVED GRID**

6.9 2R7

## REFERENCES

1. Fox, S. R.; and Smetana, F. O.: "A Study of Optimum Cowl Shapes and Flow Port Locations for Minimum Drag with Effective Engine Cooling--Volume I." NASA CR-159379, November 1980.
2. Hess, J. L.; and Smith, A. M. O.: "Calculation of Potential Flow About Arbitrary Bodies." Progress in Aeronautical Sciences, Vol. 8, pp. 1-138, Pergamon Press, 1967.
3. Smetana, F. O.; Summey, D. C.; Smith, N. S.; and Carden, R. K.: "Light Aircraft Lift, Drag, and Moment Prediction--A Review and Analysis." NASA CR-2523, May 1975, 480 pages.